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COST 507

**Definition of thermochemical and
thermophysical properties to provide a
database for the development
of new light alloys**

**Thermochemical database for
light metal alloys**

Volume 2

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Edited by

I. Ansara, A. T. Dinsdale, M. H. Rand

July 1998

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COST 507
COORDINATION GROUP C

Final Report Round 2
July 1998

Partners in Coordination Group C, whose results are presented in the pages of this report, are:

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Physical Laboratory, Teddington, U.K.

Institut für Physikalische Chemie, Universität Wien, Austria

GTT - Technologies, Herzogenrath, Germany

INTRODUCTION

The COST-Action 507 has the official title:

Measurement and Evaluation of Thermochemical and Thermophysical Properties to Provide a Database for the Development of New Light Alloys

There are 14 signatory countries to the Action, which had an official commencement date on January 1, 1990.

The countries concerned are:

Austria	Germany	Norway	Switzerland
Belgium	Greece	Portugal	United Kingdom
France	Italy	Spain	
Finland	Netherlands	Sweden	

In addition, the Baikov Institute of Metallurgy, Moscow (Russia) is taking part in the Action.

The work of COST 507 is shared amongst partners in 4 Coordination Groups whose areas of interest are:

- Coordination Group A : Experimental measurement of thermochemical properties
- Coordination Group B : Critical compilation and assessment of constitutional data prior to thermodynamic calculation
- Coordination Group D : Experimental measurement and compilation of thermophysical data

Coordination Group C, whose work is presented in this report, is concerned with the general theme:

Critical thermodynamic evaluation of relevant binary, ternary and higher-order alloy systems to produce a set of optimized coefficients for the light metal alloy database.

The evaluations of Group C incorporate experimental data from Group A and Group D partners, and use the critically compiled constitution data from Group B as basis for the evaluation work.

Using this computer database, which is now in an impressive state of development, it will be possible to calculate the phase equilibria to be expected in complex light alloy systems as a function of a wide range of compositions and temperatures. For example calculation can be made of liquidus and solidus temperatures, crystallization paths for equilibrium and non-equilibrium conditions, nature and amounts of precipitated phases, enthalpy effects associated with phase transformations, etc.

The rapid accessibility of such information will considerably assist the design, manufacture and utilization of a wide range of different alloy types.

The alloy systems towards which the experimental and evaluation work is being directed, together with some major applications, are listed below:

Al-Mg-Mn-Fe-Si	: cans
Al-Mg-Si-Cu (-Fe)	: extrusions, automobiles
Al-Zn-Cu-Mg (-Zr,Cr,rare earth metals)	: aerospace, transport
Al-Li-Cu-Mg-Zr (-H)	: airframes
Ti-Al-Mo-Zr (Cu,B,C,N,O,Si)	: gas turbines
Ti-Al (-V,Cr,Mn,Ni,Fe,Nb), (B,C,N,O,Si)	: gas turbines

EVALUATION PROCEDURE

Bearing in mind the alloy categories defined by industrial partners at the beginning of the Action, a matrix was drawn up to define the binary systems forming the building blocks for the evaluation of higher-order systems. These binaries were then allocated to the different partners in Group C for evaluation.

All partners made use of the selected data for the elements published by A.T. Dinsdale¹ on behalf of SGTE.

There was also agreement amongst partners with respect to the modelling of particular phases so that consistency could be maintained on proceeding from binary to higher-order systems combining evaluations originating from different laboratories. All results were prepared in exactly the same format to facilitate exchange of data and to provide a standard format for computer storage of the data by the database manager, Dr. Ansara, in Grenoble.

Evaluations to produce optimized sets of coefficients were carried out using one or

¹A.T. Dinsdale, *Calphad*, 15, 4, 317-425 (1991).

both of the two programs *Bingss/Tergss* written by Lukas ² and *Parrot* developed by Jansson ³ contained in the *Thermo-Calc* databank system ⁴.

These programs make use of experimental thermodynamic and phase diagram data, which are fed in as measured values with error limits. Using defined models for the different phases of the systems concerned, optimized coefficients are produced which permit a self-consistent description of the thermodynamic properties and the phase boundaries of the alloys.

For some alloy systems the available experimental information is very scarce or unreliable. In such cases, only a part of the system may have been dealt with. In other cases, recourse may have had to be made to estimation procedures to obtain input data for the optimization process. The accuracy of the calculations involving these data will consequently be reduced.

The following pages present in summarized form a complete description of the evaluation work carried out by the partners in Coordination Group C during the course of Round 1 and 2 of COST 507. The brief reports for each system contain a calculated phase diagram, information on the structures of the phases in the system. The thermodynamic coefficients used to produce the calculated information are also given.

²H.L. Lukas, J. Weiss, and E.-Th. Henig, *Calphad*, 6, 229-251 (1982)

³B. Jansson. Ph. D. Thesis, (1984), Div. Phys. Met., Royal Inst. Tech., Stockholm, Sweden.

⁴B. Sundman, B. Jansson, and J.-O. Andersson, *Calphad*, 2, 9, 153-190 (1985).

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Thermodynamic Modelling

I. Ansara and N. Dupin

Introduction

Standard CALPHAD procedures were used to assess the binary and ternary systems defined in the COST507 project. In Round 1, binary systems have been assessed. Several ternary systems have been analysed during Round 2.

In many ternary systems, the three pure elements exhibit different stable crystal structure. Hence data for metastable binary solutions have been obtained and are presented in the tables.

In these systems, there are also many binary phases stable on one binary edge which extend into the ternary system but not all the way across to the other binary edges. (for example, the Laves-C15 in the Cu-Mg-Zn system or the AlM-D0₁₉ in the Al-Ti-X (X=Mo, Nb, Ti, W) systems). Thus to model the intrusion of these phases into the ternary systems, the Gibbs energies of the metastable counterparts of the intruding phase must be defined in the other binary system(s). This means that when the data of these binary systems are retrieved, there will be data for these metastable "counterparts".

As the number of ternary systems increases, the number of metastable solution phases or counterphases will increase sharply and this may lead to increasing computing time and possible problems due to metastable equilibria which may appear during the calculation.

The main characteristics of each system are given in individual chapters which include:

- a summary of the various stable and metastable phases defined in the system, the thermodynamic model used to describe their thermodynamic properties, the name of the assessor and the reference of the publication in which the evaluation is described,
- the thermodynamic properties of the compound and solution phases,
- for the binary systems: the phase diagram,
- for the binary systems: a table giving the invariant reactions,
- a table presenting the crystal structure for each phase in a given system, the structural type, the Pearson Symbol and space group as well as the occupation of the sublattices and comments when necessary. This information is taken from Massalski *et al.* [90Mas] and Villars *et al.* [91Vil].

In Appendix I, the thermodynamic functions for the elements in stable or metastable states are listed as a function of temperature. For magnetic ordering the functions are given in Appendix II.

Thermodynamic Description

Elements

The Gibbs energy of the pure element i , ${}^{\circ}G_i^{\phi}(T)$, referred to the enthalpy for its stable state ϕ at 298.15 K, ${}^{\circ}H_i^{\phi}(298.15\text{K})$, is denoted by GHSER $_i$. This quantity is described as a function of temperature by the following equation:

$$\begin{aligned} \text{GHSER}_i &= {}^{\circ}G_i^{\phi}(T) - {}^{\circ}H_i^{\phi}(298.15\text{K}) \\ &= a + bT + cT \cdot \ln T + dT^2 + eT^3 + fT^{-1} + gT^7 + hT^{-9} \quad (1) \end{aligned}$$

The first and second derivatives of this quantity with respect to temperature are related to the absolute entropy and heat capacity of the compound at the same temperature. Experimental values for heat capacities can thus be directly used in the optimisation and will be related to the coefficients c, d, e, f, g and h .

For elements which display a magnetic ordering (Cr, Fe, Ni and Mn), the term GHSER will be referred to a para-magnetic state. The magnetic contribution is treated explicitly. An additional term is thus added to the molar Gibbs energy of the magnetic phase.

For elements as well as for solutions, this term is equal to:

$$G^{\text{mag}} = RT \ln(\beta + 1) f(\tau) \quad (2)$$

where τ is T/T^* , T^* being the critical temperature for magnetic ordering (Curie temperature T_c for ferromagnetic materials or the Néel temperature T_N for antiferromagnetic materials), and β the average magnetic moment per atom of the alloy expressed in Bohr magnetons.

The function $f(\tau)$ is given as:

$$\tau < 1 : f(\tau) = 1 - [79\tau^{-1}/140p + (474/497)(1/p - 1)(\tau^3/6 + \tau^9/135 + \tau^{15}/600)]/A$$

$$\tau > 1 : f(\tau) = -[\tau^{-5}/10 + \tau^{-15}/315 + \tau^{-25}/1500]/A$$

with $A = 518/1125 + (11692/15975)(1/p - 1)$.

These equations were derived by Hillert *et al.* [78Hil] from an expression of the magnetic heat capacity C_p^{mag} proposed by Inden [81Ind].

The value of p depends on the structure. For example, p is equal to 0.28 for fcc and hcp metals and 0.40 for bcc metals [81Ind].

For each element, equation 1 is taken from the SGTE database [91Din]. These equations and the magnetic parameters for pure elements are given in Appendices I and II.

The function GHSER_i is also often used to express the thermodynamic functions of a structure φ^* different from the stable structure of the pure element. The expression $G_i^{\circ,\varphi^*}(T) - H_i^{\circ,\phi}(298.15\text{K})$ is equivalent to $G_i^{\circ,\varphi^*}(T) - G_i^{\circ,\phi}(T) + \text{GHSER}_i$. The term $G_i^{\circ,\varphi^*}(T) - G_i^{\circ,\phi}(T)$ is often called the lattice stability of element i .

Binary Compounds

The Gibbs energy of formation of the compound A_aB_b is expressed as:

$$G_{A_aB_b}^{\circ}(T) - a H_A^{\circ,\phi}(298.15\text{K}) - b H_B^{\circ,\phi}(298.15\text{K}) = f(T) \quad (3)$$

The expression for $f(T)$ is identical to that given by equation 1.

Equation 3 can be transformed by applying equation 1 for each component

$$\begin{aligned} f(T) &= G_{A_aB_b}^{\circ}(T) - a G_A^{\circ,\phi}(T) - b G_B^{\circ,\phi}(T) + a \text{GHSER}_A + b \text{GHSER}_B \\ &= \Delta_f G_{A_aB_b}^T + a \text{GHSER}_A + b \text{GHSER}_B \end{aligned} \quad (4)$$

The term $\Delta_f G_{A_aB_b}(T)$ is the Gibbs energy of formation of the compound referred to the stable elements at temperature T .

Gaseous species

An expression identical to equation 3 is used to describe the Gibbs energy of formation of the gaseous species with the additional $RT \ln P$ term, where P is the total pressure. The gas phase is assumed to form an ideal solution. The reference state for each vapor species is taken to be the pure component at 0.1 MPa pressure.

Condensed phases

1: Substitutional solutions:

For the substitutional solution ϕ , the Gibbs energy of mixing is expressed as follows:

$$G_m = G^{\phi,\text{id}} + G^{\phi,\text{xs}} \quad (5)$$

with

$$G^{\phi,\text{id}} = RT \sum_i x_i \ln x_i \quad (6)$$

The Redlich - Kister equation [48Red], a power series expansion, is used to express the excess Gibbs energy, $G_m^{\phi,\text{xs}}$, as follows:

$$G_m^{\phi, x^s} = x_i x_j \sum_{\nu=0} L_{ij}^{\nu, \phi} (x_i - x_j)^\nu \quad (7)$$

x_i is the molar fraction of component i with $\sum_i x_i = 1$. The model parameter L_{ij}^ν can be temperature dependent as follows:

$$L_{i,j;i} = y'_i y'_j [a_0 + b_0 T + c_0 T \cdot \ln T (a_1 + b_1 T) (y'_i - y'_j)] \quad (8)$$

For a ternary solution, the excess Gibbs energy is expressed as follows:

$$G^{\phi, x^s} = \sum_i \sum_{j>i} x_i^\phi x_j^\phi \sum_\nu L^{\nu, \phi} - (x_i^\phi - x_j^\phi)^\nu \quad (9)$$

If experimental information relative to ternary solutions are available then an extra term can be added to 9. For a ternary system A-B-C, this term is equal to:

$$x_A x_B x_C (\alpha_1 x_A + \alpha_2 x_B + \alpha_3 x_C) \quad (10)$$

For magnetic alloys, the composition dependence of T_c and β are expressed by:

$$T_c^*(x) = \sum_i x_i T_{c,i}^{o,*} + T_c^{*,x^s} \quad (11)$$

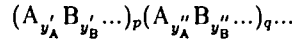
$$\beta(x) = \sum_i x_i \beta_i^o + \beta^{x^s} \quad (12)$$

where T^{*,x^s} and β^{x^s} are both represented by an equation similar to 7.

2: Ordered Phases:

The use of the sublattice model, developed by Hillert and Staffansson [70Hil] based on Temkin's model for ionic solutions [45Tem] and extended by Sundman and Ågren [81Sun], allows a variety of solution phases to be treated, in particular ordered phases.

As non-stoichiometric phases are formed by several sublattices, they can be schematically described as follows:



where the species A, B, ... can be atoms, vacancies or ions on the different sublattices ', ', The number of sites are p, q, \dots . If $p + q + \dots = 1$, then the thermodynamic quantities are referred to one mole of sites.

For each sublattice s , the site fraction of the species i is equal to

$$y_i^s = \frac{n_i^s}{\sum_j n_j^s} = \frac{n_i^s}{n^s} \quad \text{with} \quad \sum_i y_i^s = 1 \quad \text{and} \quad \sum_s n^s = n \quad (13)$$

where n_i^s is the number of species i in sublattice s , n^s the number of sites in sublattice s , and n the total number of sites. n^s is related to n by $n^s = n \cdot p / (p + q + \dots)$. The

number of sublattices and the species occupying them, is generally obtained from crystallographical information.

This model also describes stoichiometric phases, in which case the sublattices are occupied by a single atom, and substitutional phases which only contain one sublattice.

The molar Gibbs energy expressed by the sublattice model is equal to

$$G_m = G^{\text{ref}} + G^{\text{id}} + G^{\text{ex}} \quad (14)$$

For a two sublattice phase taken as an example, with two elements A and B in each of the sublattices, the term G^{ref} , which defines a surface of reference, is equal to

$$G^{\text{ref}} = y'_A y''_A G_{A:A}^{\circ} + y'_A y''_B G_{A:B}^{\circ} + y'_B y''_A G_{B:A}^{\circ} + y'_B y''_B G_{B:B}^{\circ} \quad (15)$$

The terms $G_{A:A}^{\circ}$ and $G_{B:B}^{\circ}$ represent the Gibbs energy of formation of the constituent elements A and B. The colon separates the different sublattices.

The terms $G_{0:A:B}^{\circ}$ and $G_{B:A}^{\circ}$ represent the Gibbs energy of formation of the stoichiometric compounds $A_p B_q$ and $B_p A_q$, which may be stable or metastable.

The term G^{id} is related to the molar configurational entropy and is equal to:

$$G^{\text{id}} = R T [p(y'_A \ln y'_A + y'_B \ln y'_B) + q(y''_A \ln y''_A + y''_B \ln y''_B)] \quad (16)$$

Finally, the excess Gibbs energy G^{ex} is equal to

$$\begin{aligned} G^{\text{ex}} = & y'_A y'_B [y''_A L_{A,B:A} + y''_B L_{A,B:B}] \\ & + y''_A y''_B [y'_A L_{A:A,B} + y'_B L_{B:A,B}] \\ & + y'_A y'_B y''_A y''_B L_{A,B:A,B} \end{aligned} \quad (17)$$

The terms $L_{i,j;i}$ and $L_{i;i,j}$ represent the interaction parameters between the atoms on one sublattice for a given occupancy of the other, and can be described by a polynomial, as follows:

$$L_{i,j;i} = y'_i y'_j [a_0 + b_0 T + (a_1 + b_1 T)(y'_i - y'_j)] \quad (18)$$

The above equations can be expressed for ternary systems and they become more complicated when the number of species increases in each sublattice.

3. Order-disorder transformation:

For the COST project, only the order-disorder transformation relative to the bcc-A2 and bcc-B2 was considered. A unique function representing the Gibbs energy is used to describe the thermodynamic properties of both phases as follows:

$$G_m = G_m^{\text{dis}}(x_i) + \Delta G_m^{\text{ord}}(y_i^j) \quad (19)$$

where $\Delta G_m^{ord}(y_i^s)$ and $G_m^{dis}(x_i)$ are respectively the ordering energy, equal to zero in the disordered state, and $G_m^{dis}(x_i)$ the molar Gibbs energy of the disordered phase. $\Delta G_m^{ord}(y_i^s)$ is equal to:

$$\begin{aligned} \Delta G_m^{ord}(y_i^s) = & \sum_i \sum_j y_i^s y_j^s \Delta^o G_{i;j}^{ord} + RT \left(a \sum_i y_i^s \ln y_i^s + b \sum_i y_i^s \ln y_i^s \right) \\ & + y_A^s y_B^s \sum_i y_i^s L_{A,B;i}^{0,ord} + y_A^s y_B^s (y_A^s - y_B^s) \sum_i y_i^s L_{A,B;i}^{1,ord} \\ & + y_A^s y_B^s \sum_i y_i^s L_{i:A,B}^{0,ord} + y_A^s y_B^s (y_A^s - y_B^s) \sum_i y_i^s L_{i:A,B}^{1,ord} \\ & + y_A^s y_B^s y_A^s y_B^s L_{A,B:A,B}^{ord} \end{aligned} \quad (20)$$

$G_m^{dis}(x_i)$ is given in the Redlich-Kister formalism by equation 7. x_i and y_i^s are the molar fraction of element i in the phase and its site fraction in sublattice s respectively.

To ensure stability of the disordered phase, the first derivative of G_m with respect to the site occupation must be zero for any given composition. This condition and the fact that the ordering energy is zero for disorder leads to constraints between the thermodynamic parameters describing ordering [88Ans]. Using these constraints and converting the Gibbs energy of the disordered state into the sublattice formalism, allows to express the whole Gibbs energy of both phases (A2 and B2) in the sublattice formalism as follows:

$$\begin{aligned} G^o(T) - H_A^{o,ref}(298.15 \text{ K}) &= G(A:A) = \text{GREF}_A \\ G^o(T) - 0.5 H_A^{o,ref}(298.15 \text{ K}) - 0.5 H_B^{o,ref}(298.15 \text{ K}) &= G(A:B) = \\ & 0.5 \text{GREF}_A + 0.5 \text{GREF}_A + \Delta^o G_{A:B}^{ord} + \frac{1}{4} L_{A,B}^{0,dis} \\ G^o(T) - 0.5 H_A^{o,ref}(298.15 \text{ K}) - 0.5 H_B^{o,ref}(298.15 \text{ K}) &= G(B:A) = \\ & 0.5 \text{GREF}_A + 0.5 \text{GREF}_A + \Delta^o G_{A:B}^{ord} + \frac{1}{4} L_{A,B}^{0,dis} \\ G^o(T) - H_B^{o,ref}(298.15 \text{ K}) &= G(B:B) = \text{GREF}_B \\ L_{A,B:A}^0 &= L_{A:A,B}^0 = -\Delta^o G_{A:B}^{ord} - L_{A,B:A}^{1,ord} + \frac{1}{4} L_{A,B}^{0,dis} + \frac{3}{8} L_{A,B}^{1,dis} + \frac{3}{16} L_{A,B}^{2,dis} \\ L_{A,B:A}^1 &= L_{A:A,B}^1 = L_{A,B:A}^{1,ord} + \frac{1}{8} L_{A,B}^{1,dis} + \frac{4}{16} L_{A,B}^{2,dis} \\ L_{A,B:A}^2 &= L_{A:A,B}^2 = \frac{1}{16} L_{A,B}^{2,dis} \\ L_{A,B:B}^0 &= L_{B:A,B}^0 = -\Delta^o G_{A:B}^{ord} + L_{A,B:B}^{1,ord} + \frac{1}{4} L_{A,B}^{0,dis} - \frac{3}{8} L_{A,B}^{1,dis} + \frac{3}{16} L_{A,B}^{2,dis} \\ L_{A,B:B}^1 &= L_{B:A,B}^1 = L_{A,B:B}^{1,ord} + \frac{1}{4} L_{A,B}^{1,dis} - \frac{4}{8} L_{A,B}^{2,dis} \\ L_{A,B:B}^2 &= L_{B:A,B}^2 = \frac{1}{16} L_{A,B}^{2,dis} \\ L_{A,B:A,B} &= 4L_{A,B:A}^{1,ord} - 4L_{A,B:B}^{1,ord} - \frac{24}{16} L_{A,B}^{2,dis} \end{aligned} \quad (21)$$

where $\Delta^{\circ}G_{A:B}^{ord}$, $L_{A,B:A}^{1,ord}$, $L_{A,B:B}^{1,ord}$ are the independent ordering parameters and $L_{A,B}^{0,dis}$, $L_{A,B}^{1,dis}$, and $L_{A,B}^{2,dis}$ ^[1] are parameters of the disordered state.

In the binary systems Al-Fe, Cu-Mg, Cu-Zn, Fe-Si and Mg-Zn, the equations 21 were used with $L_{A,B:A}^{1,ord}$ and $L_{A,B:B}^{1,ord}$ equal to zero.

In a ternary system A-B-C, the relations 21 stand for each binary system. Moreover, the following constraints have to be fulfilled:

$$\begin{aligned}
 L_{C:A,B}^0 &= L_{A,B:C}^0 &= L_{A,B:C}^{0,ord} + \frac{1}{4} L_{A,B}^{0,dis} - \frac{1}{8} (L_{A,C}^{1,dis} + L_{B,C}^{1,dis}) \\
 &&+ \frac{1/2}{16} (L_{A,C}^{2,dis} + L_{B,C}^{2,dis}) \\
 L_{B:A,C}^0 &= L_{A,C:B}^0 &= L_{A,C:B}^{0,ord} + \frac{1}{4} L_{A,C}^{0,dis} - \frac{1}{8} (L_{A,B}^{1,dis} - L_{B,C}^{1,dis}) \\
 &&+ \frac{1/2}{16} (L_{A,B}^{2,dis} + L_{B,C}^{2,dis}) \\
 L_{A:B,C}^0 &= L_{B,C:A}^0 &= L_{A:B,C}^{0,ord} + \frac{1}{4} L_{B,C}^{0,dis} + \frac{1}{8} (L_{A,B}^{1,dis} + L_{A,C}^{1,dis}) \\
 &&+ \frac{1/2}{16} (L_{A,B}^{2,dis} + L_{A,C}^{2,dis}) \\
 L_{C:A,B}^1 &= L_{A,B:C}^1 &= L_{A,B:C}^{1,ord} + \frac{1}{8} L_{A,B}^{1,dis} \\
 &&- \frac{1/2}{16} (L_{A,C}^{2,dis} - L_{B,C}^{2,dis}) \\
 L_{B:A,C}^1 &= L_{A,C:B}^1 &= L_{A,C:B}^{1,ord} + \frac{1}{8} L_{A,C}^{1,dis} - \frac{1/2}{16} (L_{A,B}^{2,dis} - L_{B,C}^{2,dis}) \\
 L_{A:B,C}^1 &= L_{B,C:A}^1 &= L_{B,C:A}^{1,ord} + \frac{1}{8} L_{B,C}^{1,dis} - \frac{1/2}{16} (L_{A,B}^{2,dis} - L_{A,C}^{2,dis}) \\
 L_{C:A,B}^2 &= L_{A,B:C}^2 &= \frac{1}{16} L_{A,B}^{2,dis} \\
 L_{B:A,C}^2 &= L_{A,C:B}^2 &= \frac{1}{16} L_{A,C}^{2,dis} \\
 L_{A:B,C}^2 &= L_{B,C:A}^2 &= \frac{1}{16} L_{B,C}^{2,dis} \\
 L_{A,B:A,C} &= L_{A,C:A,B} &= -\Delta^{\circ}G_{A:B}^{ord} - \Delta^{\circ}G_{A:C}^{ord} - \Delta^{\circ}G_{B:C}^{ord} - L_{A,B:C}^{0,ord} - L_{A,C:B}^{0,ord} \\
 &&- L_{B,C:A}^{0,ord} + L_{A,B:A}^{1,ord} - L_{A,B:B}^{1,ord} + L_{A,C:A}^{1,ord} - L_{A,C:B}^{1,ord} \\
 &&- \frac{1}{16} (5 L_{A,B}^{2,dis} + 5 L_{A,C}^{2,dis} + 2 L_{B,C}^{2,dis})
 \end{aligned}$$

¹In the tables, the following substitutions were made: $\Delta^{\circ}G_{A:B}^{ord} = G_{A:B;\square}^*$, $\frac{1}{4} L_{A,B}^{0,dis} = L_{A,B}^0$, $\frac{1}{8} L_{A,B}^{1,dis} = L_{A,B}^1$, $\frac{1}{16} L_{A,B}^{2,dis} = L_{A,B}^2$

$$\begin{aligned}
L_{A,B:B,C} &= L_{B,C:A,B} = -\Delta^{\circ}G_{A:B}^{ord} - \Delta^{\circ}G_{A:C}^{ord} - \Delta^{\circ}G_{B:C}^{ord} - L_{A,B:C}^{0,ord} - L_{A,C:B}^{0,ord} \\
&\quad - L_{B,C:A}^{0,ord} + L_{A,B:B}^{1,ord} - L_{A,B:C}^{1,ord} + L_{B,C:A}^{1,ord} - L_{B,C:B}^{1,ord} \\
&\quad - \frac{1}{16} (5 L_{A,B}^{2,dis} + 2 L_{A,C}^{2,dis} + 5 L_{B,C}^{2,dis}) \\
L_{B,C:A,C} &= L_{A,C:B,C} = -\Delta^{\circ}G_{A:B}^{ord} - \Delta^{\circ}G_{A:C}^{ord} - \Delta^{\circ}G_{B:C}^{ord} - L_{A,B:C}^{0,ord} - L_{A,C:B}^{0,ord} \\
&\quad - L_{B,C:A}^{0,ord} + L_{A,C:B}^{1,ord} - L_{A,C:C}^{1,ord} + L_{B,C:A}^{1,ord} - L_{B,C:C}^{1,ord} \\
&\quad - \frac{1}{16} (2 L_{A,B}^{2,dis} + 5 L_{A,C}^{2,dis} + 5 L_{B,C}^{2,dis}) \\
L_{A:A,B,C} &= L_{A,B,C:A} = \frac{1}{32} (3 L_{A,B}^{2,dis} + 3 L_{A,C}^{2,dis}) \\
L_{B:A,B,C} &= L_{A,B,C:B} = \frac{1}{32} (3 L_{A,B}^{2,dis} + 3 L_{B,C}^{2,dis}) \\
L_{C:A,B,C} &= L_{A,B,C:C} = \frac{1}{16} (3/2 L_{A,C}^{2,dis} + 3/2 L_{B,C}^{2,dis}) \\
L_{A,B:A,B,C} &= L_{A,B,C:A,B} = 0 \\
L_{A,C:A,B,C} &= L_{A,B,C:A,C} = 0 \\
L_{B,C:A,B,C} &= L_{A,B,C:B,B} = 0 \\
L_{A,B,C:A,B,C} &= 0
\end{aligned} \tag{22}$$

where $L_{A,B:C}^{0,ord}$, $L_{A,C:B}^{0,ord}$, $L_{B,C:A}^{0,ord}$, $L_{A,B:C}^{1,ord}$, $L_{A,C:B}^{1,ord}$, $L_{B,C:A}^{1,ord}$ are the independent ternary parameters of ordering.

In the ternary system Cu-Mg-Zn, the regular interaction parameters $L_{A,B:C}^{0,ord}$, $L_{A,C:B}^{0,ord}$ and $L_{B,C:A}^{0,ord}$, were taken respectively identical to $-\Delta^{\circ}G_{A:B}^{ord}$, $-\Delta^{\circ}G_{A:C}^{ord}$ and $-\Delta^{\circ}G_{B:C}^{ord}$, and the sub-regular terms $L_{A,B:C}^{1,ord}$, $L_{A,C:B}^{1,ord}$ and $L_{B,C:A}^{1,ord}$ equal to zero like in the corresponding binary systems.

Nevertheless, the use of this sublattice formalism to describe the order – disorder transformation requires the conversion of the parameters of the disordered state into the sublattice model which is cumbersome. A new treatment of the order–disorder transformation was introduced later on by Sundman [91Sun] where G_m is expressed as follows :

$$G_m = G_m^{dis}(x_i) + \Delta G^{ord*}(y_i', y_i'') - \Delta G^{ord*}(x_i, x_i) \tag{23}$$

with

$$G_m^{dis}(x_i) = \sum_i x_i G_i^{dis} + RT \sum_i x_i \ln x_i + x_A x_B \sum_{\nu} L_{A,B}^{\nu,dis} (x_A - x_B)^{\nu} \tag{24}$$

$$\begin{aligned}
\Delta G^{ord*}(y_i, y_i'') &= \sum_i \sum_j y_i y_j'' \Delta^{\circ}G_{i;j}^{ord*} + RT \left(a \sum_i y_i \ln y_i + b \sum_i y_i'' \ln y_i'' \right) \\
&+ y_A y_B' \sum_i y_i'' L_{A,B;i}^{0,ord*} + y_A y_B' (y_A - y_B') \sum_i y_i'' L_{A,B;i}^{1,ord*} \\
&+ y_A'' y_B'' \sum_i y_i L_{i;A,B}^{0,ord*} + y_A'' y_B'' (y_A'' - y_B'') \sum_i y_i L_{i;A,B}^{1,ord*} \\
&+ y_A' y_B' y_A'' y_B'' L_{A,B;A,B}^{ord*} \quad (25)
\end{aligned}$$

$$\begin{aligned}
\Delta G^{ord*}(x_i, x_i) &= \sum_i \sum_j x_i x_j \Delta^{\circ}G_{i;j}^{ord*} + RT \left(a \sum_i x_i \ln x_i + b \sum_i x_i \ln x_i \right) \\
&+ x_A x_B \sum_i x_i L_{A,B;i}^{0,ord*} + x_A x_B (x_A - x_B) \sum_i x_i L_{A,B;i}^{1,ord*} \\
&+ x_A x_B \sum_i x_i L_{i;A,B}^{0,ord*} + x_A x_B (x_A - x_B) \sum_i x_i L_{i;A,B}^{1,ord*} \\
&+ x_A x_B x_A x_B L_{A,B;A,B}^{ord*} \quad (26)
\end{aligned}$$

Hence, the disordered and ordered phases can be treated separately. The parameters of the disordered phase, $L_{A,B}^{dis}$, and those describing the ordering $\Delta^{\circ}G_{A;B}^{ord*}$, $L_{A,B;i}^{\nu,ord*}$, $L_{i;A,B}^{\nu,ord*}$ and $L_{A,B;A,B}^{ord*}$ are introduced as usual thermodynamic parameters of the sublattice model and a special command then allows their combination to define the expression of the order-disorder sublattice following equation 23.

Constraints must still be introduced between the thermodynamic parameters of the function $\Delta G(y_i, y_i'')$ to ensure stability of the disordered state. But the value zero for the ordering energy is now built in. This allows to simplify the expression of the constraints linking the ordering parameters.

The ternary systems Al-Ti-(Mo,Nb,Ta,W) were assessed with equation 23 assuming

$$\begin{aligned}
\Delta^{\circ}G_{i;j}^{ord*} = \Delta^{\circ}G_{j;i}^{ord*} &= -L_{i;j;i}^{0,ord*} = -L_{i;j;j}^{0,ord*} = -L_{i;j;k}^{0,ord*} \\
&= -L_{i;i,j}^{0,ord*} = -L_{j;i,j}^{0,ord*} = -L_{k;i,j}^{0,ord*} = \alpha_{ij} \quad (27)
\end{aligned}$$

These relations are identical to 21 and 22 when disordered parameters are not considered and sub-regular ordering terms are zero. The use of equation 23 allows a simpler but mathematically equivalent description with only two ordering parameters:

$$\Delta^{\circ}G_{i;j}^{ord*} = \Delta^{\circ}G_{j;i}^{ord*} = 2\alpha_{ij} \quad (28)$$

When such simplification is possible, the two descriptions (the original using equations 27 and the modified using equations 28) are presented in this report.

For sake of uniformity, the descriptions using the sublattice model with the constraints 21 and 22 were also converted for use of equation 23 in the simpler way possible .

Only the parameters derived from the simpler description are in the database. In this report, they are presented in a frame. An example is shown hereunder for a binary system.

Phase bcc-B2

$$G^\circ(T) - H_A^{\circ,\text{ref}}(298.15 \text{ K}) = G(\text{A:A}) = 0.0$$

$$G^\circ(T) - 0.5 H_A^{\circ,\text{ref}}(298.15 \text{ K}) - 0.5 H_B^{\circ,\text{ref}}(298.15 \text{ K}) = G(\text{A:B}) = 2.0 G_{\text{A:B}}^{\text{ord}}$$

$$G^\circ(T) - 0.5 H_A^{\circ,\text{ref}}(298.15 \text{ K}) - 0.5 H_B^{\circ,\text{ref}}(298.15 \text{ K}) = G(\text{B:A}) = 2.0 G_{\text{A:B}}^{\text{ord}}$$

$$G^\circ(T) - H_B^{\circ,\text{ref}}(298.15 \text{ K}) = G(\text{B:B}) = 0.0$$

Phase bcc-A2

$$G^\circ(T) - H_A^{\circ,\text{ref}}(298.15 \text{ K}) = \text{GREF}_A$$

$$G^\circ(T) - H_B^{\circ,\text{ref}}(298.15 \text{ K}) = \text{GREF}_B$$

$$L_{\text{A,B};\square}^{0,\text{dis}} = 4 L_{\text{A,B}}^0$$

$$L_{\text{A,B};\square}^{1,\text{dis}} = 8 L_{\text{A,B}}^1$$

$$L_{\text{A,B};\square}^{2,\text{dis}} = 16 L_{\text{A,B}}^2$$

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BINARY SYSTEMS

System Al–B

Solution Phases:

Liquid, fcc-Al

Compounds:

AlB₂, AlB₁₂-L, AlB₁₂-H

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-Al	:	Substitutional, Redlich-Kister
AlB ₂	:	Stoichiometric, (Al)(B) ₂
AlB ₁₂ -L	:	Stoichiometric, (Al)(B) ₁₂
AlB ₁₂ -H	:	Stoichiometric, (Al)(B) ₁₂

Assessor and Date:

H.L. Lukas 1992

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlB₂

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 2.0 H_{\text{B}}^{\circ, \beta\text{-rhombo-B}}(298.15 \text{ K}) = -85808.76 + 45.46923 T + \text{GHSER}_{\text{Al}} + 2.0 \text{GHSER}_{\text{B}}$$

Phase AlB₁₂-L

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 12.0 H_{\text{B}}^{\circ, \beta\text{-rhombo-B}}(298.15 \text{ K}) = -198290.69 + 33.68638 T + \text{GHSER}_{\text{Al}} + 12.0 \text{GHSER}_{\text{B}}$$

Phase AlB₁₂-H

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 12.0 H_{\text{B}}^{\circ, \beta\text{-rhombo-B}}(298.15 \text{ K}) = -75292.23 - 33.66376 T + \text{GHSER}_{\text{Al}} + 12.0 \text{GHSER}_{\text{B}}$$

Phase fcc-Al

$$L_{\text{Al,B};\square}^{\circ, \text{fcc-Al}} = 12242.44 - 1.74891 T$$

Phase liquid

$$L_{Al,B}^{0,liquid} = -12671.16 + 1.81016 T$$

$$L_{Al,B}^{1,liquid} = 31988.28$$

$$L_{Al,B}^{2,liquid} = -15873.74$$

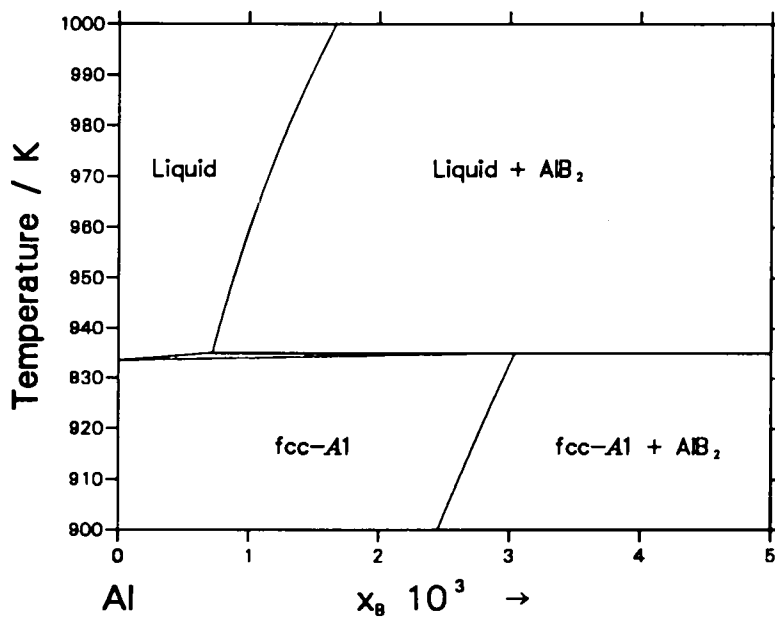
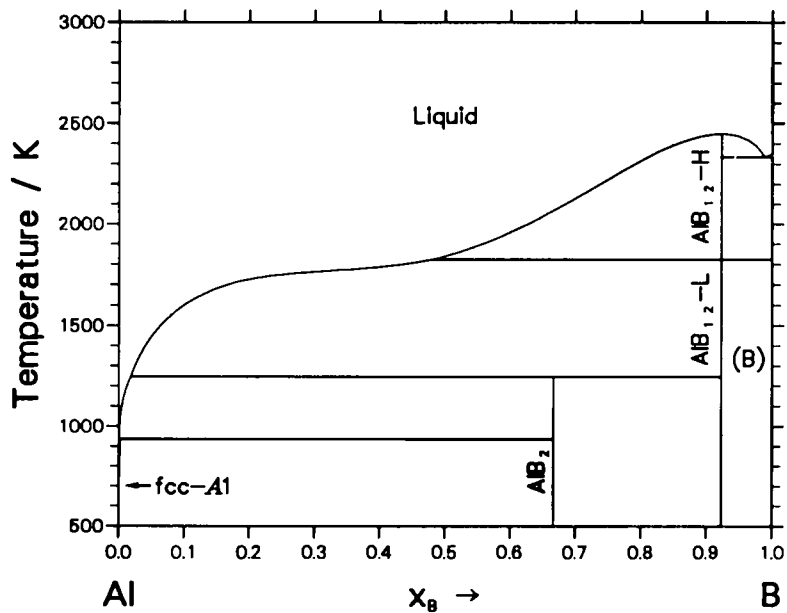


Table I - Invariant Reactions.

Reaction	Type	Compositions x_B	T / K
Liquid + AlB ₂ \rightleftharpoons fcc-Al	Peritectic	.003 .667 .0007	935.0
Liquid + AlB ₁₂ -L \rightleftharpoons AlB ₂	Peritectic	.019 .923 .667	1245.8
AlB ₁₂ -L \rightleftharpoons AlB ₁₂ -H	Polymorphic	.923 .923	1826.2
Liquid \rightleftharpoons AlB ₁₂ -H + β -rhombo-B	Eutectic	.988 .923 1.000	2336.0
AlB ₁₂ -H \rightleftharpoons Liquid	Congruent	.923 .923	2448.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-B	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	(B)	β -rhombo-B			
	AlB ₁₀	AlB ₁₀	<i>oC88</i> <i>Cmcm</i>		not assessed
	AlB ₁₂ -L	AlB ₁₂	<i>oP384</i> <i>P2₁2₁2₁</i>		AlB ₁₂ - α in [90Mas]
	AlB ₁₂ -H	AlB ₁₂	<i>tP216</i> <i>P4₁2₁2</i>		AlB ₁₂ - β in [90Mas]
	AlB ₂	AlB ₂	<i>hP3</i> <i>P6/mmm</i>	Al 1 B 2	

System Al–C

Solution Phases:

Liquid, fcc-Al

Compound:

Al₄C₃

Modelling:

Liquid : Substitutional, Redlich–Kister
 fcc-Al : Sublattice model , (Al)(C,□)
 Al₄C₃ : Stoichiometric, (Al)₄(C)₃

Assessor and Date:

J. Gröbner, H. L. Lukas, and F. Aldinger.

Publication:

Calphad, **20**, 2 (1996) 247-254.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₄C₃

$$G^{\circ}(T) - 4.0 H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 3.0 H_{\text{C}}^{\circ, \text{graphite}}(298.15 \text{ K}) = \\ - 286002.0 + 1030.273 T - 161.709142 T \cdot \ln T - 0.011523 T^2 \\ + 2450000 T^{-1} + 7\text{E-}07 T^3$$

Phase fcc-Al

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - H_{\text{C}}^{\circ, \text{graphite}}(298.15 \text{ K}) = \\ 80 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{C}}$$

$$L_{\text{Al:C,}\square}^{\circ, \text{fcc-Al}} = 80 T$$

Phase graphite

$$L_{\text{Al,C}}^{\circ, \text{graphite}} = 80 T$$

Phase liquid

$$L_{\text{Al,C}}^{\circ, \text{liquid}} = 40861.02 - 33.21138 T$$

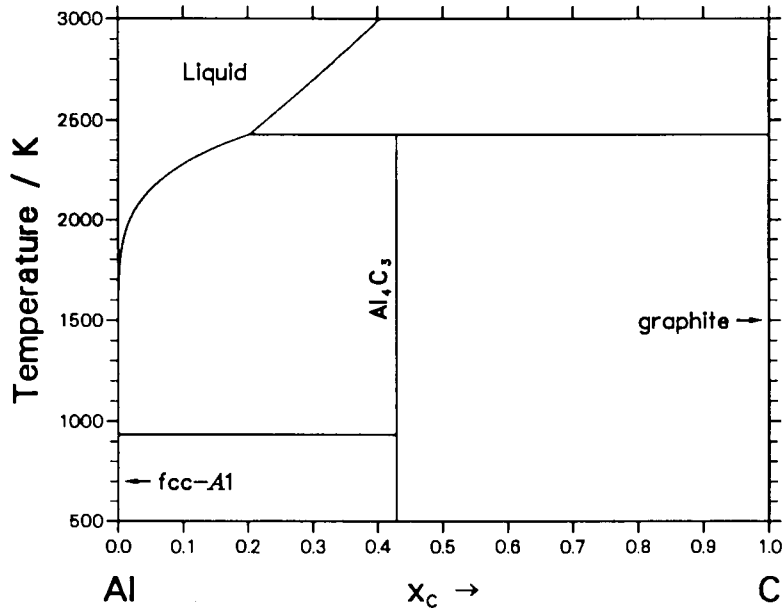


Table I - Invariant Reactions.

Reaction	Type	Compositions x_C	T / K
Liquid + graphite \rightleftharpoons Al_4C_3	Peritectic	.198 1.000 .429	2429.0
Liquid \rightleftharpoons fcc-Al + Al_4C_3	Degenerate	.000 .000 .429	933.5

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-C	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4
	(C)	graphite		
	Al_4C_3	Al_4C_3	$hR7$ $R\bar{3}m$	Al ₁ 2 Al ₂ 2 C ₁ 1 C ₂ 2

System Al–Ce

Solution Phases:

Liquid, bcc-A2, fcc-Al

Compounds:

Al₁₁Ce₃, Al₃Ce, AlCe, AlCe₂, Al₂Ce

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc-A2	:	Substitutional, Redlich–Kister
fcc-Al	:	Substitutional, Redlich–Kister
Al ₁₁ Ce ₃	:	Stoichiometric, (Al) ₁₁ (Ce) ₃
Al ₃ Ce	:	Stoichiometric, (Al) ₃ (Ce)
Al ₂ Ce	:	Stoichiometric, (Al) ₂ (Ce)
AlCe	:	Stoichiometric, (Al)(Ce)
AlCe ₂	:	Stoichiometric, (Al)(Ce) ₂

Assessor and Date:

G. Cacciamani, G. Borzone, R. Ferro

Publication:

revised 1997

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₁₁Ce₃

$$G^{\circ}(T) - 11.0 H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 3.0 H_{\text{Ce}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) = \\ - 574000 + 179.3087 T + 11.0 \text{ GHSE}_{\text{Al}} + 3.0 \text{ GIISER}_{\text{Ce}}$$

Phase Al₃Ce

$$G^{\circ}(T) - 3.0 H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - H_{\text{Ce}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) = \\ - 176000 + 54.97964 T + 3.0 \text{ GHSE}_{\text{Al}} + \text{GIISER}_{\text{Ce}}$$

Phase AlCe

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - H_{\text{Ce}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) = \\ - 92000 + 33.90118 T + \text{GHSE}_{\text{Al}} + \text{GHSE}_{\text{Ce}}$$

Phase AlCe_3

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc}-\text{Al}}(298.15 \text{ K}) - 3.0 H_{\text{Ce}}^{\circ, \text{fcc}-\text{Al}}(298.15 \text{ K}) = -108000 + 41.3726 T + \text{GHISER}_{\text{Al}} + 3.0 \text{GHISER}_{\text{Ce}}$$

Phase Laves-C15

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc}-\text{Al}}(298.15 \text{ K}) - H_{\text{Ce}}^{\circ, \text{fcc}-\text{Al}}(298.15 \text{ K}) = -150000.0 + 45.66405 T + 2.0 \text{GHISER}_{\text{Al}} + \text{GHISER}_{\text{Ce}}$$

Phase bcc-A2

$$L_{\text{Al,Ce};\square}^{0, \text{bcc}-\text{A}2} = 80 T$$

Phase fcc-A1

$$L_{\text{Al,Ce};\square}^{0, \text{fcc}-\text{A}1} = 80 T$$

Phase Liquid

$$L_{\text{Al,Ce}}^{0, \text{liquid}} = -167593.1 + 84.87628 T$$

$$L_{\text{Al,Ce}}^{1, \text{liquid}} = -36060 + 5.89346 T$$

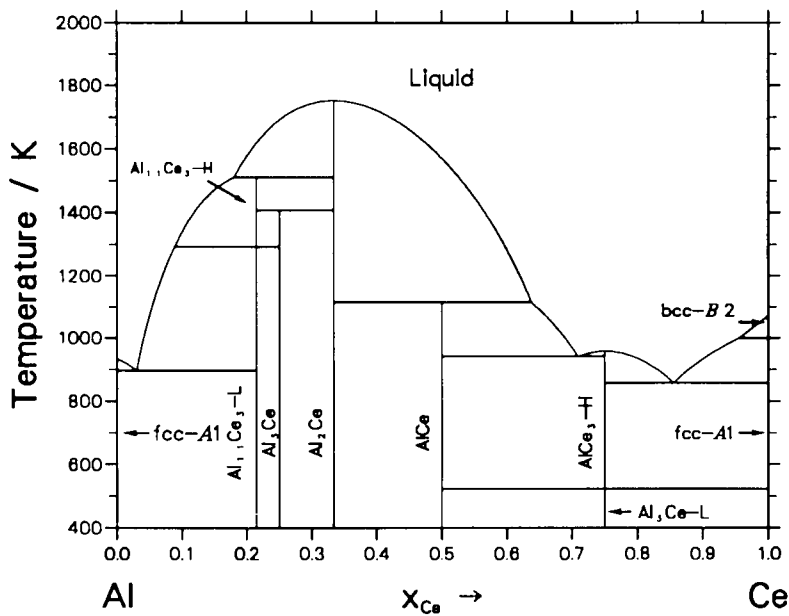


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Ce}			T / K
Liquid \rightleftharpoons fcc-Al + Al ₁₁ Ce ₃	Eutectic	.028	.000	.214	902.6
Liquid + Laves-C15* \rightleftharpoons Al ₁₁ Ce ₃	Peritectic	.179	.333	.214	1497.1
Liquid + Laves-C15* \rightleftharpoons AlCe	Peritectic	.619	.333	.500	1116.9
Liquid \rightleftharpoons AlCe + AlCe ₃	Eutectic	.704	.500	.750	911.3
Liquid \rightleftharpoons AlCe ₃ + fcc-Al	Eutectic	.854	.750	1.000	852.2
Liquid \rightleftharpoons bcc-A2 + fcc-Al	Polymorphic	.956	1.000	1.000	1000.0
Al ₁₁ Ce ₃ + Laves-C15* \rightleftharpoons Al ₃ Ce	Peritectoid	.214	.333	.250	1408.0
Laves-C15* \rightleftharpoons Liquid	Congruent	.333	.333	1752.0

* Laves-C15 \equiv Al₂Ce

Table II - Crystal Structure and Phase Description.

System	Phase	Structural Type	Pearson Symbol Space Group	Sub-lattices	Comments	
Al-Ce	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	polymorphic trans. not considered	
	(Ce)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4		
	(Ce)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2		
	Al ₁₁ Ce ₃ - α	Al ₁₁ La ₃	<i>Immm</i> <i>oI28</i>			
	Al ₁₁ Ce ₃ - β	Al ₄ Ba	<i>I₄/mmm</i> U10			
	Al ₃ Ce	Ni ₃ Sn	<i>hP8</i> <i>P6₃/mmc</i>			
	Al ₂ Ce	Cu ₂ Mg	<i>cF24</i> <i>Fd$\bar{3}m$</i>	Ce 8 Al 16		
	AlCe	AlCe	<i>oC16</i> <i>Cmcm</i>	Al ₁ 4 Al ₂ 4 Ce 8		
	AlCe ₃ - α	Ni ₃ Sn	<i>hP8</i> <i>P6₃/mmc</i>	Al 2 Ce 6		polymorphic trans. not considered
	AlCe ₃ - β	AlCu ₃	<i>cP4</i> <i>Pm$\bar{3}m$</i>	Al 1 Ce 3		

System Al-Cr

Solution Phases:

Liquid, bcc-A2, fcc-A1

Compounds:

AlCr₂, Al₄Cr, Al₈Cr₅-L, Al₈Cr₅-H, Al₉Cr₄-L,
Al₉Cr₄-H, Al₁₁Cr₂, Al₁₃Cr₂

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
AlCr ₂	:	Stoichiometric, (Al)(Cr) ₄
Al ₄ Cr	:	Stoichiometric, (Al) ₄ (Cr)
Al ₈ Cr ₅ -L	:	Stoichiometric, (Al) ₈ (Cr) ₅ -L
Al ₈ Cr ₅ -H	:	Stoichiometric, (Al) ₈ (Cr) ₅ -H
Al ₉ Cr ₄ -L	:	Stoichiometric, (Al) ₉ (Cr) ₄ -L
Al ₉ Cr ₄ -H	:	Stoichiometric, (Al) ₉ (Cr) ₄ -H
Al ₁₁ Cr ₂	:	Stoichiometric, (Al) ₁₁ (Cr) ₂
Al ₁₃ Cr ₂	:	Stoichiometric, (Al) ₁₃ (Cr) ₂

Assessor and Date:

N. Saunders, 1991

Publication:

based on the publication of N. Saunders and V.G. Rivlin
in Z. für Metallkde, 78, (11) 795-801 (1987).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlCr₂

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = \\ - 32700.0 - 8.79 T + \text{GHSE}_{\text{Al}} + 2.0 \text{GHSE}_{\text{Cr}}$$

Phase Al₄Cr

$$G^{\circ}(T) - 4.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = \\ - 89025.0 + 19.05 T + 4.0 \text{GHSE}_{\text{Al}} + \text{GHSE}_{\text{Cr}}$$

Phase Al₈Cr₅-L

$$G^\circ(T) - 8.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 5.0 H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) = \\ - 229515.0 + 8.0 \text{ GHSER}_{\text{Al}} + 5.0 \text{ GHSER}_{\text{Cr}}$$

Phase Al₈Cr₅-H

$$G^\circ(T) - 8.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 5.0 H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) = \\ - 147732.0 - 58.5 T + 8.0 \text{ GHSER}_{\text{Al}} + 5.0 \text{ GHSER}_{\text{Cr}}$$

Phase Al₉Cr₄-L

$$G^\circ(T) - 9.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 4.0 H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) = \\ - 230750.0 + 16.094 T + 9.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Cr}}$$

Phase Al₉Cr₄ - H

$$G^\circ(T) - 9.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 4.0 H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) = \\ - 134433.0 - 56.16 T + 9.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Cr}}$$

Phase Al₁₁Cr₂

$$G^\circ(T) - 11.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 2.0 H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) = \\ - 175500.0 + 25.805 T + 11.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Cr}}$$

Phase Al₁₃Cr₂

$$G^\circ(T) - 13.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 2.0 H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) = \\ - 174405.0 + 22.2 T + 13.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Cr}}$$

Phase bcc-A2

$$L_{\text{Al,Cr};\square}^{0,\text{bcc}-\text{A2}} = - 54900 + 10 T$$

Phase fcc-A1

$$L_{\text{Al,Cr};\square}^{0,\text{fcc}-\text{A1}} = - 45900 + 6.0 T$$

Phase liquid

$$L_{\text{Al,Cr}}^{0,\text{liquid}} = - 29000.0$$

$$L_{\text{Al,Cr}}^{1,\text{liquid}} = - 11000.0$$

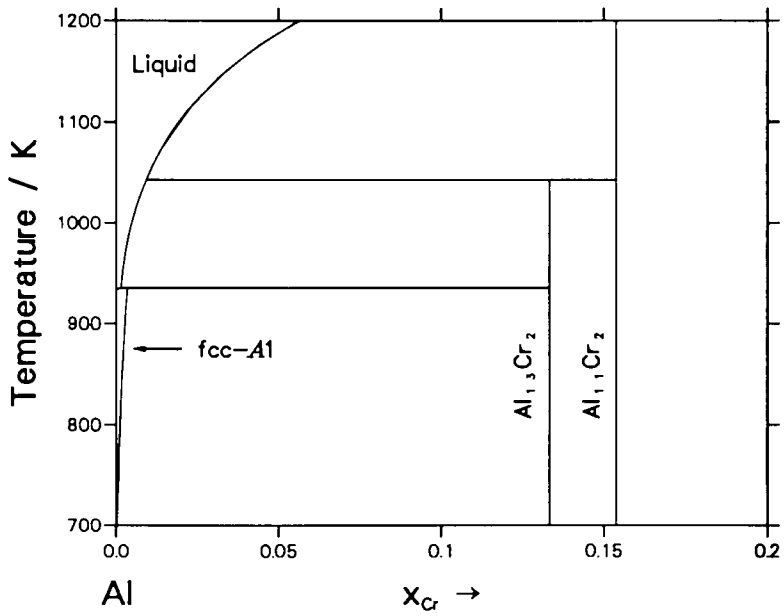
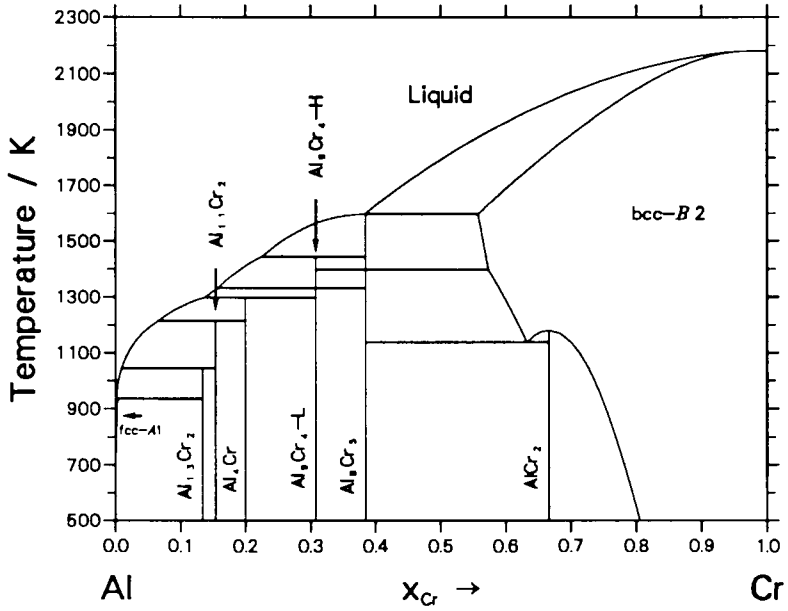


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Cr}			T / K
Liquid + Al ₁₃ Cr ₂ \rightleftharpoons fcc-A1	Peritectic	.002	.133	.003	934.8
Liquid + Al ₁₁ Cr ₂ \rightleftharpoons Al ₁₃ Cr ₂	Peritectic	.009	.154	.133	1042.9
Liquid + Al ₄ Cr \rightleftharpoons Al ₁₁ Cr ₂	Peritectic	.066	.200	.154	1214.6
Liquid + Al ₉ Cr ₄ -L \rightleftharpoons Al ₄ Cr	Peritectic	.137	.308	.200	1298.1
Al ₉ Cr ₄ -H \rightleftharpoons Al ₉ Cr ₄ -L	Polymorphic	.158	.158	...	1333.0
Liquid + Al ₈ Cr ₅ -H \rightleftharpoons Al ₉ Cr ₄ -H	Peritectic	.225	.385	.307	1443.1
Liquid \rightleftharpoons Al ₈ Cr ₅ -H + bcc-A2	Eutectic	.385	.383	.558	1597.0
Al ₈ Cr ₅ -H \rightleftharpoons Al ₈ Cr ₅ -L	Polymorphic	.385	.385	...	1398.0
bcc-A2 \rightleftharpoons Al ₈ Cr ₅ -L + AlCr ₂	Eutectoid	.633	.385	.667	1139.3
AlCr ₂ \rightleftharpoons bcc-A2	Congruent	.667	.667	...	1181.0

Table II:a - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Cr	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Cr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	AlCr ₂	MoSi ₂	<i>tI6</i> <i>I4/mmm</i>	Al 2 Cr 4	
	Al ₄ Cr	Al ₄ Cr	<i>mP180</i> <i>P2/m</i>		
	Al ₁₁ Cr ₂	Al ₅ Cr	<i>mP48</i> <i>P2</i>		also designated by Al ₅ Cr in [90Mas]
	Al ₈ Cr ₅ -L	Al ₈ Cr ₅	<i>hR26</i> <i>R$\bar{3}m$</i>		
	Al ₈ Cr ₅ -H	Al ₈ Cr ₅	<i>hR26</i>		indicated in [90Mas]
	Al ₉ Cr ₄ -L		<i>cI52</i> <i>I$\bar{4}3m$</i>		
	Al ₉ Cr ₄ -H				indicated in [90Mas]

Table II:b - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
	$\text{Al}_{13}\text{Cr}_2\text{-}\beta$	Al_{45}V_7	<i>mC104</i> <i>C2/m</i>	Al_1 2 Al_2 4 Al_3 4 Al_4 4 Al_5 4 Al_6 4 Al_7 4 Al_8 4 Al_9 4 Al_{10} 8 Al_{11} 8 Al_{12} 8 Al_{13} 8 Al_{14} 8 Al_{15} 4 Al_{16} 4 Cr_1 2 Cr_2 4 Cr_3 8	also designated by by Al_7Cr in [90Mas]

System Al–Cu

Solution Phases:

(stable) Liquid, bcc-*A2*, fcc-*A1*
 (metastable) hcp-*A3*

Compounds:

(stable) AlCu- δ , AlCu- ϵ , AlCu- η , AlCu- θ , AlCu- γ (*D8₃*)
 AlCu- γ (H), AlCu- ζ
 (metastable) Laves-*C14*, Laves-*C15*, Laves-*C36*

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-*A2* : Substitutional, Redlich-Kister
 fcc-*A1* : Substitutional, Redlich-Kister
 hcp-*A3* : Substitutional, Redlich-Kister
 AlCu- δ : Sublattice model, (Al,Cu)₂(Cu)₃
 AlCu- ϵ : Sublattice model, (Al,Cu)(Cu)
 AlCu- η : Sublattice model, (Al,Cu)(Cu)
 AlCu- θ : Sublattice model, (Al)(Al,Cu)₂
 AlCu- γ (*D8₃*) : Sublattice model, (Al)₄(Al,Cu)(Cu)₈
 AlCu- γ (H) : Sublattice model, (Al)₄(Al,Cu)(Cu)₈
 AlCu- ζ : Stoichiometric, (Al)₉(Cu)₁₁
 Laves-*C14* : Sublattice model, (Al,Cu)₂(Al,Cu)
 Laves-*C15* : Sublattice model, (Al,Cu)₂(Al,Cu)
 Laves-*C36* : Sublattice model, (Al,Cu)₂(Al,Cu)

Assessor and Date:

N. Saunders, 1991
 Data relative to the Laves phases evaluated in Round II.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase AlCu- δ**

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = \\ - 106700.0 + 3.0 T + 2.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Cu}}$$

Phase AlCu- ϵ

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ - 36976 + 1.2 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 2.0 \text{ GBCC}_{\text{Cu}}$$

$$L_{\text{Al,Cu:Cu}}^{0,\text{AlCu}-\epsilon} = 7600 - 24 T$$

$$L_{\text{Al,Cu:Cu}}^{1,\text{AlCu}-\epsilon} = - 72000$$

Phase AlCu- η

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ - 40560.0 + 3.14 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 2.0 \text{ GBCC}_{\text{Cu}}$$

$$L_{\text{Al,Cu:Cu}}^{0,\text{AlCu}-\eta} = - 25740 - 20 T$$

Phase AlCu- θ

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = G(\text{Al:Al}) = 3.0 \text{ GBCC}_{\text{Al}}$$

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ - 47406.0 + 6.75 T + 2.0 \text{ GHSER}_{\text{Al}} + 1.0 \text{ GHSER}_{\text{Cu}}$$

$$L_{\text{Al:Al:Cu}}^{0,\text{AlCu}-\theta} = 2211$$

Phase AlCu- ζ

$$G^\circ(T) - 9.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 11.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = \\ - 420000.0 + 18.0 T + 9.0 \text{ GHSER}_{\text{Al}} + 11.0 \text{ GHSER}_{\text{Cu}}$$

Phase AlCu- $\gamma(D8_3)$

$$G^\circ(T) - 5.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 8.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = G(\text{Al:Al:Cu}) = \\ - 300716.0 + 390.0 T - 52 T \cdot \ln T + 5.0 \text{ GHSER}_{\text{Al}} \\ + 8.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 9.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) = G(\text{Al:Cu:Cu}) = \\ - 280501.0 + 379.6 T - 52 T \cdot \ln T + 4.0 \text{ GHSER}_{\text{Al}} \\ + 9.0 \text{ GHSER}_{\text{Cu}}$$

Phase AlCu- γ (H)

$$G^\circ(T) - 5.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - 8.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Al}:\text{Al}:\text{Cu}) =$$

$$- 219258.0 - 45.5 T + 5.0 \text{ GHSER}_{\text{Al}} + 8.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - 9.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Al}:\text{Cu}:\text{Cu}) =$$

$$- 200460.0 - 58.5 T + 4.0 \text{ GHSER}_{\text{Al}} + 9.0 \text{ GHSER}_{\text{Cu}}$$

Phase Laves-C14

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Al}:\text{Al}) =$$

$$15000.0 + 3.0 \text{ GHSER}_{\text{Al}}$$

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Al}:\text{Cu}) =$$

$$15000.0 + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Cu}:\text{Al}) =$$

$$15000.0 + \text{GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Cu}:\text{Cu}) =$$

$$15000.0 + 3.0 \text{ GHSER}_{\text{Cu}}$$

$$L_{\text{Al,Cu:Al}}^{0,\text{Laves-C14}} = - 24000 + 2.44 T$$

$$L_{\text{Al,Cu:Cu}}^{0,\text{Laves-C14}} = - 24000 + 2.44 T$$

Phase Laves-C15

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Al}:\text{Al}) =$$

$$15000.0 + 3.0 \text{ GHSER}_{\text{Al}}$$

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Al}:\text{Cu}) =$$

$$15000.0 + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Cu}:\text{Al}) =$$

$$15000.0 + \text{GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Cu}:\text{Cu}) =$$

$$15000.0 + 3.0 \text{ GHSER}_{\text{Cu}}$$

$$L_{\text{Al,Cu:Al}}^{0,\text{Laves-C15}} = - 105000 - 1.615 T$$

$$L_{\text{Al,Cu:Cu}}^{0,\text{Laves-C15}} = - 105000 - 1.615 T$$

Phase Laves-C36

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Al}:\text{Al}) =$$

$$15000.0 + 3.0 \text{ GHSER}_{\text{Al}}$$

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Al}:\text{Cu}) =$$

$$15000.0 + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}}$$

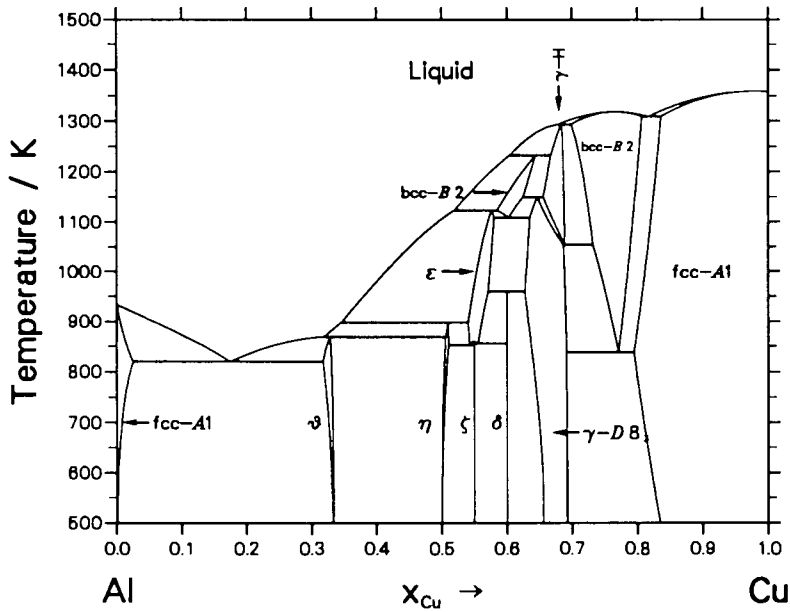
$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Cu}:\text{Al}) =$$

$$15000.0 + \text{GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = G(\text{Cu}:\text{Cu}) =$$

$$L_{Al,Cu:Al}^{0,Laves-C36} = 15000.0 + 3.0 \text{ GHSER}_{Cu} - 126169 + 14.61 T$$

$$L_{Al,Cu:Cu}^{0,Laves-C36} = -126169 + 14.61 T$$



Phase bcc-A2

$$L_{Al,Cu:\square}^{0,bcc-A2} = -73554 + 4.0 T$$

$$L_{Al,Cu:\square}^{1,bcc-A2} = 51500 - 11.84 T$$

Phase fcc-A1

$$L_{Al,Cu:\square}^{0,fcc-A1} = -53520 + 2 T$$

$$L_{Al,Cu:\square}^{1,fcc-A1} = 38590 - 2 T$$

$$L_{Al,Cu:\square}^{2,fcc-A1} = 1170$$

Phase liquid

$$L_{\text{Al,Cu}}^{0,\text{liquid}} = -66622 + 8.1 T$$

$$L_{\text{Al,Cu}}^{1,\text{liquid}} = 46800 - 90.8 T + 10 T \cdot \ln T$$

$$L_{\text{Al,Cu}}^{2,\text{liquid}} = -2812$$

Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Cu}	T / K
Liquid \rightleftharpoons fcc-A1 + AlCu- θ	Eutectic	.175 .025 .318	820.7
Liquid + AlCu- η \rightleftharpoons AlCu- θ	Peritectic	.319 .506 .329	869.0
Liquid + AlCu- ϵ \rightleftharpoons AlCu- η	Peritectic	.345 .541 .510	898.0
Liquid + bcc-A2 \rightleftharpoons AlCu- ϵ	Peritectic	.519 .585 .576	1124.0
Liquid + AlCu- γ (H) \rightleftharpoons bcc-A2	Peritectic	.604 .667 .644	1232.4
Liquid + bcc-A2 \rightleftharpoons AlCu- γ (H)	Peritectic	.678 .698 .684	1293.4
Liquid \rightleftharpoons bcc-A2 + fcc-A1	Eutectic	.817 .807 .837	1309.3
bcc-A2 \rightleftharpoons AlCu- γ (D8 ₃) + fcc-A1	Eutectoid	.771 .691 .795	837.9
AlCu- γ (H) \rightleftharpoons AlCu- γ (D8 ₃) + bcc-A2	Eutectoid	.688 .686 .732	1054.2
bcc-A2 + AlCu- γ (H) \rightleftharpoons AlCu- γ (D8 ₃)	Peritectoid	.625 .656 .647	1150.5
bcc-A2 \rightleftharpoons AlCu- ϵ + AlCu- γ (D8 ₃)	Eutectoid	.602 .580 .635	1109.3
AlCu- ϵ + AlCu- γ (D8 ₃) \rightleftharpoons AlCu- δ	Peritectoid	.572 .628 .600	959.7
AlCu- ϵ \rightleftharpoons AlCu- ζ + AlCu- δ	Eutectoid	.555 .550 .600	855.8
AlCu- ϵ \rightleftharpoons AlCu- η + AlCu- ζ	Eutectoid	.543 .511 .550	852.4
AlCu- ζ \rightleftharpoons AlCu- ϵ	Congruent	.550 .550 ...	861.0

Table II:a – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Cu	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Cu)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	β	W	$cI2$ $Im\bar{3}m$	M 2	
	β_0				

Table II:b – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
	AlCu- δ	 <i>R3m</i>		
	AlCu- η_1		<i>Pbn</i> or <i>Cmmm</i> <i>oP16</i> or <i>oC16</i>		high <i>T</i> phase
	AlCu- η_2	AlCu	<i>mC20</i> <i>C2/m</i>		low <i>T</i> phase
	AlCu- θ	Al ₂ Cu	<i>tI12</i> <i>I4/mcm</i>	Al 8 Cu 4	
	AlCu- δ <i>R3m</i>		
	AlCu- ϵ_1	NiAs	<i>hP4</i> <i>P6₃/mmc</i>		low <i>T</i> phase
	AlCu- ϵ_2		not considered
	AlCu- $\gamma(D8_3)$	Al ₄ Cu ₉	<i>cP52</i> <i>P43m</i>	Al ₁ 4 Al ₂ 12 Cu ₁ 4 Cu ₂ 4 Cu ₃ 4 Cu ₄ 6 Cu ₅ 6 Cu ₆ 12	
	AlCu- $\gamma(II)$		
	AlCu- ζ_1	<i>hP42</i> <i>C2/m</i>		ζ_1
	AlCu- ζ_2			ζ_2 not considered

System Al-Fe

Solution Phases:

(stable)	:	Liquid, fcc-A1, bcc-A2, bcc-B2, Al ₅ Fe ₄
(metastable)	:	cbcc-A12, cub-A13, hcp-A3

Compounds:

stable	:	Al ₂ Fe, Al ₅ Fe ₂ , Al ₁₃ Fe ₄ ,
metastable	:	Al ₁₁ Mn ₄ , Al ₁₂ Mn, Al ₆ Mn

Modelling:

Liquid	:	Substitutional, Redlich-Kister
cbcc-A12	:	Substitutional, Redlich-Kister
cub-A13	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
bcc-A2	:	see below
bcc-B2	:	Sublattice model, (Al,Fe) _{0.5} (Al,Fe) _{0.5} (□) ₃ Two descriptions of the bcc-A2: bcc-B2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
Al ₅ Fe ₄	:	Substitutional, Redlich-Kister
Al ₁₃ Fe ₄	:	Sublattice model, (Al) _{0.6275} (Fe) _{0.235} (Al,□) _{0.1375}
Al ₂ Fe	:	Stoichiometric, (Al) ₂ (Fe)
Al ₅ Fe ₂	:	Stoichiometric, (Al) ₅ (Fe) ₂
Al ₁₁ Mn ₄	:	Stoichiometric, (Al) ₁₁ (Mn) ₄
Al ₁₂ Mn	:	Stoichiometric, (Al) ₁₂ (Mn)
Al ₆ Mn	:	Stoichiometric, (Al) ₆ (Mn)

Assessor and Date:

M. Seierstein, 1991

Comments:

Al₁₁Mn₄, Al₁₂Mn and Al₆Mn and the hcp-A3 phase have been evaluated by Å. Jansson and T.G. Chart (1995) in the assessment of the Al-Fe-Mn system.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase fcc-A1**

$$L_{\text{Al,Fe};\square}^{0,\text{fcc-A1}} = -76066.1 + 18.6758 T$$

$$L_{\text{Al,Fe};\square}^{1,\text{fcc-A1}} = 21167.4 + 1.3398 T$$

Phase hcp-A3

$$L_{\text{Al,Fe};\square}^{0,\text{hcp-A3}} = -106903.0 + 20.0 T$$

Phase liquid

$$L_{\text{Al,Fe}}^{0,\text{liquid}} = -91976.5 + 22.1314 T$$

$$L_{\text{Al,Fe}}^{1,\text{liquid}} = -5672.58 + 4.8728 T$$

$$L_{\text{Al,Fe}}^{2,\text{liquid}} = 121.9$$

Phase Al₂Fe

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Fe}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ -98097.0 + 18.7503 T + 2.0 \text{ GHSE}_{\text{Al}} + \text{GHSE}_{\text{Fe}}$$

Phase Al₁₃Fe₄

$$G^\circ(T) - 0.765 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.235 H_{\text{Fe}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ G(\text{Al:Fe:Al}) = -30714.4 + 7.44 T + 0.765 \text{ GHSE}_{\text{Al}} + 0.235 \text{ GHSE}_{\text{Fe}}$$

$$G^\circ(T) - 0.6275 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.235 H_{\text{Fe}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ G(\text{Al:Fe};\square) = -27781.3 + 7.2566 T + 0.6275 \text{ GHSE}_{\text{Al}} + 0.235 \text{ GHSE}_{\text{Fe}}$$

Phase Al₅Fe₂

$$G^\circ(T) - 5.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Fe}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ -228576 + 48.99503 T + 5.0 \text{ GHSE}_{\text{Al}} + 2.0 \text{ GHSE}_{\text{Fe}}$$

Phase Al_5Fe_4

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = 12178.90 - 4.813 T + \text{GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-\text{A2,para}}(298.15 \text{ K}) = 5009.03 + \text{GHSER}_{\text{Fe}}$$

$$L_{\text{Al,Fe}}^{0,\text{Al}_5\text{Fe}_4} = -131649 + 29.4833 T$$

$$L_{\text{Al,Fe}}^{1,\text{Al}_5\text{Fe}_4} = -18619.5$$

Phase bcc-B2

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al}:\text{Al}:\square) = \text{GBCC}_{\text{Al}}$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 0.5 H_{\text{Fe}}^{\circ,\text{bcc}-\text{A2,para}}(298.15 \text{ K}) = G(\text{Fe}:\text{Al}:\square) =$$

$$-37890.5 + 7.9972 T + 0.5 \text{GBCC}_{\text{Al}} + 0.5 \text{GHSER}_{\text{Fe}}$$

$$T_{\text{c,Fe:Al}:\square}^{\text{bcc-B2}} = 521.5 \quad \beta_{\text{Fe:Al}:\square}^{\text{bcc-B2}} = 1.11$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 0.5 H_{\text{Fe}}^{\circ,\text{bcc}-\text{A2,para}}(298.15 \text{ K}) = G(\text{Al}:\text{Fe}:\square) =$$

$$-37890.5 + 7.9972 T + 0.5 \text{GBCC}_{\text{Al}} + 0.5 \text{GHSER}_{\text{Fe}}$$

$$T_{\text{c,Al:Fe}:\square}^{\text{bcc-B2}} = 521.5 \quad \beta_{\text{c,Al:Fe}:\square}^{\text{bcc-B2}} = 1.11$$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-\text{A2,para}}(298.15 \text{ K}) = G(\text{Fe}:\text{Fe}:\square) = \text{GHSER}_{\text{Fe}}$$

$$T_{\text{c,Fe:Fe}:\square}^{\text{bcc-B2}} = 1043 \text{ K} \quad \beta_{\text{c,Al:Fe}:\square}^{\text{bcc-B2}} = 2.22$$

$$L_{\text{Al,Fe:Al}:\square}^{0,\text{bcc-B2}} = L_{\text{Al:Al,Fe}:\square}^{0,\text{bcc-B2}} = -22485.07 + 7.9772 T$$

$$L_{\text{Al,Fe:Al}:\square}^{1,\text{bcc-B2}} = L_{\text{Al:Al,Fe}:\square}^{1,\text{bcc-B2}} = 368.15$$

$$T_{\text{c,Al,Fe:Al}:\square}^{0,\text{bcc-B2}} = T_{\text{c,Al:Al,Fe}:\square}^{0,\text{bcc-B2}} = 189.0$$

$$T_{\text{c,Al,Fe:Al}:\square}^{1,\text{bcc-B2}} = T_{\text{c,Al:Al,Fe}:\square}^{1,\text{bcc-B2}} = 63.0$$

$$\beta_{\text{Al,Fe:Al}:\square}^{0,\text{bcc-B2}} = \beta_{\text{Al:Al,Fe}:\square}^{0,\text{bcc-B2}} = 0.0$$

$$T_{\text{c,Al,Fe:Fe}:\square}^{0,\text{bcc-B2}} = T_{\text{c,Fe:Al,Fe}:\square}^{0,\text{bcc-B2}} = -189.0$$

$$T_{\text{c,Al,Fe:Fe}:\square}^{1,\text{bcc-B2}} = T_{\text{c,Fe:Al,Fe}:\square}^{1,\text{bcc-B2}} = 63.0$$

$$\beta_{\text{Al,Fe:Fe}:\square}^{0,\text{bcc-B2}} = \beta_{\text{Fe:Al,Fe}:\square}^{0,\text{bcc-B2}} = 0.0$$

$$L_{\text{Fe:Al,Fe}:\square}^{0,\text{bcc-B2}} = L_{\text{Al,Fe:Fe}:\square}^{0,\text{bcc-B2}} = -24694.0 + 7.9772 T$$

$$L_{\text{Fe:Al,Fe}:\square}^{1,\text{bcc-B2}} = L_{\text{Al,Fe:Fe}:\square}^{1,\text{bcc-B2}} = 368.15$$

$$G_{\text{Al:Fe:}\square}^* = -860 R \quad (R = 8.31451)$$

$$L_{\text{Al,Fe}}^0 = -30740 + 7.9972 T$$

$$L_{\text{Al,Fe}}^1 = 386.15$$

Phase bcc-B2

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Fe}}^{\circ,\text{fcc-A1,para}}(298.15 \text{ K}) = G(\text{Al:Fe:}\square) = 2.0 G_{\text{Al:Fe:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Fe}}^{\circ,\text{fcc-A1,para}}(298.15 \text{ K}) = G(\text{Fe:Al:}\square) = 2.0 G_{\text{Al:Fe:}\square}^*$$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{fcc-A1,para}}(298.15 \text{ K}) = G(\text{Fe:Fe:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Al,Fe:}\square}^{0,\text{bcc-A2}} = 4.0 L_{\text{Al,Fe}}^0$$

$$L_{\text{Al,Fe:}\square}^{1,\text{bcc-A2}} = 8.0 L_{\text{Al,Fe}}^1$$

$$T_{\text{C,Al,Fe:}\square}^{1,\text{bcc-A2}} = 504$$

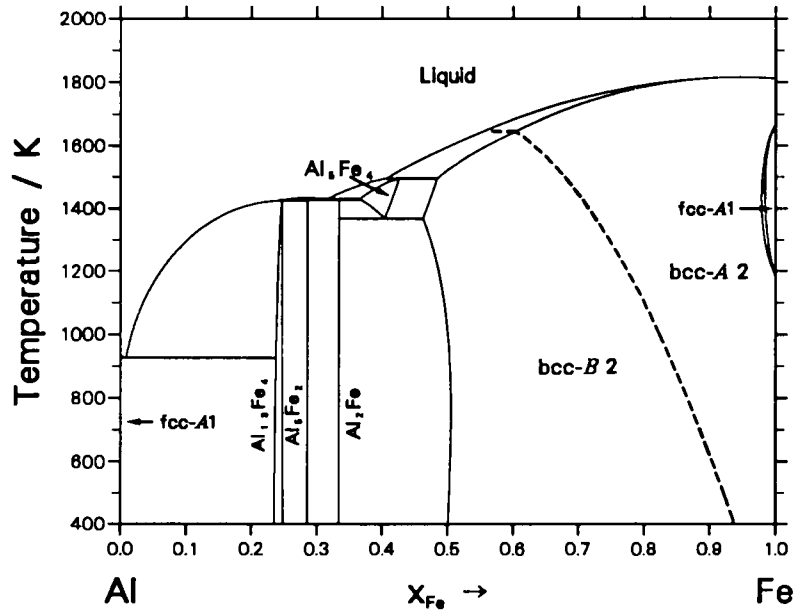


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Fe}	T / K
$Al_5Fe_4 \rightleftharpoons bcc-B2 + Al_2Fe$	Eutectoid	.403 .462 .333	1368.2
$Al_5Fe_2 \rightleftharpoons Liquid$	Congruent	.286 .286	1434.5
$Liquid \rightleftharpoons Al_5Fe_2 + Al_5Fe_4$	Eutectic	.316 .286 .365	1430.0
$Liquid + Al_5Fe_2 \rightleftharpoons Al_{13}Fe_4$	Peritectic	.242 .286 .247	1424.4
$Liquid \rightleftharpoons fcc-A1 + Al_{13}Fe_4$	Eutectic	.009 .000 .237	927.1
$Liquid + bcc-B2 \rightleftharpoons Al_5Fe_4$	Peritectic	.405 .483 .425	1495.5
$Al_5Fe_2 + Al_5Fe_4 \rightleftharpoons Al_2Fe$	Peritectoid	.286 .366 .333	1428.1

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Fe	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Fe)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Fe)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	AlFe	CsCl	<i>cP2</i> <i>Pm$\bar{3}m$</i>	M ₁ 1 M ₂ 1	
	AlFe ₃	BiF ₃	<i>cF16</i> <i>Fm$\bar{3}m$</i>	Al 4 Fe ₁ 4 Fe ₂ 8	not considered
	Al ₂ Fe	Al ₂ Fe	<i>aP18</i> <i>P1</i>		
	Al ₃ Fe		<i>mC102</i> <i>C2/m</i>		designated by Al ₁₃ Fe ₄
	Al ₅ Fe ₂		<i>oC*</i> <i>Cmcm</i>		
	ϵ		<i>cI16?</i>		designated by Al ₅ Fe ₄
	Al ₆ Fe	Al ₆ Fe	<i>oC28</i> <i>Cmc2₁</i>	Al ₁ 4 Al ₂ 4 Al ₃ 8 Al ₄ 8 Fe 4	metastable
	Al ₉ Fe ₂	Al ₉ Co ₂	<i>mP22</i> <i>P2₁/c</i>		metastable

System Al–Li

Solution Phases:

(stable) : Liquid, bcc-A2, fcc-A1
 (metastable) : hcp-A3

Compounds:

(stable) AlLi, Al₂Li₃, Al₄Li₉
 (metastable) AlMg-β, Al₂Zr, Al₃Zr, Al₃Zr₂, Al₁₂Mg₁₇

Modelling:

bcc-A2 : Substitutional, Redlich–Kister
 fcc-A1 : Substitutional, Redlich–Kister
 hcp-A3 : Substitutional, Redlich–Kister
 Liquid : Substitutional, Redlich–Kister
 AlLi : Sublattice model, (Al,Li)(Li,□)
 Al₂Li₃ : Stoichiometric, (Al)₂(Li)₃
 Al₄Li₉ : Stoichiometric, (Al)₄(Li)₉
 Al₁₂Mg₁₇ : Sublattice model, (Li)₂₄(Al,Li)₁₀(Al)₂₄
 Al₂Zr : Sublattice model, (Al)₂(Zr)
 Al₃Zr : Sublattice model, (Al)₃(Zr)
 Al₃Zr₂ : Sublattice model, (Al)₃(Zr)₂

Assessor and Date:

N. Saunders

Publication:

Calphad, 1, (3), 237–251 (1977)

Comments:

Data below used to calculate the Al–Li–Mg and Al–Li–Zr systems.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase hcp-A3

$$L_{\text{Al,Li:}\square}^{0,\text{hcp-A3}} = -27000.0 + 8.0 T$$

Phase bcc-A2

$$L_{\text{Al,Li};\square}^{0,\text{bcc-A2}} = -27000.0 + 8.0 T$$

$$L_{\text{Al,Li};\square}^{1,\text{bcc-A2}} = 1.0\text{E-}06$$

$$L_{\text{Al,Li};\square}^{2,\text{bcc-A2}} = 3000.0$$

Phase fcc-A1

$$L_{\text{Al,Li};\square}^{0,\text{fcc-A1}} = -27000.0 + 8.0 T$$

$$L_{\text{Al,Li};\square}^{1,\text{fcc-A1}} = 1.0\text{E-}06$$

$$L_{\text{Al,Li};\square}^{2,\text{fcc-A2}} = 3000.0 + 0.1 T$$

Phase liquid

$$L_{\text{Al,Li}}^{0,\text{liquid}} = -41500.0 + 20.96 T$$

$$L_{\text{Al,Li}}^{1,\text{liquid}} = 10000.0 - 5.8 T$$

$$L_{\text{Al,Li}}^{2,\text{liquid}} = 15902.0 - 9.368 T$$

$$L_{\text{Al,Li}}^{3,\text{liquid}} = -250.0$$

Phase AlLi

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Li}) = -41300.0 + 16.86 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Li}}$$

$$G^\circ(T) - 2.0 H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Li:Li}) = 2.0 \text{ GHSER}_{\text{Li}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al};\square) = 24000.0 + \text{GIISER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Li};\square) = 50000.0 + \text{GHSER}_{\text{Li}}$$

$$L_{\text{Al,Li;Li}}^{0,\text{AlLi}} = 20000.0$$

$$L_{\text{Al,Li;Li}}^{1,\text{AlLi}} = -26000.0$$

$$L_{\text{Al,Li};\square}^{0,\text{AlLi}} = 2000.0$$

$$L_{\text{Al;Li},\square}^{0,\text{AlLi}} = -24000.0 + 10.0 T$$

Phase Al₂Li₃

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ - 89640.0 + 32.79 T + 2.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Li}}$$

Phase Al₄Li₉

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 9.0 H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ - 185250.0 + 67.8 T + 4.0 \text{ GHSER}_{\text{Al}} + 9.0 \text{ GHSER}_{\text{Li}}$$

Phase Al₁₂Mg₁₇

$$G^\circ(T) - 34.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 24.0 H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Li:Al:Al}) = \\ - 800000 + 405 T + 34.0 \text{ GHSER}_{\text{Al}} + 24.0 \text{ GHSER}_{\text{Li}}$$

$$G^\circ(T) - 24.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 34.0 H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Li:Li:Al}) = \\ - 750000 + 405 T + 24.0 \text{ GHSER}_{\text{Al}} + 34.0 \text{ GHSER}_{\text{Li}}$$

Phase Al₂Zr

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ - 24240 + 16.869 T + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Li}}$$

Phase Al₃Zr

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ - 24400 + 16.88 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Li}}$$

Phase Al₃Zr₂

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ - 46625 + 33.25 T + 3.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Li}}$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Li}	T / K
Liquid \rightleftharpoons fcc-A1 + AlLi	Eutectic	.256 .155 .462	868.8
Liquid + AlLi \rightleftharpoons Al ₂ Li ₃	Peritectic	.775 .555 .600	793.6
Liquid + Al ₂ Li ₃ \rightleftharpoons Al ₄ Li ₉	Peritectic	.912 .600 .692	607.6
Liquid \rightleftharpoons Al ₄ Li ₉ + bcc-A2	Eutectic	.989 .692 .999	447.8
AlLi \rightleftharpoons Liquid	Congruent	.500 .500	978.0

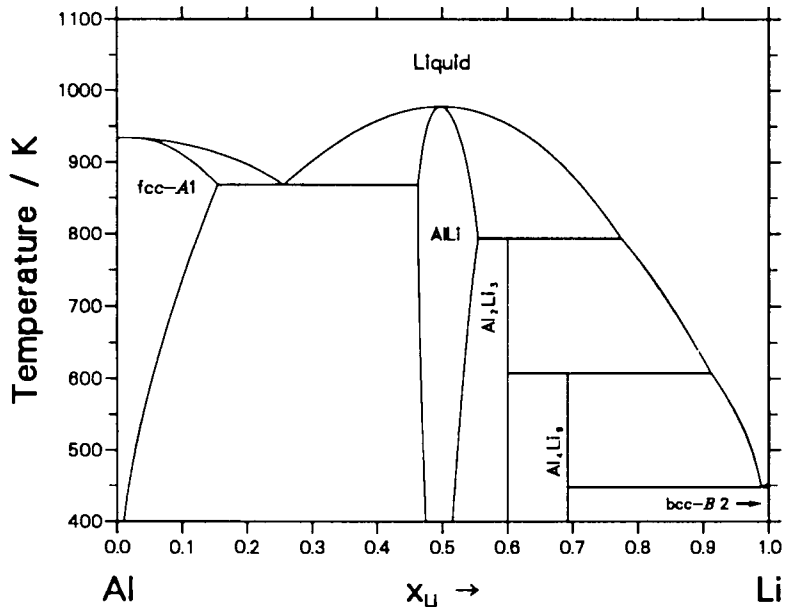


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Li	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Li)	W	$cI2$ $Im\bar{3}m$	M 2	
	AlLi	NaTl	$cF16$ $Fd\bar{3}m$	M ₁ 8 M ₂ 8	
	Al ₂ Li ₃	Ga ₂ Tc ₃	$hR15$ $R\bar{3}m$	Al 6 Li ₁ 3 Li ₂ 6	
	Al ₃ Li	AuCu ₃	$cP4$ $Pm\bar{3}m$	Al 3 Li 1	metast.
	Al ₄ Li ₉	Al ₄ Li ₉	$mC26$ $C2/m$		

System Al–Mg

Version I

Solution Phases:

(stable) Liquid, fcc-A1, hcp-A3
(metastable) bcc-A2

Compounds:

(stable) AlMg- β , AlMg- ϵ , Al-Mg- ζ , Al₁₂Mg₁₇
(metastable) AlLi

Modelling:

Liquid : Substitutional, Redlich–Kister
bcc-A2 : Substitutional, Redlich–Kister
fcc-A1 : Substitutional, Redlich–Kister
hcp-A3 : Substitutional, Redlich–Kister
Al₁₂Mg₁₇ : Sublattice model, Mg₂₄(Al,Mg)₁₀(Al,Mg)₂₄
AlMg- β : Stoichiometric, (Al)_{0.615}(Mg)_{0.385}
AlMg- ϵ : Stoichiometric, (Al)_{0.56}(Mg)_{0.44}
AlMg- ζ : Stoichiometric, (Al)_{0.525}(Mg)_{0.475}
AlLi : Sublattice model (Al,Mg)(Mg, \square)

Assessor and Date:

N. Saunders, 1991

Comments:

The data below were used for the thermodynamic assessment of the Al–Li–Mg system in COST507 Round I .

Thermodynamic properties of the solution and compound phases(J.mol⁻¹)

Phase AlMg- β

$$G^{\circ}(T) - 0.615 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 0.385 H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 1000.0 - 3.017 T + 0.615 \text{ GHSER}_{\text{Al}} + 0.385 \text{ GHSER}_{\text{Mg}}$$

Phase AlMg- ϵ

$$G^\circ(T) - 14.0 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 11.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \\ - 9275.0 - 104.0 T + 14.0 \text{ GHSER}_{\text{Al}} + 11.0 \text{ GHSER}_{\text{Mg}}$$

Phase AlMg- ζ

$$G^\circ(T) - 21.0 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 19.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \\ - 21040.0 - 163.76 T + 21.0 \text{ GHSER}_{\text{Al}} + 19.0 \text{ GHSER}_{\text{Mg}}$$

Phase Al₁₂Mg₁₇

$$G^\circ(T) - 34.0 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 24.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \text{G}(\text{Mg}:\text{Al}:\text{Al}) = \\ - 36800.0 - 140.0 T + 34.0 \text{ GHSER}_{\text{Al}} + 24.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 24.0 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 34.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \text{G}(\text{Mg}:\text{Mg}:\text{Al}) = \\ - 123200.0 - 56.26 T + 24.0 \text{ GHSER}_{\text{Al}} + 34.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 10.0 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 48.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \text{G}(\text{Mg}:\text{Al}:\text{Mg}) = \\ 151000.0 + 10.0 \text{ GHSER}_{\text{Al}} + 48.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 58.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \text{G}(\text{Mg}:\text{Mg}:\text{Mg}) = \\ 290000 + 58.0 \text{ GHSER}_{\text{Mg}}$$

$$L_{\text{Mg}:\text{Al}:\text{Mg}:\text{Al}}^{0, \text{Al}_{12}\text{Mg}_{17}} = - 17000$$

$$L_{\text{Mg}:\text{Al}:\text{Mg}:\text{Mg}}^{0, \text{Al}_{12}\text{Mg}_{17}} = - 17000$$

Phase AlLi

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) = \text{G}(\text{Al}:\square) = \\ 24000 + \text{GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \text{G}(\text{Mg}:\square) = \\ 50000 + \text{GBCC}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \text{G}(\text{Mg}:\text{Mg}) = \\ 2.0 \text{ GBCC}_{\text{Mg}}$$

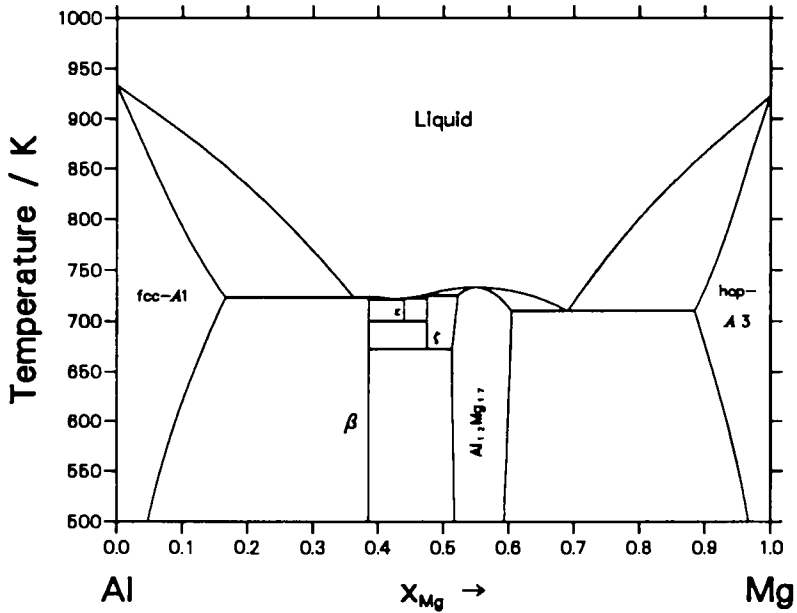
$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \text{G}(\text{Al}:\text{Mg}) = \\ 2486 - 1.75 T + \text{GBCC}_{\text{Al}} + \text{GBCC}_{\text{Mg}}$$

Phase bcc-A2

$$L_{\text{Al}:\text{Mg}:\square}^{0, \text{bcc}-A2} = 4971.0 - 3.5 T$$

$$L_{\text{Al}:\text{Mg}:\square}^{1, \text{bcc}-A2} = 900.0 + 0.423 T$$

$$L_{\text{Al}:\text{Mg}:\square}^{2, \text{bcc}-A2} = 950.0$$



Phase fcc-A1

$$L_{Al,Mg;\square}^{0, fcc-A1} = 4971.0 - 3.5 T$$

$$L_{Al,Mg;\square}^{1, fcc-A1} = 900.0 + 0.423 T$$

$$L_{Al,Mg;\square}^{2, fcc-A1} = 950.0$$

Phase hcp-A3

$$L_{Al,Mg;\square}^{0, hcp-A3} = 1950.0 - 2.0 T$$

$$L_{Al,Mg;\square}^{1, hcp-A3} = 1480.0 - 2.08 T$$

$$L_{Al,Mg;\square}^{2, hcp-A3} = 3500.0$$

Phase liquid

$$L_{Al,Mg}^{0, liquid} = -12000.0 + 8.566 T$$

$$L_{Al,Mg}^{1, liquid} = 1894.0 - 3.0 T$$

$$L_{Al,Mg}^{2, liquid} = 2000.0$$

Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Mg}	T / K
Liquid \rightleftharpoons fcc-Al + AlMg- β	Eutectic	.363 .166 .385	723.3
Liquid \rightleftharpoons AlMg- β + AlMg- ϵ	Eutectic	.423 .385 .440	721.5
Liquid + AlMg- ζ \rightleftharpoons + AlMg- ϵ	Peritectic	.436 .475 .440	722.0
Liquid + Al ₁₂ Mg ₁₇ \rightleftharpoons AlMg- ζ	Peritectic	.468 .522 .475	725.0
AlMg- ϵ \rightleftharpoons AlMg- β + AlMg- ζ	Eutectoid	.440 .385 .475	700.0
AlMg- ζ \rightleftharpoons AlMg- β + Al ₁₂ Mg ₁₇	Eutectoid	.475 .385 .513	673.0
Liquid \rightleftharpoons Al ₁₂ Mg ₁₇ + hcp-A3	Eutectic	.690 .604 .884	710.0
AlMg- β \rightleftharpoons Liquid	Congruent	.385 .385	724.1
Al ₁₂ Mg ₁₇ \rightleftharpoons Liquid	Congruent	.556 .556	733.3

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mg	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	Al ₁₂ Mg ₁₇	α -Mn cbcc-A12	<i>cI58</i> <i>I$\bar{4}3m$</i>	Al 24 Mg ₁ 2 Mg ₂ 8 Mg ₃ 24	γ in Mas1
	Al ₃ Mg ₂	Cd ₂ Na	<i>cF112</i> <i>Fd$\bar{3}m$</i>		<i>cF1832</i> in [91Vil] designated as AlMg- β
	Al ₃₀ Mg ₂₃	Co ₅ Cr ₂ Mo ₃ (Mn ₄₄ Si ₉)	<i>hR53</i> <i>R$\bar{3}$</i>	Al ₁ 18 Al ₂ 18 Al ₃ 18 Al ₄ 18 Al ₅ 18 Mg ₁ 3 Mg ₂ 6 Mg ₃ 6 Mg ₄ 18 Mg ₅ 18 Mg ₆ 18	ϵ
	Al ₄₉ Mg ₃₂	Al ₆ Mg ₁₁ Zn ₁₁	<i>cI162</i> <i>I$\bar{m}\bar{3}$</i>		ζ

System Al–Mg

Version II

Solution Phases:

(stable) Liquid, fcc-A1, hcp-A3
 (metastable) bcc-A2, hcp-Zn

Compounds:

(stable) AlMg- β , AlMg- ϵ , AlMg- γ
 (metastable) Laves-C14, Laves-C15, Laves-C36, Mg₂Zn₁₁,
 Mg₂Zn₃, MgZn, φ -phase, τ -phase

Modelling:

Liquid : Substitutional, Redlich–Kister
 bcc-A2 : Substitutional, Redlich–Kister
 fcc-A1 : Substitutional, Redlich–Kister
 hcp-A3 : Substitutional, Redlich–Kister
 hcp-Zn : Substitutional, Redlich–Kister
 AlMg- β : Stoichiometric, (Al)_{0.615}(Mg)_{0.385}
 AlMg- ϵ : Stoichiometric, (Al)_{0.56}(Mg)_{0.44}
 MgZn : Stoichiometric, (Al)₁₃(Mg)₁₂
 Mg₂Zn₃ : Stoichiometric, (Al)₃(Mg)₂
 φ -phase : Stoichiometric, (Al)₅(Mg)₆
 Mg₂Zn₁₁ : Stoichiometric, (Al)₁₁(Mg)₂
 AlMg- γ : Sublattice model, Mg₅(Al,Mg)₁₂(Al,Mg)₁₂
 Laves-C14 : Sublattice model (Al,Mg)₂(Al,Mg)
 Laves-C15 : Sublattice model (Al,Mg)₂(Al,Mg)
 Laves-C36 : Sublattice model (Al,Mg)₂(Al,Mg)
 τ -phase : Sublattice model (Mg)₂₆(Al,Mg)₆(Al,Mg)₄₈(Al)

Assessor and Date:

H.-L. Lukas

Comments:

The data for the Laves-C15 phase were evaluated by T. Bühler for the thermodynamic assessment of the Al–Cu–Mg system

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase liquid**

$$L_{Al,Mg}^{0,liquid} = -12000 + 8.566 T$$

$$L_{Al,Mg}^{1,liquid} = 1894 - 3 T$$

$$L_{Al,Mg}^{2,liquid} = 2000$$

Phase AlMg-β

$$G^\circ(T) - 140.0 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 89.0 H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = \\ -246175 - 675.55 T + 140.0 \text{ GHSER}_{Al} + 89.0 \text{ GHSER}_{Mg}$$

Phase AlMg-ε

$$G^\circ(T) - 30.0 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 23.0 H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = \\ -52565.4 - 173.1775 T + 30.0 \text{ GHSER}_{Al} + 23.0 \text{ GHSER}_{Mg}$$

Phase AlMg-γ

$$G^\circ(T) - 24.0 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 5.0 H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = G(\text{Mg:Al:Al}) = \\ 97875 - 101.5 T + 24.0 \text{ GHSER}_{Al} + 5.0 \text{ GHSER}_{Mg}$$

$$G^\circ(T) - 12.0 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 17.0 H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = G(\text{Mg:Mg:Al}) = \\ -52780 - 50.75 T + 12.0 \text{ GHSER}_{Al} + 17.0 \text{ GHSER}_{Mg}$$

$$G^\circ(T) - 12.0 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 17.0 H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = G(\text{Mg:Al:Mg}) = \\ 284124.6 - 138.069 T + 12.0 \text{ GHSER}_{Al} + 17.0 \text{ GHSER}_{Mg}$$

$$G^\circ(T) - 29.0 H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = G(\text{Mg:Mg:Mg}) = \\ 133469.6 - 87.319 T + 29.0 \text{ GHSER}_{Mg}$$

$$L_{Mg:Al:Al,Mg}^{0,Al_{12}Mg_{17}} = 113100 - 14.5 T$$

$$L_{Mg:Mg:Al,Mg}^{0,Al_{12}Mg_{17}} = 113100 - 14.5 T$$

Phase fcc-A1

$$L_{Al,Mg;\square}^{0, fcc-A1} = 4971 - 3.5 T$$

$$L_{Al,Mg;\square}^{1, fcc-A1} = 900 + 0.423 T$$

$$L_{Al,Mg;\square}^{2, fcc-A1} = 950$$

Phase hcp-A3

$$L_{\text{Al,Mg};\square}^{0,\text{hcp-A3}} = 1950 - 2 T$$

$$L_{\text{Al,Mg};\square}^{1,\text{hcp-A3}} = 1480 - 2.08 T$$

$$L_{\text{Al,Mg};\square}^{2,\text{hcp-A3}} = 3500$$

Phase hcp-Zn

$$L_{\text{Al,Mg};\square}^{0,\text{hcp-Zn}} = 1950 - 2 T$$

$$L_{\text{Al,Mg};\square}^{1,\text{hcp-Zn}} = 1480 - 2.08 T$$

$$L_{\text{Al,Mg};\square}^{2,\text{hcp-Zn}} = 3500$$

Phase Laves-C14

$$G^{\circ}(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al}) =$$

$$15000 + 3.0 \text{ GHSER}_{\text{Al}}$$

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Al}) =$$

$$17329 - 16.8 T + \text{GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Mg}}$$

$$G^{\circ}(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al:Mg}) =$$

$$12671.1 + 16.8 T + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mg}}$$

$$G^{\circ}(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Mg}) =$$

$$15000 + 3.0 \text{ GHSER}_{\text{Mg}}$$

$$L_{\text{Al,Mg:Al}}^{0,\text{Laves-C14}} = 15000$$

$$L_{\text{Al:Al,Mg}}^{0,\text{Laves-C14}} = 8000$$

$$L_{\text{Mg:Al,Mg}}^{0,\text{Laves-C14}} = 8000$$

$$L_{\text{Al,Mg:Mg}}^{0,\text{Laves-C14}} = 15000$$

Phase Laves-C15

$$G^{\circ}(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al}) =$$

$$15000 + 3.0 \text{ GHSER}_{\text{Al}}$$

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Al}) =$$

$$104970.96 - 16.46448 T + \text{GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Mg}}$$

$$G^{\circ}(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al:Mg}) =$$

$$30000 + 4.0 T + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mg}}$$

$$G^{\circ}(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000 + 3.0 \text{ GHSER}_{\text{Mg}}$$

$$L_{\text{Al,Mg:Al}}^{0,\text{Laves-C15}} = 15000$$

$$L_{\text{Al:Al,Mg}}^{0,\text{Laves-C15}} = 8000$$

$$L_{\text{Mg:Al,Mg}}^{0,\text{Laves-C15}} = 8000$$

$$L_{\text{Al,Mg:Mg}}^{0,\text{Laves-C15}} = 15000$$

Phase Laves-C36

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al}) =$$

$$15000 + 3.0 \text{ GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Al}) =$$

$$84970.96 - 16.46448 T + \text{GHSER}_{\text{Al}} + 2 \text{ GHISER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al:Mg}) =$$

$$21734 + 11.02 T + 2.0 \text{ GHISER}_{\text{Al}} + \text{GHISER}_{\text{Mg}}$$

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Mg}) =$$

$$15000 + 3.0 \text{ GHISER}_{\text{Mg}}$$

$$L_{\text{Al,Mg:Al}}^{0,\text{Laves-C36}} = 15000$$

$$L_{\text{Al:Al,Mg}}^{0,\text{Laves-C36}} = 8000$$

$$L_{\text{Mg:Al,Mg}}^{0,\text{Laves-C36}} = 8000$$

$$L_{\text{Al,Mg:Mg}}^{0,\text{Laves-C36}} = 15000$$

Phase Mg₂Zn₁₁

$$G^\circ(T) - 11.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$+ 130000 - 26.0 T + 11.0 \text{ GHISER}_{\text{Al}} + 2.0 \text{ GHISER}_{\text{Mg}}$$

Phase Mg₂Zn₃

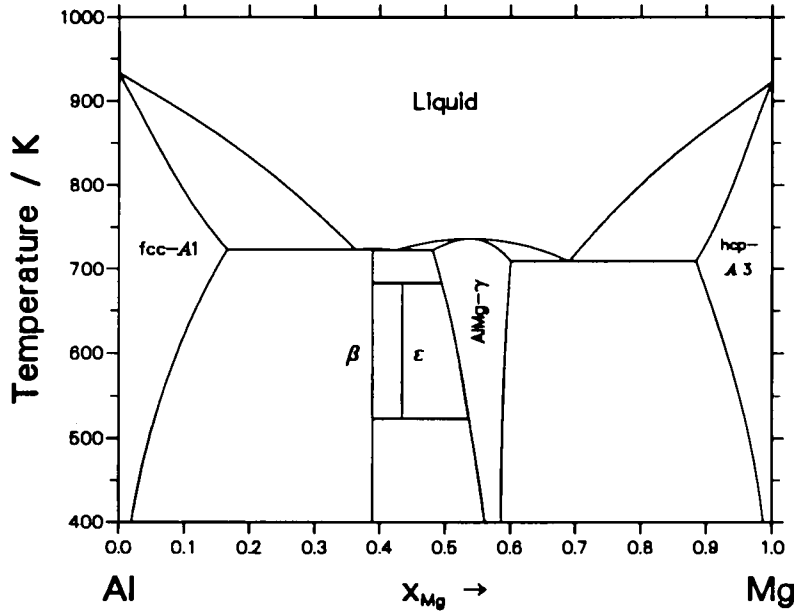
$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$1000 - 0.2 T + 3.0 \text{ GHISER}_{\text{Al}} + 2.0 \text{ GHISER}_{\text{Mg}}$$

Phase MgZn

$$G^\circ(T) - 13.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 12.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$- 10000 + 2.5 T + 13.0 \text{ GHISER}_{\text{Al}} + 12.0 \text{ GHISER}_{\text{Mg}}$$



Phase φ -phase

$$G^\circ(T) - 5.0 \cdot H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 6.0 \cdot H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 15400 - 16.5 \cdot T + 5.0 \cdot \text{GHSER}_{\text{Al}} + 6.0 \cdot \text{GHSER}_{\text{Mg}}$$

Phase τ -phase

$$G^\circ(T) - 55.0 \cdot H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 26.0 \cdot H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ G(\text{Mg:Al:Al:Al}) = - 105.3 \cdot T + 55.0 \cdot \text{GHSER}_{\text{Al}} + 26.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 49.0 \cdot H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 32.0 \cdot H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ G(\text{Mg:Mg:Al:Al}) = - 81000 - 186.3 \cdot T + 49.0 \cdot \text{GHSER}_{\text{Al}} + 32.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 7.0 \cdot H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 74.0 \cdot H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ G(\text{Mg:Al:Mg:Al}) = 1053000 + 405 \cdot T + 7.0 \cdot \text{GHSER}_{\text{Al}} + 74.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 80.0 \cdot H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ G(\text{Mg:Mg:Mg:Al}) = 405000 + 243 \cdot T + \text{GHSER}_{\text{Al}} + 80.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$L_{\text{Mg:Al:Al,Mg:Al}}^{0, \tau\text{-phase}} = - 202500 - 40.5 \cdot T$$

$$L_{\text{Mg:Mg:Al,Mg:Al}}^{0, \tau\text{-phase}} = - 202500 - 40.5 \cdot T$$

Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Mg}	T / K
Liquid \rightleftharpoons fcc-Al + AlMg- β	Eutectic	.363 .166 .389	723.6
Liquid \rightleftharpoons AlMg- β + AlMg- γ	Eutectic	.424 .389 .480	722.7
AlMg- β + AlMg- γ \rightleftharpoons AlMg- ϵ	Peritectoid	.389 .494 .434	682.9
AlMg- ϵ \rightleftharpoons AlMg- β + AlMg- γ	Eutectoid	.434 .389 .536	523.2.0
Liquid \rightleftharpoons AlMg- γ + hcp-Al3	Eutectic	.690 .601 .884	709.4
AlMg- β \rightleftharpoons Liquid	Congruent	.385 .385	724.7
Al ₁₂ Mg ₁₇ \rightleftharpoons Liquid	Congruent	.523 .523	736.3

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mg	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Mg)	Mg	$hP2$ $P6_3/mmc$	M 2	
	AlMg- γ	α -Mn bcc-Al2	$cI58$ $I\bar{4}3m$	Al 24 Mg ₁ 2 Mg ₂ 8 Mg ₃ 24	designated as Al ₁₂ Mg ₁₇
	Al ₃ Mg ₂	Cd ₂ Na	$cF112$ $Fd\bar{3}m$		$cF1832$ in [91Vil] designated as AlMg- β
	AlMg- ϵ	Co ₅ Cr ₂ Mo ₃ (Mn ₄₄ Si ₉)	$hR53$ $R\bar{3}$	Al ₁ 18 Al ₂ 18 Al ₃ 18 Al ₄ 18 Al ₅ 18 Mg ₁ 3 Mg ₂ 6 Mg ₃ 6 Mg ₄ 18 Mg ₅ 18 Mg ₆ 18	R phase in [Mas1]

System Al-Mn

Solution Phases:

Liquid, bcc-A2, cbcc-A12,
cub-A13, fcc-A1, hcp-A3

Stoichiometric Compounds:

(stable)

Al₁₁Mn₄, Al₆Mn, Al₄Mn, Al₈Mn₅-D8₁₀

(metastable)

Al₂Fe, Al₅Fe₂, Al₁₃Fe₄

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
cbcc-A12	:	Substitutional, Redlich-Kister
cub-A13	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Al ₈ Mn ₅ - D8 ₁₀	:	Sublattice model, (Al) ₁₂ (Mn) ₄ (Al,Mn) ₁₀
Al ₂ Fe	:	Stoichiometric, (Al) ₂ (Fe) ₁
Al ₅ Fe ₂	:	Stoichiometric, (Al) ₅ (Fe) ₂
Al ₁₃ Fe ₄	:	Sublattice model, (Al) _{.6275} (Fe) _{.235} (Al,□) _{.1375}

Assessor and Date:

Å. Jansson

Publication:

Trita-Mac-0462, May 1991, Materials Research Center,
The Royal Institute of Technology, Stockholm

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₁₁Mn₄

$$G^{\circ}(T) - 11.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 4.0 H_{\text{Mn}}^{\circ, \text{cbcc-A12, para}}(298.15 \text{ K}) = \\ - 354690.0 + 103.031 T + 11.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Mn}}$$

Phase Al₁₂Mn

$$G^{\circ}(T) - 12.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mn}}^{\circ, \text{cbcc-A12, para}}(298.15 \text{ K}) = \\ - 125730.0 + 54.98103 T + 12.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mn}}$$

Phase Al₄Mn

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12,para}}(298.15 \text{ K}) = \\ - 100005.0 + 30.0 T + 4.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mn}}$$

Phase Al₆Mn

$$G^\circ(T) - 6.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12,para}}(298.15 \text{ K}) = \\ - 124564.3 + 53.6593 T + 6.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mn}}$$

Phase Al₈Mn₅-D8₁₀

$$G^\circ(T) - 22.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 4.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12,para}}(298.15 \text{ K}) = G(\text{Al:Mn:Al}) = \\ - 308671 + 56.6488 T + 22.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Mn}}$$

$$G^\circ(T) - 12.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 14.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12,para}}(298.15 \text{ K}) = \\ G(\text{Al:Mn:Mn}) = - 596867 + 94.612 T + 12.0 \text{ GHSER}_{\text{Al}} + 14.0 \text{ GHSER}_{\text{Mn}}$$

$$L_{\text{Al:Mn:Al,Mn}}^{0,\text{Al}_8\text{Mn}_5-\text{D8}_{10}} = - 546234 + 387.348 T$$

Phase Al₂Fe

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12,para}}(298.15 \text{ K}) = \\ - 14065.0 T + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mn}}$$

Phase Al₅Fe₂

$$G^\circ(T) - 5.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 2.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12,para}}(298.15 \text{ K}) = \\ 5.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Mn}}$$

Phase Al₁₃Fe₄

$$G^\circ(T) - 0.765 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 0.235 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12,para}}(298.15 \text{ K}) = \\ - 20000.0 + 10.0 T + 0.765 \text{ GHSER}_{\text{Al}} + 0.235 \text{ GHSER}_{\text{Mn}}$$

$$G^\circ(T) - 0.6275 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 0.235 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12,para}}(298.15 \text{ K}) = \\ - 17000.0 + 10.0 T + 0.6275 \text{ GHSER}_{\text{Al}} + 0.235 \text{ GHSER}_{\text{Mn}}$$

Phase bcc-A2

$$L_{\text{Al,Mn:}\square}^{0,\text{bcc}-\text{A2}} = - 120077 + 52.851 T \quad L_{\text{Al,Mn:}\square}^{1,\text{bcc}-\text{A2}} = - 40652 + 29.2764 T$$

Phase cbcc-A12

$$L_{\text{Al,Mn:}\square}^{0,\text{cbcc}-\text{A12}} = - 101410 + 43.0 T$$

Phase cub-A13

$$L_{\text{Al,Mn:}\square}^{0,\text{cub}-\text{A13}} = - 119022 + 52.507 T \quad L_{\text{Al,Mn:}\square}^{1,\text{cub}-\text{A13}} = - 1763$$

Phase fcc-A1

$$L_{\text{Al,Mn};\square}^{0,\text{fcc-A1}} = -69300 + 25.0 T \quad L_{\text{Al,Mn};\square}^{1,\text{fcc-A1}} = 8800$$

Phase hcp-A3

$$L_{\text{Al,Mn};\square}^{0,\text{hcp-A3}} = -108066 + 43.83 T \quad L_{\text{Al,Mn};\square}^{1,\text{hcp-A3}} = -54519.8 + 40 T$$

Phase liquid

$$L_{\text{Al,Mn}}^{0,\text{liquid}} = -66174 + 27.0988 T$$

$$L_{\text{Al,Mn}}^{1,\text{liquid}} = -7509 + 5.4836 T$$

$$L_{\text{Al,Mn}}^{2,\text{liquid}} = -2639$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Mn}			T / K
Liquid + Al ₄ Mn \rightleftharpoons Al ₆ Mn	Peritectic	.021	.200	.143	978.0
Liquid \rightleftharpoons fcc-A1 + Al ₆ Mn	Eutectic	.010	.007	.143	931.1
fcc-A1 + Al ₆ Mn \rightleftharpoons Al ₁₂ Mn	Peritectoid	.002	.143	.077	817.0
Liquid + Al ₁₁ Mn ₄ \rightleftharpoons Al ₄ Mn	Peritectic	.127	.266	.200	1193.1
Liquid + Al ₈ Mn ₅ -D8 ₁₀ \rightleftharpoons Al ₁₁ Mn ₄	Peritectic	.205	.324	.266	1262.4
Liquid + hcp-A3 \rightleftharpoons Al ₈ Mn ₅ -D8 ₁₀	Peritectic	.425	.519	.486	1433.3
hcp-A3 \rightleftharpoons Al ₈ Mn ₅ -D8 ₁₀ + cub-A13	Eutectoid	.551	.511	.590	1143.7
bcc-A2 \rightleftharpoons hcp-A3 + cub-A13	Eutectoid	.601	.592	.621	1207.0
fcc-A1 + bcc-A2 \rightleftharpoons cub-A13	Pertitectoid	.913	.903	.910	1330.9
Liquid + bcc-A2 \rightleftharpoons hcp-A3	Peritectic	.588	.644	.641	1522.3
bcc-A2 \rightleftharpoons Liquid	Congruent	.816	.816	1582.0

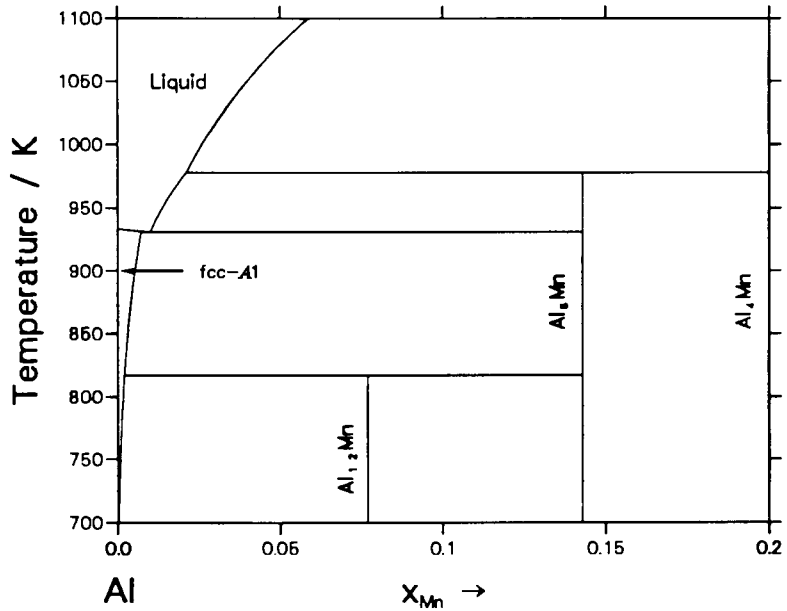
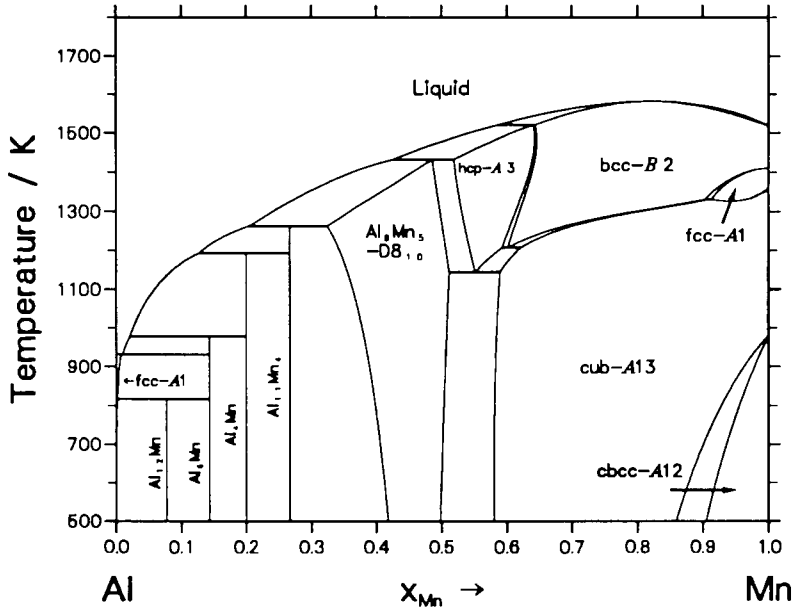


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mn	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M ₁ 4	
	α -Mn	α -Mn	<i>c58</i> <i>I43m</i>		cbcc-A1
	β -Mn	β -Mn	<i>cP20</i> <i>P4₁32</i>		cub-A13
	γ -Mn	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>		fcc-A1
	δ -Mn	W	<i>cF2</i> <i>Im$\bar{3}$m</i>		bcc-A2
	AlMn	AuCu-L1 ₀	<i>tP2</i> <i>P4/mmm</i>	M ₁ 1 M ₂ 1	metast.
	λ	Al ₄ Mn	<i>oP60</i> <i>Pnnn</i>		reported as Al ₄ Mn
	Al ₆ Mn	Al ₆ Mn	<i>oC28</i> <i>Cmcm</i>	Al ₁ 8 Al ₂ 8 Al ₃ 8 Mn 4	
	Al ₁₀ Mn ₃	Al ₅ Mn ₂	<i>hP28</i> <i>P6₃/mmc</i>	Al ₁ 2 Al ₂ 6 Al ₃ 12 Mn 6	
	Al ₁₁ Mn ₄ -L	Al ₁₁ Mn ₄	<i>aP30</i> <i>P$\bar{1}$</i>		transformation not taken into account reported as <i>aP15</i> in [91Vil]
	Al ₁₁ Mn ₄ -H	<i>oP160</i> <i>Pnma</i>		not in [90Mas] metast.
	Al ₁₂ Mn	Al ₁₂ W	<i>cF26</i> <i>Im$\bar{3}$</i>		not quoted in [90Mas] metast.
	Al ₈ Mn ₅	Al ₈ Cr ₅	<i>hR26</i> <i>R3m</i>		Al ₈ Mn ₅ -D0 ₈

System Al-Mo

Solution Phases:

(stable) Liquid, bcc-A2, fcc-A1
 (metastable) bcc-B2, hcp-A3

Compounds:

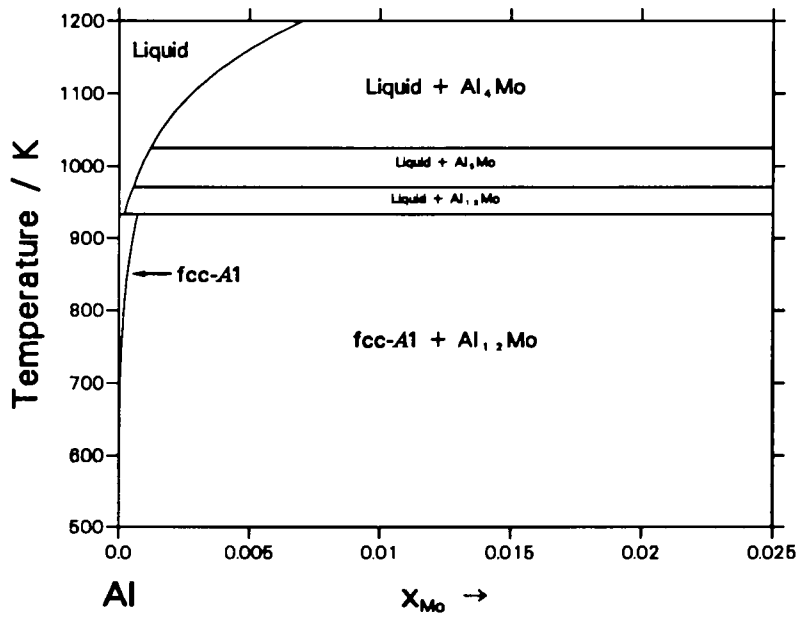
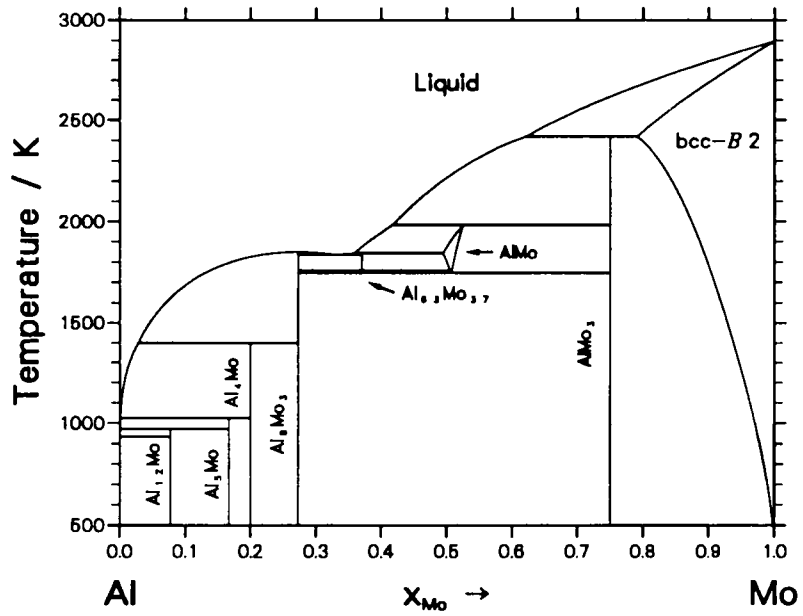
(stable) Al₁₂Mo, Al₄Mo, Al₅Mo, Al₆₃Mo₃₇, Al₈Mo₃, AlMo,
 cub-A15
 (metastable) AlM-D0₁₉, AlTi-L1₀

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Al ₁₂ Mo	:	Stoichiometric, (Al) ₁₂ (Mo)
Al ₅ Mo	:	Stoichiometric, (Al) ₅ (Mo)
Al ₄ Mo	:	Stoichiometric, (Al) ₄ (Mo)
Al ₆₃ Mo ₃₇	:	Stoichiometric, (Al) ₆₃ (Mo) ₃₇
Al ₈ Mo ₃	:	Stoichiometric, (Al) ₈ (Mo) ₃
cub-A15	:	Stoichiometric, (Al)(Mo) ₃
AlMo	:	Sublattice model, (Al,Mo)(Al,Mo)
bcc-B2	:	Sublattice model, (Al,Mo) _{0.5} (Al,Mo) _{0.5} (□) ₃ The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 ⇌ bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM-D0 ₁₉	:	Sublattice model, (Al,Mo) ₃ (Al,Mo)(□) _{0.5}
AlTi-L1 ₀	:	Sublattice model, (Al,Mo)(Al,Mo)

Assessor and Date:

N. Saunders (1996)



Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase Al₁₂Mo**

$$G^\circ(T) - 12.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 139100 + 26.975 T + 12.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mo}}$$

Phase Al₄Mo

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 137570 + 29.69 T + 4.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mo}}$$

Phase Al₅Mo

$$G^\circ(T) - 5.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -139104 + 30.156 T + 5.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mo}}$$

Phase Al₆₃Mo₃₇

$$G^\circ(T) - 63.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 37.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 2268100 + 167.2 T + 63.0 \text{ GHSER}_{\text{Al}} + 37.0 \text{ GHSER}_{\text{Mo}}$$

Phase Al₈Mo₃

$$G^\circ(T) - 8.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 412500 + 105.05 T + 8.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Mo}}$$

Phase cub-A15

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 89000 + 20 T - 0.003 T^2 + \text{GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Mo}}$$

Phase AlMo

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = \\ 2.0 \text{ GBCC}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Mo}) = \\ - 36850 + T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mo}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Al}) = \\ - 36850 + T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mo}}$$

$$G^\circ(T) - 2.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Mo}) = \\ 2.0 + \text{GHSER}_{\text{Mo}}$$

$$L_{\text{Al,Mo:Al}}^{0,\text{AlMo}} = L_{\text{Al:Al,Mo}}^{0,\text{AlMo}} = -5000$$

$$L_{\text{Mo:Al,Mo}}^{0,\text{AlMo}} = L_{\text{Al,Mo:Mo}}^{0,\text{AlMo}} = 25000$$

$$L_{\text{Mo:Al,Mo}}^{1,\text{AlMo}} = L_{\text{Al,Mo:Mo}}^{1,\text{AlMo}} = -10000$$

Phase AlM-DO₁₉

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al}) =$$

$$4.0 \text{ GHCP}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mo:Al}) =$$

$$-64000 + 15.32 T + \text{GHCP}_{\text{Al}} + 3.0 \text{ GHCP}_{\text{Mo}}$$

$$G^\circ(T) - 3.0 \text{ GHCP}_{\text{Al}} - H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Mo}) =$$

$$-64000 + 15.32 T + 3.0 \text{ GHCP}_{\text{Al}} + \text{GHCP}_{\text{Mo}}$$

$$G^\circ(T) - 4.0 H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mo:Mo}) =$$

$$4.0 \text{ GHSER}_{\text{Mo}}$$

Phase liquid

$$L_{\text{Al,Mo}}^{0,\text{liquid}} = -100000 + 35 T$$

$$L_{\text{Al,Mo}}^{1,\text{liquid}} = -15000 + 6.3 T$$

Phase fcc-A1

$$L_{\text{Al,Mo:\square}}^{0,\text{fcc-A1}} = -92220 + 20 T$$

Phase bcc-A2

$$L_{\text{Al,Mo:\square}}^{0,\text{bcc-A2}} = -75000 + 25 T$$

Phase bcc-B2

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al:\square}) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mo:Al:\square}) =$$

$$-7050 + T$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Mo:\square}) =$$

$$-7050 + T$$

$$G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mo:Mo:\square}) = 0.0$$

$$L_{\text{Al:Al,Mo:\square}}^{0,\text{bcc-B2}} = 7050 - T$$

$$L_{\text{Mo:Al,Mo:\square}}^{0,\text{bcc-B2}} = 7050 - T$$

$$L_{\text{Al,Mo:Al:\square}}^{0,\text{bcc-B2}} = 7050 - T$$

$$L_{\text{Al,Mo:Al:\square}}^{0,\text{bcc-B2}} = 7050 - T$$

Phase bcc-B2

$$G_{\text{Al:Mo:}\square}^* = -7050 + T$$

$$G^\circ(T) - {}_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Mo:}\square) = 2.0 \quad G_{\text{Al:Mo:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mo:Al:}\square) = 2.0 \quad G_{\text{Al:Mo:}\square}^*$$

$$G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mo:Mo:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Al:Mo:}\square}^{0,\text{bcc-A2}} = -75000 + 25 T$$

Phase hcp-A3

$$L_{\text{Al:Mo:}\square}^{0,\text{hcp-A3}} = -85570 + 25 T$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Mo}			T / K
$\text{AlMo} \rightleftharpoons \text{Al}_8\text{Mo}_3 + \text{cub-A15}$	Eutectoid	.507	.273	.750	1745.6
$\text{Al}_{63}\text{Mo}_{37} \rightleftharpoons \text{Al}_8\text{Mo}_3 + \text{AlMo}$	Eutectoid	.370	.273	.505	1759.6
$\text{Liquid} \rightleftharpoons \text{Al}_8\text{Mo}_3 + \text{Al}_{63}\text{Mo}_{37}$	Eutectic	.333	.273	.370	1836.4
$\text{Liquid} + \text{AlMo} \rightleftharpoons \text{Al}_{63}\text{Mo}_{37}$	Peritectic	.358	.4955	.370	1844.7
$\text{Liquid} + \text{cub-A15} \rightleftharpoons \text{AlMo}$	Peritectic	.417	.750	.525	1983.6
$\text{Liquid} + \text{bcc-A2} \rightleftharpoons \text{cub-A15}$	Peritectic	.621	.791	.750	2418.9
$\text{Liquid} + \text{Al}_4\text{Mo} \rightleftharpoons \text{Al}_5\text{Mo}$	Peritectic	.0012	.200	.166	1025.2
$\text{Liquid} + \text{Al}_5\text{Mo} \rightleftharpoons \text{Al}_{12}\text{Mo}$	Peritectic	.0005	.167	.077	971.6
$\text{Liquid} + \text{Al}_{12}\text{Mo} \rightleftharpoons \text{fcc-A1}$	Peritectic	.0002	.077	.0007	933.8
$\text{Liquid} + \text{Al}_8\text{Mo}_3 \rightleftharpoons \text{Al}_4\text{Mo}$	Peritectic	.028	.273	.200	1397.7
$\text{Al}_8\text{Mo}_3 \rightleftharpoons \text{Liquid}$	Congruent	.273	.273	...	1850.5

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mo	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Mo)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	$\Lambda_{12}\text{Mo}$	$\Lambda_{12}\text{W}$	<i>cI26</i> <i>Im$\bar{3}$</i>	Al 24 Mo 2	
	$\Lambda_5\text{Mo}$	$\Lambda_5\text{W}$	<i>hP12</i> <i>P6$\bar{3}$</i>		
	$\Lambda_4\text{Mo}$	$\Lambda_4\text{W}$	<i>mC30</i> <i>Cm</i>	Al ₁ 2 Al ₂ 2 Mo ₁ 2 Al ₃ 4 Al ₄ 4 Al ₅ 4 Al ₆ 4 Al ₇ 4 Mo ₂ 4	
	$\Lambda_8\text{Mo}_3$	$\Lambda_8\text{Mo}_3$	<i>mC22</i> <i>C2/m</i>	Mo ₁ 2 Al ₁ 48 Al ₂ 4 Al ₃ 4 Al ₄ 4 Mo ₂ 4	
	$\Lambda_{23}\text{V}_4$	$\Lambda_{23}\text{V}_4$	<i>hP54</i> <i>P6$\bar{3}$/mmc</i>		
	$\Lambda_{63}\text{Mo}_{37}$				
	ΛMo	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	ΛMo_3	Cr_3Si	<i>cP8</i> <i>Pm$\bar{3}n$</i>	Al 2 Mo 6	cub-A15

System Al-N

Solution Phases:

(stable) Liquid, fcc-A1
 (metastable) bcc-A2, hcp-A3

Compound:

AlN

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Sublattice model, (Al)(C,□)₃
 fcc-A1 : Sublattice model, (Al)(C,□)
 hcp-A3 : Sublattice model, (Al)(C,□)_{0.5}
 gas : ideal (Al,Al₂,N,N₂,N₃)
 AlN : Stoichiometric, (Al)(N)

Assessor and Date:

H.L. Lukas 1992
 Data relative for the bcc-A2 and hcp-3 phases were
 evaluated by R. Fetzer and K. Zeng for the Al-N-Ti
 system.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlN

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) =$$

$$- 338005.5 + 305.211 T - 46.94867 T \cdot \ln T - 0.00189068 T^2$$

$$+ 874528 T^{-1} + 1.3756\text{E-}07 T^3$$

Phase bcc-A2

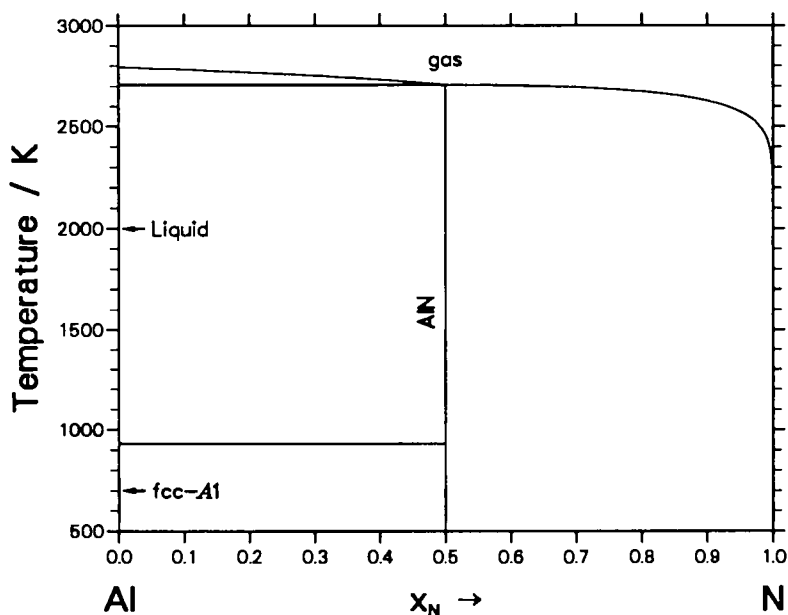
$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) =$$

$$23000 + 10 T + \text{GHSER}_{\text{Al}} + 3.0 \text{GHSER}_{\text{N}}$$

Phase fcc-A1

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) =$$

$$80 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{N}}$$



Phase hcp-A3

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{0.5\text{N}_2}^{\circ, \text{gcs}}(298.15 \text{ K}) = 80000 T + \text{GHSER}_{\text{Al}} + 0.5 \text{GHSER}_{\text{N}}$$

Phase liquid

$$L_{\text{Al,N}}^{0, \text{liquid}} = -336826.61 + 103.22478 T$$

Phase gas(Al, Al₂, N, N₂, N₃) (P = 0.1 MPa)

$$G_{\text{Al}}^{\circ, \text{gas}}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) = RT \ln P +$$

298.15 < T < 4300.00 :	323947.58 - 25.1480948 T - 20.859 T · ln T + 4.5665E-05 T ² - 3.942E-09 T ³ - 24275.5 T ⁻¹
4300.00 < T < 8200.00 :	342017.234 - 54.0526114 T - 17.7891 T · ln T + 6.822E-05 T ² - 1.9111E-08 T ³ - 14782200 T ⁻¹
8200.00 < T < 10000.00 :	542396.07 - 411.214335 T + 22.2419 T · ln T - 0.00349619 T ² + 4.0491E-08 T ³ - 2.0366965E+08 T ⁻¹

$$\begin{aligned}
G_{\text{Al}_2}^{\circ, \text{gas}}(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) &= RT \ln P + \\
298.15 < T < 900.00 &: 496408.232 + 35.4797382 T - 41.6397 T \cdot \ln T \\
&\quad + 0.00249636 T^2 - 4.9050\text{E-}07 T^3 \\
&\quad + 85390.3 T^{-1} \\
900.00 < T < 10000.00 &: + 497613.221 + 17.3681302 T - 38.85476 T \cdot \ln T \\
&\quad - 2.249805\text{E-}04 T^2 - 9.49003167\text{E-}09 T^3 \\
&\quad - 5287.23 T^{-1} \\
G_{\text{N}}^{\circ, \text{gas}}(T) - H_{0.5\text{N}_2}^{\circ, \text{gas}}(298.15 \text{ K}) &= RT \ln P + \\
298.15 < T < 2950.00 &: 466446.153 + 2788.78662 T^{-1} - 13.2660528 T \\
&\quad - 20.8939295 T \cdot \ln T + 8.4552092\text{E-}05 T^2 \\
&\quad - 1.00186856\text{E-}08 T^3 \\
2950.00 < T < 6000.00 &: 481259.023 - 7559107.28 T^{-1} - 52.4348889 T \\
&\quad - 16.3761342 T \cdot \ln T - 2.28373808\text{E-}04 T^2 \\
&\quad - 2.78997209\text{E-}08 T^3 \\
G_{\text{N}_2}^{\circ, \text{gas}}(T) - 2.0 H_{0.5\text{N}_2}^{\circ, \text{gas}}(298.15 \text{ K}) &= 2.0 \text{ GHSE}_{\text{N}} + RT \ln P \\
G_{\text{N}_3}^{\circ, \text{gas}}(T) - 3.0 H_{0.5\text{N}_2}^{\circ, \text{gas}}(298.15 \text{ K}) &= RT \ln P + \\
298.15 < T < 800.00 &: 403075.636 - 14.3245228 T - 29.5595416 T \cdot \ln T \\
&\quad - 0.02413122 T^2 + 3.6156036\text{E-}06 T^3 \\
&\quad + 55714.144 T^{-1} \\
800.00 < T < 2000.00 &: 388937.207 + 158.809275 T - 55.404528 T \cdot \ln T \\
&\quad - 0.0026570492 T^2 + 1.9365644\text{E-}07 T^3 \\
&\quad + 1536448.48 T^{-1} \\
2000.00 < T < 6000.00 &: 380898.006 + 210.207464 T - 62.295576 T \cdot \ln T \\
&\quad + 6.5726456\text{E-}06 T^2 - 7.868012\text{E-}10 T^3 \\
&\quad + 3336949.2 T^{-1}
\end{aligned}$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{N}	T / K
Liquid \rightleftharpoons fcc-Al + AlN	Degenerate	.000 .000 .500	933.3
Liquid + gas \rightleftharpoons AlN	Peritectic-like	.001 .503 .500	2707.7

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Al-N	(Al)	Cu	$cF4$ $Fm\bar{3}m$	Wurtzite
	AlN	ZnS	$hP4$ $P6_3mc$	

System Al-Nb

Solution Phases:

(stable) Liquid, bcc-A2, fcc-A1
 (metastable) bcc-B2, hcp-A3

Compounds :

(stable) AlM-D0₂₂, σ , AlNb₃-A15
 (metastable) AlTi-L1₀, AlM-D0₁₉

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 bcc-B2 : Sublattice model, (Al,Nb)_{0.5}(Al,Nb)_{0.5}(□)₃
 The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 \rightleftharpoons bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.

AlM-D0₂₂ : Sublattice model, (Al)₃(Nb)
 AlNb₃-A15 : Sublattice model, (Al,Nb)(Nb)₃
 σ : Sublattice model, (Al)₈(Nb)₄(Al,Nb)₁₈
 AlTi-L1₀ : Sublattice model, (Al)(Nb)
 AlM-D0₁₉ : Sublattice model, (Al,Nb)₃(Al,Nb)(□)

Assessor and Date:

N. Saunders, 1997.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase AlM-D0₂₂**

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = \\ - 136000 + 24 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nb}}$$

Phase AlM-D0₁₉

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al}:\text{Al}:\square) = 4.0 \text{ GHCP}_{\text{Al}}$$

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al}:\text{Nb}:\square) = \\ - 98000 + 22 T + 3.0 \text{ GHCP}_{\text{Al}} + \text{GHCP}_{\text{Nb}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb}:\text{Al}:\square) = \\ - 98000 + 10 T + \text{GHCP}_{\text{Al}} + 3.0 \text{ GHCP}_{\text{Nb}}$$

$$G^\circ(T) - 4.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb}:\text{Nb}:\square) = 4.0 \text{ GHCP}_{\text{Nb}}$$

$$L_{\text{Al},\text{Nb}:\text{Al}:\square}^{0,\text{AlM-D0}_{19}} = - 137400 + 60 T$$

$$L_{\text{Al}:\text{Al},\text{Nb}:\square}^{0,\text{AlM-D0}_{19}} = - 45760 + 20 T$$

$$L_{\text{Nb}:\text{Al},\text{Nb}:\square}^{0,\text{AlM-D0}_{19}} = 4000$$

$$L_{\text{Al},\text{Nb}:\text{Nb}:\square}^{0,\text{AlM-D0}_{19}} = 12000$$

Phase AlNb₃-A15

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb}:\text{Al}) = \\ - 77920 + 4.88 T + \text{GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Nb}}$$

$$G^\circ(T) - 4.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb}:\text{Nb}) = \\ 20000 + 10 T + 4.0 \text{ GHSER}_{\text{Nb}}$$

$$L_{\text{Nb}:\text{Al},\text{Nb}}^{0,\text{AlNb}_3\text{-A15}} = - 68000 + 20 T$$

$$L_{\text{Nb}:\text{Al},\text{Nb}}^{1,\text{AlNb}_3\text{-AA15}} = 1.0\text{E-}04$$

$$L_{\text{Nb}:\text{Al},\text{Nb}}^{2,\text{AlNb}_3\text{-AA15}} = - 12000$$

Phase σ

$$G^\circ(T) - 26.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 4.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al}:\text{Nb}:\text{Al}) = \\ - 150000 + 96 T + 26.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Nb}}$$

$$G^\circ(T) - 8.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 22.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al}:\text{Nb}:\text{Nb}) = \\ - 635250 + 60 T + 8.0 \text{ GHSER}_{\text{Al}} + 22.0 \text{ GHSER}_{\text{Nb}}$$

$$L_{\text{Al}:\text{Nb}:\text{Al},\text{Nb}}^{0,\sigma} = - 990000 + 270 T$$

$$L_{\text{Al}:\text{Nb}:\text{Al},\text{Nb}}^{1,\sigma} = 420000$$

Phase AlTi-L1₀

$$G^{\circ}(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 4 + 2.0 \text{ GHSER}_{\text{Al}}$$

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Nb}) =$$

$$- 44400 + 5.5 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nb}}$$

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Al}) =$$

$$- 44400 + 5.5 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nb}}$$

$$G^{\circ}(T) - 2.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Nb}) = 2.0 \text{ GFCC}_{\text{Nb}}$$

$$L_{\text{Al:Nb:Al}}^{0,\text{AlTi-L1}_0} = - 80800 + 30 T$$

$$L_{\text{Al:Al:Nb}}^{0,\text{AlTi-L1}_0} = - 80800 + 30 T$$

$$L_{\text{Nb:Al:Nb}}^{0,\text{AlTi-L1}_0} = - 37600$$

$$L_{\text{Al:Nb:Nb}}^{0,\text{AlTi-L1}_0} = - 37600$$

Phase bcc-A2

$$L_{\text{Al:Nb:}\square}^{0,\text{bcc-A2}} = - 104050 + 30 T$$

$$L_{\text{Al:Nb:}\square}^{1,\text{bcc-A2}} = 9140 - 4 T$$

$$L_{\text{Al:Nb:}\square}^{2,\text{bcc-A2}} = 12000$$

Phase bcc-B2

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 0$$

$$G^{\circ}(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Nb})$$

$$- 8650 + T$$

$$G^{\circ}(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Al})$$

$$- 8650 + T$$

$$G^{\circ}(T) - H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Nb}) = 0$$

$$L_{\text{Al:Al:Nb:}\square}^{0,\text{bcc-B2}} = 8650 - T$$

$$L_{\text{Nb:Al:Nb:}\square}^{0,\text{bcc-B2}} = 8650 - T$$

$$L_{\text{Al:Nb:Al:}\square}^{0,\text{bcc-B2}} = 8650 - T$$

$$L_{\text{Al:Nb:Nb:}\square}^{0,\text{bcc-B2}} = 8650 - T$$

Phase bcc-B2

$$G_{\text{Al:Nb:}\square}^* = -8650 + T$$

$$G^\circ(T) - {}_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Nb:}\square) = 2.0 \quad G_{\text{Al:Nb:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Nb:Al:}\square) = 2.0 \quad G_{\text{Al:Nb:}\square}^*$$

$$G^\circ(T) - H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Nb:Nb:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Al:Nb:}\square}^{0,\text{bcc-A2}} = -104050 + 30 T$$

$$L_{\text{Al:Nb:}\square}^{1,\text{bcc-A2}} = 9140 - 4 T$$

$$L_{\text{Al:Nb:}\square}^{2,\text{bcc-A2}} = 12000$$

Phase fcc-A1

$$L_{\text{Al:Nb:}\square}^{0,\text{fcc-A1}} = -113500 + 21.1 T$$

$$L_{\text{Al:Nb:}\square}^{1,\text{fcc-A1}} = 5000$$

$$L_{\text{Al:Nb:}\square}^{2,\text{fcc-A1}} = 10000$$

Phase hcp-A3

$$L_{\text{Al:Nb:}\square}^{0,\text{hcp-A3}} = -113500 + 21.1 T$$

$$L_{\text{Al:Nb:}\square}^{1,\text{hcp-A3}} = 5000$$

$$L_{\text{Al:Nb:}\square}^{2,\text{hcp-A3}} = 10000$$

Phase liquid

$$L_{\text{Al,Nb}}^{0,\text{liquid}} = -91000 + 25 T$$

$$L_{\text{Al,Nb}}^{1,\text{liquid}} = 6000$$

$$L_{\text{Al,Nb}}^{2,\text{liquid}} = 15000$$

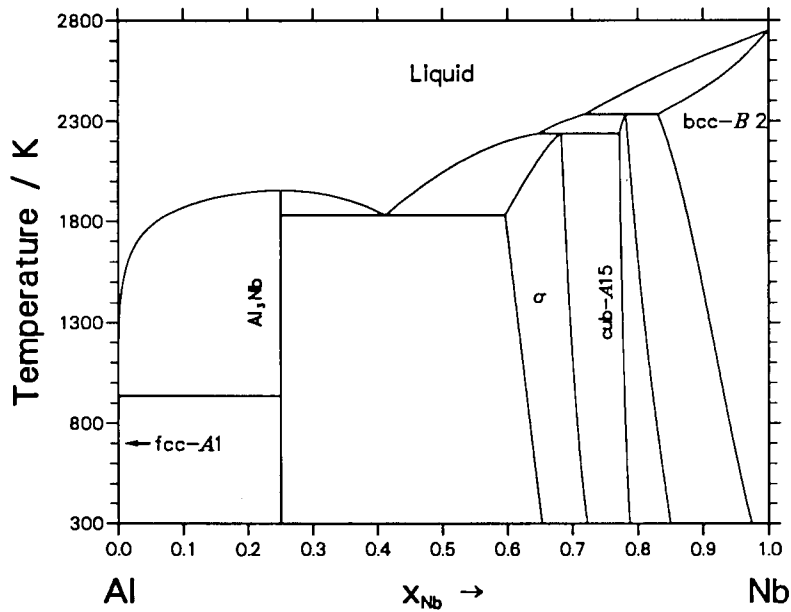


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Nb}	T / K
Liquid + Al_3Nb^* \rightleftharpoons fcc-A1	Peritectic	.000 .250 .001	934.2
Liquid \rightleftharpoons Al_3Nb^* + σ	Eutectic	.412 .250 .596	1832.1
Liquid + $AlNb_3^*$ \rightleftharpoons σ	Peritectic	.647 .772 .683	2237.6
Liquid + bcc-A2 \rightleftharpoons $AlNb_3^{**}$	Peritectic	.718 .831 .782	2333.7
Al_3Nb^* \rightleftharpoons Liquid	Congruent	.250 .250 ...	1955.5

* Al_3Nb-D0_{22} ** $Cr_3Si-A15$

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Nb	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Nb)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	AlNb ₃	Cr ₃ Si	<i>cP8</i> <i>Pm$\bar{3}n$</i>	Al 2 Nb 6	cub-A15
	AlNb ₂	σ -CrFe	<i>tP30</i> <i>P4₂/mnm</i>	Al ₁ 2 Nb ₁ 4 Al ₂ 8 Nb ₂ 8 Nb ₃ 8	
	Al ₃ Nb	Al ₃ Ti	<i>tI8</i> <i>I4/m$\bar{3}m$</i>	Nb 2 Al ₁ 2 Al ₁ 42	AlM-D0 ₂₂

System Al-Nd

Solution Phases:

Liquid, bcc-A2, dhcp

Compounds:

Al₁₁Nd₃-H, Al₁₁Nd₃-L, Al₃Nd, AlNd, AlNd₂, AlNd₃,
Laves-C15

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
dhcp	:	Substitutional, Redlich-Kister
Al ₁₁ Nd ₃ -H	:	Stoichiometric, (Al) ₁₁ (Nd) ₃
Al ₁₁ Nd ₃ -L	:	Stoichiometric, (Al) ₁₁ (Nd) ₃
Al ₃ Nd	:	Stoichiometric, (Al) ₃ (Nd)
AlNd	:	Stoichiometric, (Al)(Nd)
AlNd ₂	:	Stoichiometric, (Al)(Nd) ₂
AlNd ₃	:	Stoichiometric, (Al)(Nd) ₃
Laves-C15	:	Stoichiometric, (Al) ₂ (Nd)

Assessor and Date:

G. Cacciamani, G. Borzone, R. Ferro

Publication:

G. Cacciamani, G. Borzone, R. Ferro, *Anales de Fisica*
86B, 160-162 (1991)
Revised in 1997.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₁₁Nd₃-H

$$G^{\circ}(T) - 11.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Nd}}^{\circ, \text{dhcp}}(298.15 \text{ K}) = \\ - 526776.18 + 114.5827 T + 11.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Nd}}$$

Phase Al₁₁Nd₃-L

$$G^{\circ}(T) - 11.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Nd}}^{\circ, \text{dhcp}}(298.15 \text{ K}) = \\ - 548308.18 + 132.1646 T + 11.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Nd}}$$

Phase Laves-C15

$$G^{\circ}(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Nd}}^{\circ, \text{dhcp}}(298.15 \text{ K}) = \\ - 158935.47 + 41.37165 T + 2.0 \text{ GHSE}_{\text{Al}} + \text{GHSE}_{\text{Nd}}$$

Phase Al₃Nd

$$G^{\circ}(T) - 3.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Nd}}^{\circ, \text{dhcp}}(298.15 \text{ K}) = \\ - 181169.24 + 47.75868 T + 3.0 \text{ GHSE}_{\text{Al}} + \text{GHSE}_{\text{Nd}}$$

Phase AlNd₂

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Nd}}^{\circ, \text{dhcp}}(298.15 \text{ K}) = \\ - 107787.66 + 37.00017 T + \text{GHSE}_{\text{Al}} + 2.0 \text{ GHSE}_{\text{Nd}}$$

Phase AlNd

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Nd}}^{\circ, \text{dhcp}}(298.15 \text{ K}) = \\ - 99854.84 + 34.32248 T + \text{GHSE}_{\text{Al}} + \text{GHSE}_{\text{Nd}}$$

Phase AlNd₃

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Nd}}^{\circ, \text{dhcp}}(298.15 \text{ K}) = \\ - 107474.72 + 35.0142 T + \text{GHSE}_{\text{Al}} + 3.0 \text{ GHSE}_{\text{Nd}}$$

Phase bcc-A2

$$L_{\text{Al,Nd};\square}^{0, \text{bcc-A2}} = - 113226 + 45.05 T$$

$$L_{\text{Al,Nd};\square}^{1, \text{bcc-A2}} = 10340 - 15.93 T$$

Phase fcc-A1

$$L_{\text{Al,Nd};\square}^{0, \text{fcc-A1}} = 0$$

Phase Liquid

$$L_{\text{Al,Nd}}^{0, \text{liquid}} = - 125909.87 + 56.16354 T - 21805836 T^{-1}$$

$$L_{\text{Al,Nd}}^{1, \text{liquid}} = 35170.81 - 33.34898 T - 32643234 T^{-1}$$

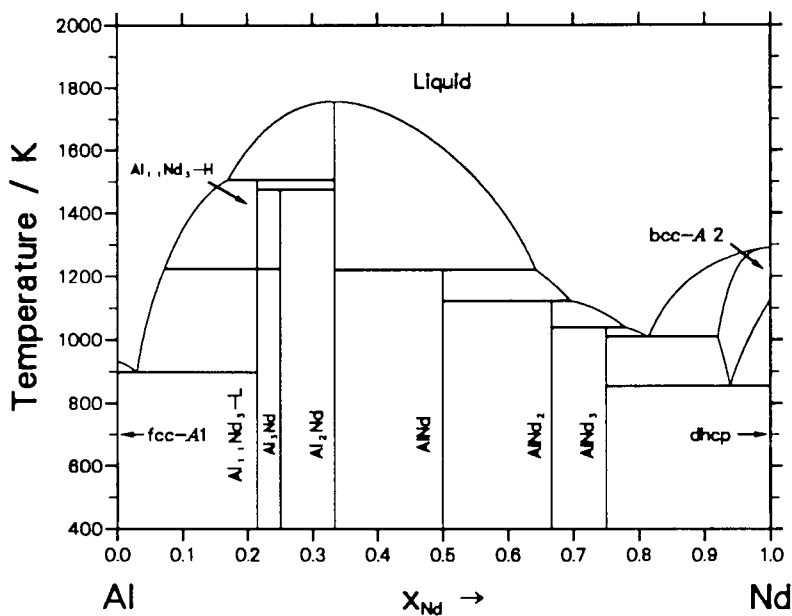


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Nd}	T / K
Liquid \rightleftharpoons Al ₁₁ Nd ₃ -L + fcc-Al	Eutectic	.030 .000 .214	898.6
Liquid + Laves-C15* \rightleftharpoons Al ₁₁ Nd ₃ -H	Peritectic	.170 .333 .214	1506.6
Al ₁₁ Nd ₃ -H + Al ₂ Nd* \rightleftharpoons Al ₃ Nd	Peritectic	.214 .333 .250	1475.8
Liquid + AlNd \rightleftharpoons Al ₂ Nd	Peritectic	.643 0.500 .333	1220.3
Liquid + AlNd \rightleftharpoons AlNd ₂	Peritectic	.696 .500 .667	1122.2
Liquid + AlNd ₂ \rightleftharpoons AlNd ₃ -L	Peritectic	.780 .667 .750	1037.9
Liquid \rightleftharpoons AlNd ₃ -L + bcc-A2	Eutectic	.815 .750 .920	1008.9
bcc-A2 \rightleftharpoons AlNd ₃ -L + dhcp	Eutectoid	.939 .750 1.000	855.3
Al ₂ Nd \rightleftharpoons Liquid	Congruent	.333 .333 ...	1758.0
Al ₁₁ Nd ₃ -L \rightleftharpoons Al ₁₁ Nd ₃ -H	Polymorphic	.214 .214 ...	1224.7

* Laves-C15 \equiv Al₂Nd

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Nd	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Nd)	La- α	<i>hP4</i> <i>P6$_3$/mmc</i>	M 4	
	(Nd)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	Al ₁₁ Nd ₃ - α	Al ₁₁ La ₃ - α	<i>oI28</i> <i>Immm</i>		Al ₁₁ Nd ₃ -L
	Al ₁₁ Nd ₃ - β	Al ₄ Ba	<i>tI28</i> <i>I4/mmm</i>		Al ₁₁ Nd ₃ -II
	Al ₃ Nd	Ni ₃ Sn	<i>hP8</i> <i>P6$_3$/mmc</i>		
	Al ₂ Nd	Cu ₂ Mg	<i>cF24</i> <i>Fd$\bar{3}m$</i>	Nd 8 Al 16	Laves-C15
	AlNd	AlEr	<i>oP16</i> <i>Pmma</i>	Al 1 Nd 1	
	AlNd ₂	Co ₂ Si	<i>oP12</i> <i>Pnma</i>	Al 1 Nd 3	
	AlNd ₃	Ni ₃ Sn	<i>hP8</i> <i>P6$_3$/mmc</i>	Al 1 Nd 3	

System Al-Si

Solution Phases:

(stable) Liquid, fcc-A1
 (metastable) hcp-A3

Modelling:

Liquid : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 diamond : Substitutional, Redlich-Kister

Assessor and Date:

J. Gröbner, H.-L. Lukas, and F. Aldinger.

Publication:

Calphad, **20**, 2 (1996) 247-254.

Thermodynamic properties of the solution phases(J.mol⁻¹)

Phase fcc-A1

$$I_{Al,Si;\square}^{0, fcc-A1} = -3143.78 + 0.39297 T$$

Phase hcp-A3

$$I_{Al,Si;\square}^{0, hcp-A3} = -3143.78 + 0.39297 T$$

Phase diamond

$$I_{Al,Si}^{0, diamond} = 113246.16 - 47.5551 T$$

Phase liquid

$$I_{Al,Si}^{0, liquid} = -11340.1 - 1.23394 T$$

$$I_{Al,Si}^{1, liquid} = -3530.93 + 1.35993 T$$

$$I_{Al,Si}^{2, liquid} = 2265.39$$

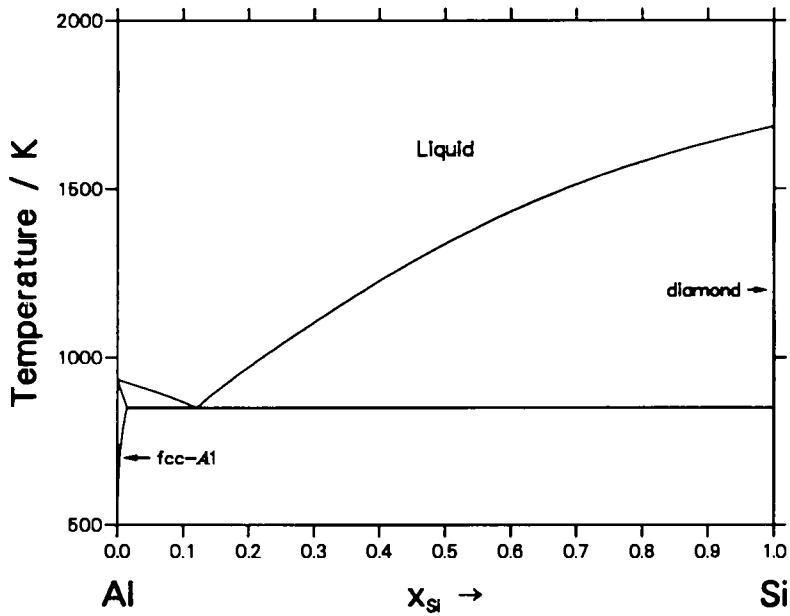


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Si}	T / K
Liquid \rightleftharpoons fcc-Al + diamond	Eutectic	.122 .016 1.000	850.1

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Al-Si	(Al)	Cu	$cF4$ $Fm\bar{3}m$
	(Si)	diamond	$cF8$ $Fd\bar{3}m$

System Al-Sn

Solution Phases:

(stable) Liquid, fcc-A1, bct-A5
 (metastable) : hcp-A3

Modelling:

Liquid : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 bct-A5 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister

Assessor and Date:

S. Fries, and H.L. Lukas,

Publication:

"Cost507 New Light Alloys", Leuven Proceedings,
 Ed. G. Effenberg (1991)

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bct-A5

$$L_{Al,Sn}^{0,bct-A5} = 14136.95 - 4.71231 T$$

Phase fcc-A1

$$L_{Al,Sn;\square}^{0,fcc-A1} = 45297.84 - 8.39814 T$$

Phase hcp-A3

$$L_{Al,Sn;\square}^{0,hcp-A3} = 0.00001$$

Phase liquid

$$L_{Al,Sn}^{0,liquid} = 16329.85 - 4.98306 T$$

$$L_{Al,Sn}^{1,liquid} = 4111.97 - 1.15145 T$$

$$L_{Al,Sn}^{2,liquid} = 1765.43 - 0.57390 T$$

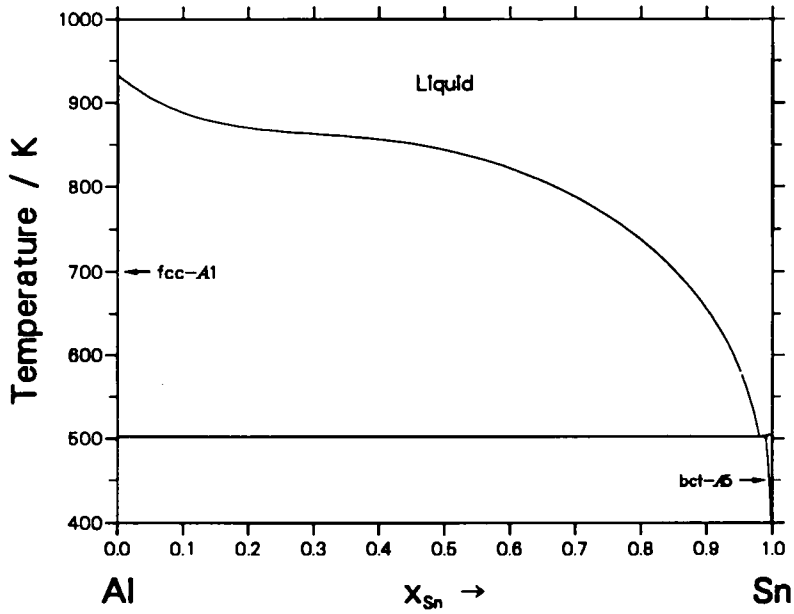


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Sn}	T / K
Liquid \rightleftharpoons fcc-Al + bct-Sn	Eutectic	.980 .000 .990	502.4

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Al-Sn	(Al)	Cu	$cF4$ $Fm\bar{3}m$
	(Sn)	β -Sn	$tI4$ $I4_1/amd$

System Al-Ta

Solution Phases:

(stable) Liquid, bcc-A2, fcc-A1
 (metastable) bcc-B2, hcp-A3

Compounds :

(stable) AlM-D0₂₂, σ
 (metastable) AlTi-L1₀, AlM-D0₁₉

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 bcc-B2 : Sublattice model, (Al,Ta)_{0.5}(Al,Ta)_{0.5}(\square)₃
 The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 \rightleftharpoons bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.

AlM-D0₁₉ : Sublattice model, (Al,Ta)₃(Al,Ta)(\square)
 AlM-D0₂₂ : Sublattice model, (Al)₃(Ta)
 σ : Sublattice model, (Al)₈(Ta)₄(Al,Ta)₁₈
 AlTi-L1₀ : Sublattice model, (Al,Ta)_{0.5}(TaTa)_{0.5}

Assessor and Date:

N. Saunders, 1997.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlM-D0₂₂

$$G^{\circ}(T) - 3.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = -130456 + 23 T + 3.0 \text{ GHSE}_{\text{Al}} + \text{GHSE}_{\text{Ta}}$$

Phase Al₃Ta₂-H

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 145000 + 17.325 T + 3.0 \text{ GHSE}_{\text{Al}} + 2.0 \text{ GHSE}_{\text{Ta}}$$

Phase Al₃Ta₂-L

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 155000 + 24 T + 3.0 \text{ GHSE}_{\text{Al}} + 2.0 \text{ GHSE}_{\text{Ta}}$$

Phase AlM-D0₁₉

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al}:\text{Al}:\square) = 4.0 \text{ GHCP}_{\text{Al}}$$

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al}:\text{Ta}:\square) = \\ - 96000 + 22.52 T + 3 \text{ GHCP}_{\text{Al}} + \text{GHCP}_{\text{Ta}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta}:\text{Al}:\square) = \\ - 96000 + 22.52 T + \text{GHCP}_{\text{Al}} + 3 \text{ GHCP}_{\text{Ta}}$$

$$G^\circ(T) - 4 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta}:\text{Ta}:\square) = 4 + 4 \text{ GHCP}_{\text{Ta}}$$

$$L_{\text{Al},\text{Ta}:\text{Al}:\square}^{0,\text{AlM-D0}_{19}} = - 200000 + 60 T$$

$$L_{\text{Al}:\text{Al},\text{Ta}:\square}^{0,\text{AlM-D0}_{19}} = - 66000 + 20 T$$

$$L_{\text{Ta}:\text{Al},\text{Ta}:\square}^{0,\text{AlM-D0}_{19}} = 8000$$

$$L_{\text{Al},\text{Ta}:\text{Ta}:\square}^{0,\text{AlM-D0}_{19}} = 20000$$

Phase σ

$$G^\circ(T) - 26 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 4 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al}:\text{Ta}:\text{Al}) = \\ - 300000 + 90 T + 26 \text{ GHSE}_{\text{Al}} + 4 \text{ GHSE}_{\text{Ta}}$$

$$G^\circ(T) - 8 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 22 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al}:\text{Ta}:\text{Ta}) = \\ - 657000 + 90 T + 8 \text{ GHSE}_{\text{Al}} + 22 \text{ GHSE}_{\text{Ta}}$$

$$L_{\text{Al}:\text{Ta}:\text{Al},\text{Ta}}^{0,\sigma} = - 1230000 + 450 T$$

$$L_{\text{Al}:\text{Ta}:\text{Al},\text{Ta}}^{1,\sigma} = 1.0\text{E-}4$$

$$L_{\text{Al}:\text{Ta}:\text{Al},\text{Ta}}^{2,\sigma} = 300000$$

Phase AlTi-L1₀

$$G^{\circ}(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 4 + 2.0 \text{ GHSER}_{\text{Al}}$$

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Ta}) =$$

$$- 71000 + 15.0 T + \text{GHSER}_{\text{Al}} + \text{GHFCC}_{\text{Ta}}$$

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Al}) =$$

$$- 71000 + 15.0 T + \text{GHSER}_{\text{Al}} + \text{GHFCC}_{\text{Ta}}$$

$$G^{\circ}(T) - 2 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Ta}) = 2 \text{ GFCC}_{\text{Ta}}$$

$$L_{\text{Al,Ta:Al}}^{0,\text{AlTi-L1}_0} = - 56000 + 20 T$$

$$L_{\text{Al,Ta:Al}}^{1,\text{AlTi-L1}_0} = 30000$$

$$L_{\text{Al,Ta:Al}}^{2,\text{AlTi-L1}_0} = 20000$$

$$L_{\text{Al:Al,Ta}}^{0,\text{AlTi-L1}_0} = - 56000 + 20 T$$

$$L_{\text{Al:Al,Ta}}^{1,\text{AlTi-L1}_0} = 30000$$

$$L_{\text{Al:Al,Ta}}^{2,\text{AlTi-L1}_0} = 20000$$

Phase bcc-A2

$$L_{\text{Al,Ta:}\square}^{0,\text{bcc-A2}} = - 89000 + 30 T$$

$$L_{\text{Al,Ta:}\square}^{1,\text{bcc-A2}} = - 5000$$

$$L_{\text{Al,Ta:}\square}^{2,\text{bcc-A2}} = 15000$$

Phase bcc-B2

$$G^{\circ}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 0$$

$$G^{\circ}(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Ta}) =$$

$$- 8250 + T$$

$$G^{\circ}(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Al}) =$$

$$- 8250 + T$$

$$G^{\circ}(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Ta}) = 0$$

$$L_{\text{Al:Al,Ta:}\square}^{0,\text{bcc-B2}} = 8250 - T$$

$$L_{\text{Ta:Al,Ta:}\square}^{0,\text{bcc-B2}} = 8250 - T$$

$$L_{\text{Al,Ta:Al:}\square}^{0,\text{bcc-B2}} = 8250 - T$$

$$L_{\text{Al,Ta:Al:}\square}^{0,\text{bcc-B2}} = 8250 - T$$

Phase bcc-B2

$$G_{\text{Al:Ta:}\square}^* = -8250 + T$$

$$G^\circ(T) - \frac{0}{\text{Al}}^{\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Ta}}^{\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Ta:}\square) = 2.0 \quad G_{\text{Al:Ta:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Ta}}^{\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ta:Al:}\square) = 2.0 \quad G_{\text{Al:Ta:}\square}^*$$

$$G^\circ(T) - H_{\text{Ta}}^{\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ta:Ta:}\square) = 0.0$$

bcc-A2

$$L_{\text{Al,Ta:}\square}^{0,\text{bcc-A2}} = -89000 + 30 T$$

$$L_{\text{Al,Ta:}\square}^{1,\text{bcc-A2}} = -5000$$

$$L_{\text{Al,Ta:}\square}^{2,\text{bcc-A2}} = 15000$$

Phase fcc-A1

$$L_{\text{Al,Ta:}\square}^{0,\text{fcc-A1}} = -100000 + 30 T$$

Phase hcp-A3

$$L_{\text{Al,Ta:}\square}^{0,\text{hcp-A3}} = -100000 + 30 T$$

Phase liquid

$$L_{\text{Al,Ta}}^{0,\text{liquid}} = -108000 + 30 T$$

$$L_{\text{Al,Ta}}^{1,\text{liquid}} = 6000$$

$$L_{\text{Al,Ta}}^{2,\text{liquid}} = 17000$$

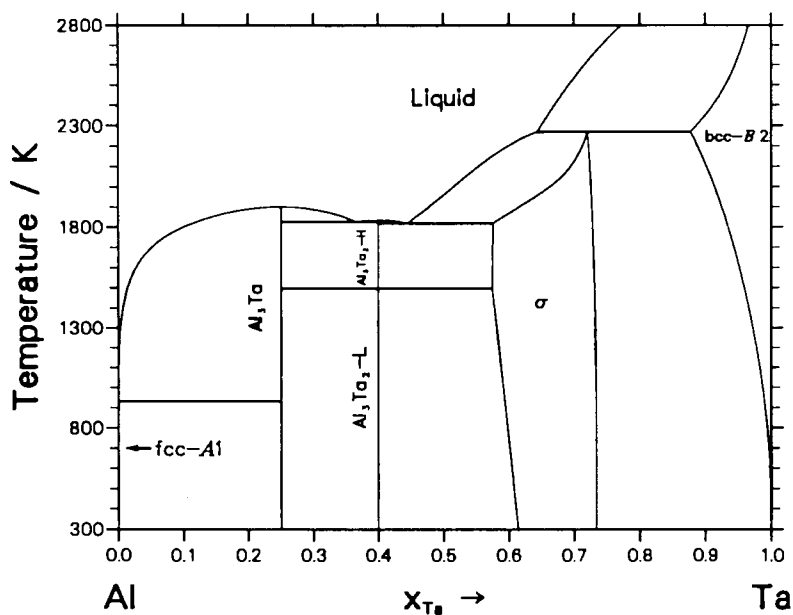


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Ta}	T / K
Liquid + $AlM-D0_{22}^*$ \rightleftharpoons fcc-Al	Peritectic	.00001 .250 .0008	934.0
Liquid \rightleftharpoons + $AlM-D0_{22}^*$ + Al_3Ta_2-II	Eutectic	.366 .250 .400	1826.8
Liquid \rightleftharpoons Al_3Ta_2-H \rightleftharpoons + σ	Eutectic	.444 .400 .576	1819.8
Liquid + bcc-A2 \rightleftharpoons σ	Peritectic	.643 .877 .720	2270.4
Al_3Ta^* \rightleftharpoons Liquid	Congruent	.250 .250 ...	1901.0
Al_3Ta_2-H \rightleftharpoons Al_3Ta_2-II	Polymorphic	.400 .400 ...	1498.1

* $AlM-D0_{22} \equiv Al_3Ta$

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Ta	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Ta)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	AlTa ₂	σ -CrFe	<i>tP30</i> <i>P4₂/mnm</i>	Al ₁ 2 Ta ₁ 4 Al ₂ 8 Ta ₂ 8 Ta ₃ 8	
	Al ₃ Ta	Al ₃ Ti	<i>tI8</i> <i>I4/m$\bar{m}3m$</i>	Ta 2 Al ₁ 2 Al ₁ 42	AlM-D0 ₂₂
	Al ₃ Ta ₂ -L		<i>o**</i>		
	Al ₃ Ta ₂ -II		<i>o*24</i>		

System Al-Ti

Solution Phases:

(stable) Liquid, bcc-A2, fcc-A1, hcp-A3, AlM-D0₁₉, AlTi-L1₀
 (metastable) bcc-B2

Compounds:

AlM-D0₂₂, Al₂Ti, Al₁₁Ti₅

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 bcc-B2 : Sublattice model, (Al,Ti)_{0.5}(Al,Ti)_{0.5}(□)₃
 The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 ⇌ bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
 hcp-A3 : Substitutional, Redlich-Kister
 AlM-D0₁₉ : Sublattice model, (Al,Ti)(Al,Ti)₃(□)_{0.5}
 L1₀-AlTi : Sublattice model, (Al,Ti)(Al,Ti)
 AlM-D0₂₂ : Stoichiometric, (Al)₃(Ti)
 Al₂Ti : Stoichiometric, (Al)₂(Ti)
 Al₁₁Ti₅ : Stoichiometric, (Al)₁₁(Ti)₅

Assessor and Date:

N. Saunders (1992)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlTi-L1₀

$$G^{\circ}(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al}) = 2.0 \text{ GHSER}_{\text{Al}}$$

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Al}) = -79644.0 + 19.2 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-\text{A3}}(298.15 \text{ K}) = G(\text{Al:Ti}) =$$

$$- 79644.0 + 19.2 T + \text{GHSE}_{\text{Al}} + \text{GHSE}_{\text{Ti}}$$

$$G^\circ(T) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-\text{A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 2.0 \text{ GFCCTi}$$

$$L_{\text{Al:Ti:Al}}^{0,\text{AlTi}-\text{L1}_0} = - 89892 + 44 T$$

$$L_{\text{Al:Ti:Al}}^{1,\text{AlTi}-\text{L1}_0} = 30000$$

$$L_{\text{Al:Ti:Al}}^{2,\text{AlTi}-\text{L1}_0} = 20000$$

$$L_{\text{Al:Al:Ti}}^{0,\text{AlTi}-\text{L1}_0} = - 89892 + 44 T$$

$$L_{\text{Al:Al:Ti}}^{1,\text{AlTi}-\text{L1}_0} = 30000$$

$$L_{\text{Al:Al:Ti}}^{2,\text{AlTi}-\text{L1}_0} = 20000$$

$$L_{\text{Ti:Al:Ti}}^{0,\text{AlTi}-\text{L1}_0} = - 15134 - 2.36 T$$

$$L_{\text{Al:Ti:Ti}}^{0,\text{AlTi}-\text{L1}_0} = - 15134 - 2.36 T$$

Phase AlM-D0₁₉

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 4.0 \text{ GHCPAl}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-\text{A3}}(298.15 \text{ K}) = G(\text{Ti:Al:}\square) =$$

$$- 110080 + 23.88 T + \text{GHSE}_{\text{Al}} + 3.0 \text{ GHSE}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-\text{A3}}(298.15 \text{ K}) = G(\text{Al:Ti:}\square) =$$

$$- 99120.0 + 32.28 T + 3.0 \text{ GHSE}_{\text{Al}} + \text{GHSE}_{\text{Ti}}$$

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-\text{A3}}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 4.0 \text{ GHSE}_{\text{Ti}}$$

$$L_{\text{Al:Ti:Al:}\square}^{0,\text{AlM}-\text{D0}_{19}} = - 298200 + 100 T$$

$$L_{\text{Al:Ti:Ti:}\square}^{0,\text{AlM}-\text{D0}_{19}} = 32000 - 4 T$$

$$L_{\text{Al:Al:Ti:}\square}^{0,\text{AlM}-\text{D0}_{19}} = - 98968 + 33.3 T$$

$$L_{\text{Ti:Al:Ti:}\square}^{0,\text{AlM}-\text{D0}_{19}} = 10656 - 1.332 T$$

Phase Al₂Ti

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-\text{A3}}(298.15 \text{ K}) =$$

$$- 121500 + 31.2 T + 2.0 \text{ GHSE}_{\text{Al}} + \text{GHSE}_{\text{Ti}}$$

Phase AlM-D0₂₂

$$\begin{aligned}
G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Al}:\text{Ti}) = \\
&- 144592.0 + 37.024 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ti}} \\
G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti}:\text{Ti}) = \\
\text{GFCC}_{\text{Ti}} \\
L_{\text{Al},\text{Ti}:\text{Ti}}^{\circ,\text{AlM-D0}_{22}} &= - 60000
\end{aligned}$$

Phase "Al₁₁Ti₅"

$$\begin{aligned}
G^\circ(T) - 17.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 8.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= \\
&- 971125.0 + 236.4 T + 17.0 \text{ GHSER}_{\text{Al}} + 8.0 \text{ GHSER}_{\text{Ti}}
\end{aligned}$$

Phase bcc-A2

$$\begin{aligned}
L_{\text{Al},\text{Ti}:\square}^{0,\text{bcc}-A2} &= - 128500 + 39 T \\
L_{\text{Al},\text{Ti}:\square}^{1,\text{bcc}-A2} &= 6000 \\
L_{\text{Al},\text{Ti}:\square}^{2,\text{bcc}-A2} &= 21200
\end{aligned}$$

Phase bcc-B2

$$\begin{aligned}
G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) &= G(\text{Al}:\text{Al}:\square) = 0 \\
G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Al}:\text{Ti}:\square) \\
&- 8750 + 1.25 T \\
G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Ti}:\text{Al}:\square) \\
&- 8750 + 1.25 T \\
G^\circ(T) - H_{\text{Ti}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Ti}:\text{Ti}:\square) = 0 \\
L_{\text{Al}:\text{Al},\text{Ti}:\square}^{0,\text{bcc}-B2} &= 8750 - 1.25 T \\
L_{\text{Ti}:\text{Al},\text{Ti}:\square}^{0,\text{bcc}-B2} &= 8750 - 1.25 T \\
L_{\text{Al},\text{Ti}:\text{Al}:\square}^{0,\text{bcc}-B2} &= 8750 - 1.25 T \\
L_{\text{Al},\text{Ti}:\text{Al}:\square}^{0,\text{bcc}-B2} &= 8750 - 1.25 T
\end{aligned}$$

Phase bcc-B2

$$G_{\text{Al,Ti:}\square}^* = -8750 + 1.25 T$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al:Ti:}\square) = 2.0 G_{\text{Al,Ti:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Al:}\square) = 2.0 G_{\text{Al,Ti:}\square}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Al,Ti:}\square}^{0,\text{bcc}-A2} = -128500 + 39 T$$

$$L_{\text{Al,Ti:}\square}^{1,\text{bcc}-A2} = 6000$$

$$L_{\text{Al,Ti:}\square}^{2,\text{bcc}-A2} = 21200$$

Phase fcc-A1

$$L_{\text{Al,Ti:}\square}^{0,\text{fcc}-A1} = -128970 + 39 T$$

$$L_{\text{Al,Ti:}\square}^{1,\text{fcc}-A1} = -5000$$

$$L_{\text{Al,Ti:}\square}^{2,\text{fcc}-A1} = 20000$$

Phase hcp-A3

$$L_{\text{Al,Ti:}\square}^{0,\text{hcp}-A3} = -133500 + 39 T$$

$$L_{\text{Al,Ti:}\square}^{1,\text{hcp}-A3} = 750.0$$

$$L_{\text{Al,Ti:}\square}^{2,\text{hcp}-A3} = 17500.0$$

Phase liquid

$$L_{Al,Ti}^{0,liquid} = -108250 + 38 T$$

$$L_{Al,Ti}^{1,liquid} = -6000 + 5 T$$

$$L_{Al,Ti}^{2,liquid} = 15000$$

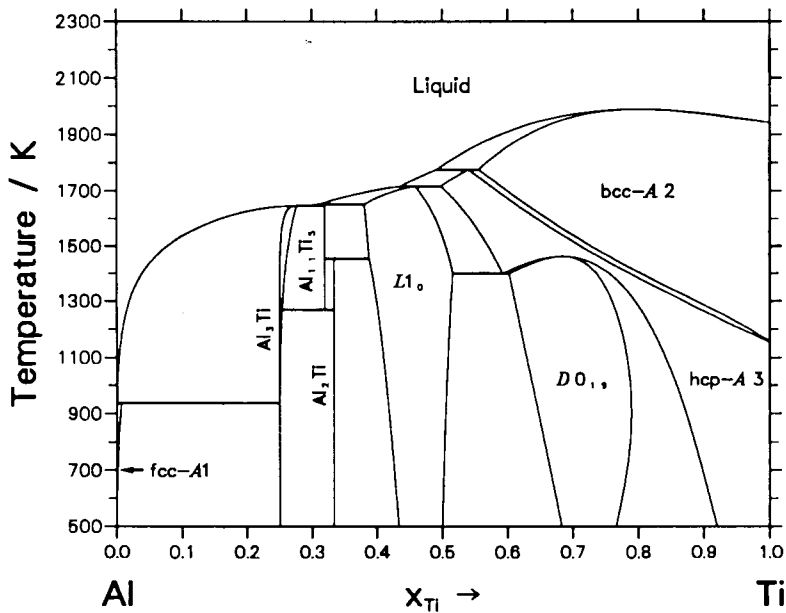


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Ti}	T / K
$Al_{11}Ti_5 + AlTi-L1_0 \rightleftharpoons Al_2Ti$	Peritectoid	.320 .388 .333	1454.3
$Al_{11}Ti_5 \rightleftharpoons AIM^* + Al_2Ti$	Eutectoid	.320 .250 .333	1259.8
$Liquid + Al_{11}Ti_5 \rightleftharpoons AIM-D0_{22}^*$	Peritectic	.247 .320 .250	1627.7
$Liquid + AIM-D0_{22}^* \rightleftharpoons fcc-A1$	Degenerate	.001 .250 .000	934.2
$Liquid + AlTi-L1_0 \rightleftharpoons Al_{11}Ti_5$	Peritectic	.310 .380 .320	1651.9
$Liquid + hcp-A3 \rightleftharpoons AlTi-L1_0$	Peritectic	.436 .498 .459	1716.7
$Liquid + bcc-A2 \rightleftharpoons hcp-A3$	Peritectic	.491 .555 .540	1775.9
$hcp-A3 \rightleftharpoons L1_0-AlTi + AIM-D0_{19}$	Eutectoid	.595 .518 .607	1384.4
$AIM-D0_{19} \rightleftharpoons hcp-A3$	Congruent	.682 .682	1452.0
$bcc-A2 \rightleftharpoons liquid$	Congruent	.788 .788	1989.0

* $AIM-D0_{22} \equiv Al_3Ti$

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	
Al-Ti	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Ti)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	AlTi	AuCu	<i>tP4</i> <i>P4/mmm</i>	Al 2 Ti ₁ 1 Ti ₂ 1	AlTi-L1 ₀
	AlTi ₃	Ni ₃ Sn	<i>hP8</i> <i>P6$_3$/mmc</i>		AlM-D0 ₁₉
	Al ₂ Ti	Ga ₂ Hf	<i>tI24</i> <i>I4$_1$/amd</i>		
	Al ₂ Ti- α	Ga ₂ Zr	<i>oC12</i> <i>Cmmm</i>		transformation not taken into account in [90Mas]
	Al ₃ Ti	Al ₃ Ti	<i>tI8</i> <i>I4/mmm</i>	Al ₁ 2 Al ₂ 4 Ti 2	AlM-D0 ₂₂
	Al ₅ Ti ₃		<i>tP32</i> <i>I4/mbm</i>		
	δ	Al ₃ Zr	<i>tI16</i>		Al ₁₁ Ti ₅ from [91Vil]
	Al ₅ Ti ₃		<i>tP32</i> <i>I4/mbm</i>		metastable

System Al-V

Solution Phases:

Liquid, bcc-A2, fcc-A1

Compounds:

Al₁₀V, Al₇V, Al₂₃V₄, AlM-D0₂₂, Al₈V₅

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
Al ₁₀ V	:	Stoichiometric, (Al) ₁₀ (V)
Al ₇ V	:	Stoichiometric, (Al) ₇ (V)
Al ₂₃ V ₄	:	Stoichiometric, (Al) ₂₃ (V) ₄
AlM-D0 ₂₂	:	Stoichiometric, (Al) ₃ (V)
Al ₈ V ₅	:	Stoichiometric, (Al) ₈ (V) ₅

Assessor and Date:

N. Saunders (1991)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₁₀V

$$G^\circ(T) - 10.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ - 111221 + 18.909 T + 10.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{V}}$$

Phase Al₂₃V₄

$$G^\circ(T) - 23.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 4.0 H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ - 430650 + 64.665 T + 23.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{V}}$$

Phase AlM-D0₂₂

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ - 104308.0 + 15.2 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{V}}$$

Phase Al₇V

$$G^\circ(T) - 7.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{V}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = -108800.0 + 16.8 T + 7.0 \text{ GHSE}_{\text{Al}} + \text{GHSE}_{\text{V}}$$

Phase Al₈V₅

$$G^\circ(T) - 8.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 5.0 H_{\text{V}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = -294320.0 - 13.0 T + 8.0 \text{ GHSE}_{\text{Al}} + 5.0 \text{ GHSE}_{\text{V}}$$

Phase bcc-A2

$$L_{\text{Al,V};\square}^{0,\text{bcc}-A2} = -95000 + 20 T$$

$$L_{\text{Al,V};\square}^{1,\text{bcc}-A2} = -6000$$

Phase fcc-A1

$$L_{\text{Al,V};\square}^{0,\text{fcc}-A1} = -69800 + 15 T$$

$$L_{\text{Al,V};\square}^{1,\text{fcc}-A1} = -8000$$

Phase liquid

$$L_{\text{Al,V}}^{0,\text{liquid}} = -50725 + 9 T$$

$$L_{\text{Al,V}}^{1,\text{liquid}} = -15000 + 8 T$$

Table I - Invariant Reactions.

Reaction	Type	Compositions <i>x_V</i>	<i>T</i> / K
Liquid + AlM-D0 ₂₂ * ⇌ Al ₂₃ V ₄	Peritectic	.003 .250 .148	1007.3
Liquid + Al ₂₃ V ₄ ⇌ Al ₇ V	Peritectic	.002 .148 .125	969.0
Liquid + Al ₇ V ⇌ Al ₁₀ V	Peritectic	.001 .125 .091	945.2
Liquid + Al ₁₀ V ⇌ fcc-A1	Peritectic	.000 .091 .001	935.3
Liquid + Al ₈ V ₅ ⇌ AlM-D0 ₂₂ *	Peritectic	.167 .384 .250	1640.1
Liquid + bcc-A2 ⇌ Al ₈ V ₅	Peritectic	.376 .471 .384	1932.7

* AlM-D0₂₂ ≡ Al₃V

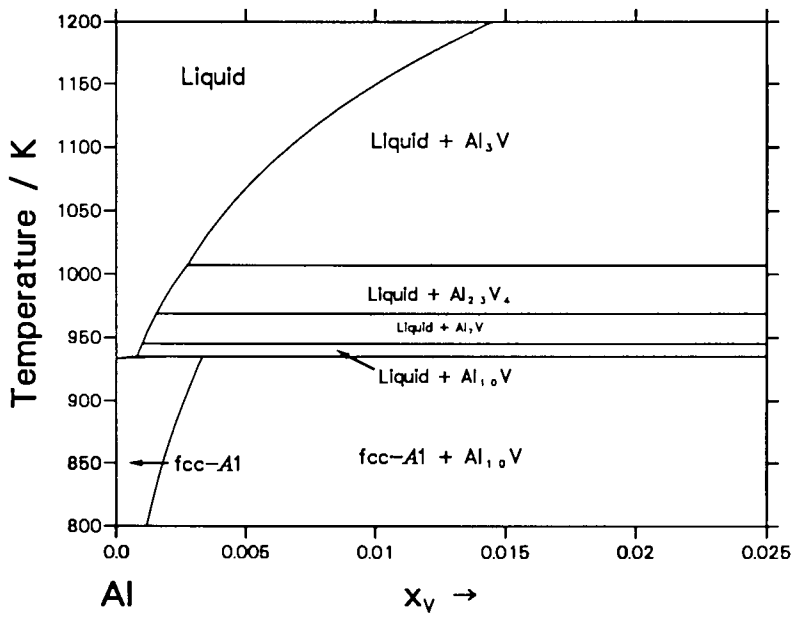
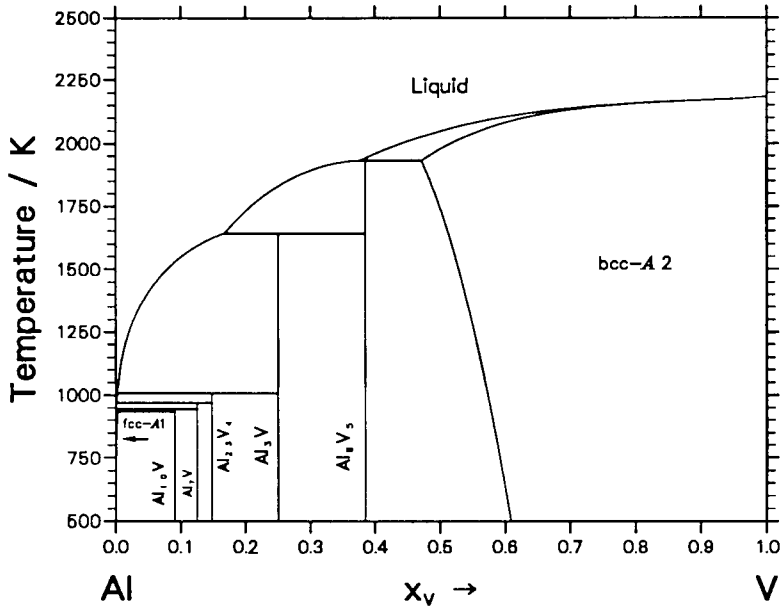


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-V	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(V)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	Al ₃ V	Al ₃ Ti	<i>tI8</i> <i>I4/mmm</i>	Al ₁ 2 Al ₂ 4 V 2	AlM-D0 ₂₂
	Al ₈ V ₅	Cu ₅ Zn ₈	<i>cI52</i> <i>I43m</i>	Al ₁ 24 M ₁ 8 M ₂ 12 V 8	
	Al ₂₁ V ₂	Al ₂₁ V ₂	<i>cF176</i> <i>Fd$\bar{3}m$</i>	Al ₁ 16 Al ₂ 48 Al ₃ 96 V 16	described as Al ₁₀ V
	Al ₂₃ V ₄	Al ₂₃ V ₄	<i>hP54</i> <i>P6₃/mmc</i>		
	Al ₄₅ V ₇	Al ₄₅ V ₇	<i>mC104</i> <i>C2/m</i>		described as Al ₇ V
	AlV ₃	Cr ₃ Si	<i>cP8</i> <i>Pm$\bar{3}n$</i>	Al 2 V 6	Al ₁₅ stable?

System Al-Y

Solution Phases:

Liquid, bcc-A2, fcc-A1, hcp-A3

Compounds:

Al₃Y, Al₂Y, AlY, Al₂Y₃, Al₃Y₅, AlY₂

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Al ₃ Y	:	Stoichiometric, (Al) ₃ (Y)
Al ₂ Y	:	Stoichiometric, (Al) ₂ (Y)
AlY	:	Stoichiometric, (Al)(Y)
Al ₂ Y ₃	:	Stoichiometric, (Al) ₂ (Y) ₃
Al ₃ Y ₅	:	Stoichiometric, (Al) ₃ (Y) ₅
AlY ₂	:	Stoichiometric, (Al)(Y) ₂

Assessor and Date:

H.L. Lukas, 1993

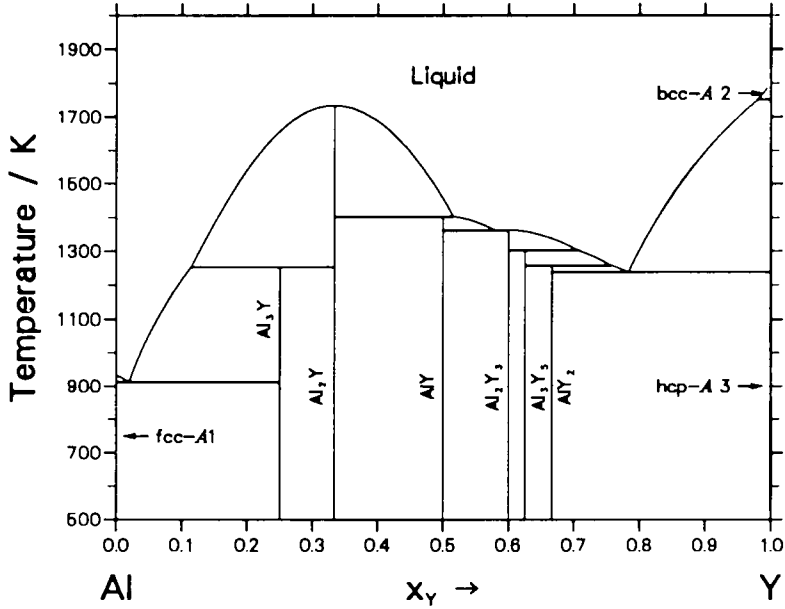
Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₂Y

$$G^{\circ}(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Y}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 246018.0 + 35.32809 T + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Y}}$$

Phase Al₂Y₃

$$G^{\circ}(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Y}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 373605.0 + 84.410 T + 2.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Y}}$$



Phase Al_3Y

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Y}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = -267460.0 + 46.48084 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Y}}$$

Phase Al_3Y_5

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 5.0 H_{\text{Y}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = -564479.2 + 127.7201 T + 3.0 \text{ GHSER}_{\text{Al}} + 5.0 \text{ GHSER}_{\text{Y}}$$

Phase AlY

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Y}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = -173810.0 + 40.86834 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Y}}$$

Phase AlY_2

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Y}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = -190908.0 + 44.38629 T + \text{GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Y}}$$

Phase bcc-A2

$$L_{Al,Y;\square}^{0,bcc-A2} = 90 T$$

Phase hcp-A3

$$L_{Al,Y;\square}^{0,hcp-A3} = 90 T$$

Phase liquid

$$L_{Al,Y}^{0,liquid} = -202611.28 + 4.63942 T$$

$$L_{Al,Y}^{1,liquid} = -54350.11 + 0.28402 T$$

$$L_{Al,Y}^{2,liquid} = 83347.01 - 34.76401 T$$

$$L_{Al,Y}^{3,liquid} = 15488.69 - 0.7988 T$$

$$L_{Al,Y}^{4,liquid} = -51205.9 + 30.2161 T$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_Y			T / K
Liquid \rightleftharpoons Al ₃ Y + fcc-A1	Eutectic	.020	.000	.250	913.0
Liquid + Al ₂ Y \rightleftharpoons Al ₃ Y	Peritectic	.114	.333	.250	1253.0
Liquid + Al ₂ Y \rightleftharpoons AlY	Peritectic	.516	.330	.500	1403.0
Liquid \rightleftharpoons AlY + Al ₂ Y ₃	Eutectic	.581	.500	.600	1361.2
Liquid + Al ₂ Y ₃ \rightleftharpoons Al ₃ Y ₅	Peritectic	.707	.600	.625	1302.5
Liquid + Al ₃ Y ₅ \rightleftharpoons AlY ₂	Peritectic	.757	.625	.666	1258.0
Liquid \rightleftharpoons AlY ₂ + hcp-A3	Eutectic	.667	.783	1.000	1239.0
hcp-A3 \rightleftharpoons bcc-A2	Allotropic	1.000	1.000	1752.0
Liquid \rightleftharpoons Al ₂ Y	Congruent	.333	.333	1734.0
Liquid \rightleftharpoons Al ₂ Y ₃	Congruent	.600	.600	1364.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Y	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Y)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2	
	(Y)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 4	
	Al ₃ Y- α	Ni ₃ Sn	<i>hP8</i> <i>P6$_3$/mmc</i>	Al 6 Y 2	
	Al ₃ Y- β	BaPb ₃	<i>hR12</i> <i>R$\bar{3}m$</i>	Al ₁ 9 Al ₂ 18 Y ₁ 3 Y ₂ 6	
	Al ₂ Y	Cu ₂ Mg	<i>cF24</i> <i>Fd$\bar{3}m$</i>	Al 16 Y 8	
	AlY	CrB	<i>oC8</i> <i>Cmcm</i>	Al 4 Y 4	
	Al ₂ Y ₃	Al ₂ Zr ₃	<i>tP20</i> <i>P4$_2$/mnm</i>	Al 8 Y ₁ 4 Y ₂ 4 Y ₃ 4	
	AlY ₂	Co ₂ Si	<i>oP12</i> <i>Pnma</i>	Al 4 Y ₁ 4 Y ₂ 4	
	AlY ₃	AuCu ₃	<i>cP4</i> <i>Pm$\bar{3}m$</i>	Al 1 Y 3	L1 ₂ metastable impurity stabilized [91Vit]?
	Al ₃ Y ₅	Mn ₅ Si ₃	<i>hP16</i> <i>P6$_3$/mcm</i>		

System Al-W

Solution Phases:

(stable) Liquid, bcc-A2, fcc-A1
 (metastable) bcc-B2, hcp-A3

Compounds:

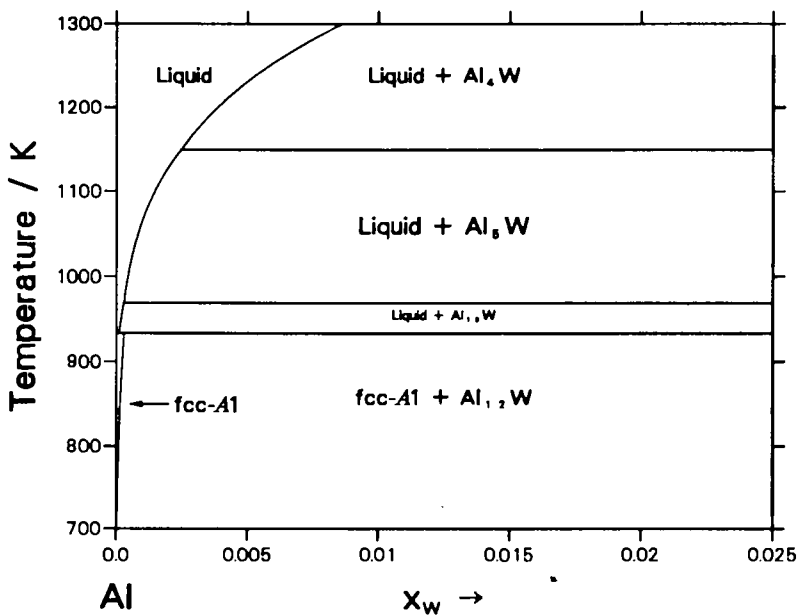
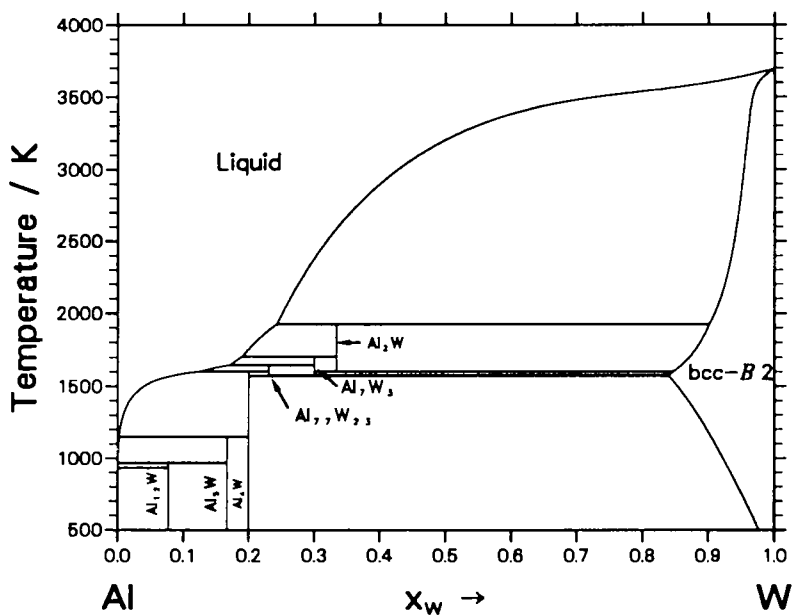
(stable) Al₁₂W, Al₄W, Al₅W, Al₇₇W₂₃, Al₇W₃, Al₂W
 (metastable) AlM-D0₁₉, AlTi-L1₀

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 Al₁₂W : Stoichiometric, (Al)₁₂(W)
 Al₅W : Stoichiometric, (Al)₅(W)
 Al₄W : Stoichiometric, (Al)₄(W)
 Al₇₇W₂₃ : Stoichiometric, (Al)₇₇(W)₂₃
 Al₇W₃ : Stoichiometric, (Al)₇(W)₃
 cub-A15 : Stoichiometric, (Al)(W)₃
 Al₂W : Sublattice model, (Al)₂(W)
 bcc-B2 : Sublattice model, (Al,W)_{0.5}(AlW)_{0.5}(□)₃
 The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 ⇌ bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
 AlM-D0₁₉ : Sublattice model, (Al,W)₃(Al,W)(□)_{0.5}
 AlTi-L1₀ : Sublattice model, (Al,W)(Al,W)

Assessor and Date:

N. Saunders, 1996.



Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase Al₁₂W**

$$G^\circ(T) - 12.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -62400 + 9.49 T + 12.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{W}}$$

Phase Al₄W

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -57500 + 9.73 T + 4.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{W}}$$

Phase Al₅W

$$G^\circ(T) - 5.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -58446 + 8.4 T + 5.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{W}}$$

Phase Al₂W

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ 13536 - 22.38 T + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{W}}$$

Phase Al₇₇W₂₃

$$G^\circ(T) - 77.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 23.0 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -189300 - 400 T + 77.0 \text{ GHSER}_{\text{Al}} + 23.0 \text{ GHSER}_{\text{W}}$$

Phase Al₇W₃

$$G^\circ(T) - 7.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ 34700 - 70 T + 7.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{W}}$$

Phase AlM-D0₁₉

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = \text{G(Al:Al)} = \\ 4.0 \text{ GHCP}_{\text{Al}} \\ G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \text{G(W:Al)} = \\ -12716 + 15.16 T + \text{GHCP}_{\text{Al}} + 3.0 \text{ GHCP}_{\text{W}} \\ G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \text{G(Al:W)} = \\ -12716 + 15.16 T + 3.0 \text{ GHCP}_{\text{Al}} + \text{GHCP}_{\text{W}} \\ G^\circ(T) - 4.0 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \text{G(W:W)} = \\ 4.0 \text{ GHSER}_{\text{W}}$$

Phase bcc-A2

$$L_{Al,W:\square}^{0,bcc-A2} = -27000 + 25 T$$

$$L_{Al,W:\square}^{1,bcc-A2} = -10000$$

Phase bcc-B2

$$G^{\circ}(T) - H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) = G(Al:Al:\square) = 0.0$$

$$G^{\circ}(T) - 0.5 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 0.5 H_{W}^{\circ, bcc-A2}(298.15 \text{ K}) = G(W:Al:\square) = 1.0E-4$$

$$G^{\circ}(T) - 0.5 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 0.5 H_{W}^{\circ, bcc-A2}(298.15 \text{ K}) = G(Al:W:\square) = 1.0E-4$$

$$G^{\circ}(T) - H_{W}^{\circ, bcc-A2}(298.15 \text{ K}) = G(W:W:\square) = 0.0$$

$$L_{Al:Al,W:\square}^{0,bcc-B2} = 1.0E-4$$

$$L_{Ta:Al,W:\square}^{0,bcc-B2} = 1.0E-4$$

$$L_{Al,W:Al:\square}^{0,bcc-B2} = 1.0E-4$$

$$L_{Al,W:Al:\square}^{0,bcc-B2} = 1.0E-4$$

Phase bcc-B2

$$G_{Al:W:\square}^* = 1.0E-4$$

$$G^{\circ}(T) - H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) = G(Al:Al:\square) = 0.0$$

$$G^{\circ}(T) - 0.5 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 0.5 H_{W}^{\circ, bcc-A2}(298.15 \text{ K}) = G(Al:W:\square) = 2.0 G_{Al:W:\square}^*$$

$$G^{\circ}(T) - 0.5 H_{Cu}^{\circ, fcc-A1}(298.15 \text{ K}) - 0.5 H_{W}^{\circ, bcc-A2}(298.15 \text{ K}) = G(W:Al:\square) = 2.0 G_{Al:W:\square}^*$$

$$G^{\circ}(T) - H_{W}^{\circ, bcc-A2}(298.15 \text{ K}) = G(W:W:\square) = 0.0$$

Phase bcc-A2

$$L_{Al,W:\square}^{0,bcc-A2} = -27000 + 25 T$$

$$L_{Al,W:\square}^{1,bcc-A2} = -10000$$

Phase fcc-A1

$$L_{Al,W;\square}^{0, fcc-A1} = -19250 + 20.2 T$$

$$L_{Al,W;\square}^{1, fcc-A1} = -10000$$

Phase hcp-A3

$$L_{Al,W;\square}^{0, hcp-A3} = -19250 + 20.2 T$$

$$L_{Al,W;\square}^{1, hcp-A3} = -10000$$

Phase liquid

$$L_{Al,W}^{0, liquid} = -70000 + 35 T$$

$$L_{Al,W}^{1, liquid} = 1.0E-4$$

$$L_{Al,W}^{2, liquid} = 15000$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_W	T / K
$Al_2W \rightleftharpoons Al_7W_3 + bcc-A2$	Eutectoid	.333 .300 .847	1602.6
Liquid + $Al_2W \rightleftharpoons Al_7W_3$	Peritectic	.190 .333 .300	1706.8
Liquid + $bcc-A2 \rightleftharpoons Al_2W$	Peritectic	.243 .901 .333	1925.7
Liquid + $Al_7W_3 \rightleftharpoons Al_{77}W_{23}$	Peritectic	.172 .300 .230	1648.2
Liquid + $Al_{77}W_{23} \rightleftharpoons Al_4W$	Peritectic	.125 .230 .200	1604.1
$Al_{77}W_{23} \rightleftharpoons Al_4W + bcc-A2$	Eutectoid	.023 .200 .840	1571.0
$Al_{77}W_{23} + bcc-A2 \rightleftharpoons Al_7W_3$	Eutectoid	.230 .841 .300	1580.0
Liquid + $Al_4W \rightleftharpoons Al_5W$	Peritectic	.0025 .200 .167	1149.6
Liquid + $Al_5W \rightleftharpoons Al_{12}W$	Peritectic	.0003 .167 .077	969.4
Liquid + $Al_{12}W \rightleftharpoons fcc-A$	Peritectic	.0002 .077 .0003	933.6
$Al_8W_3 \rightleftharpoons Liquid$	Congruent	.273 .273 ...	1850.5

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-W	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(W)	W	$cI2$ $Im\bar{3}m$	M 2	
	Al ₁₂ W	Al ₁₂ W	$cI26$ $Im\bar{3}$	Al 24 W 2	
	Al ₅ W	Al ₅ W	$hP12$ $P6_3$		
	Al ₄ W	Al ₄ W	$mC30$ Cm	Al ₁ 2 Al ₂ 2 W ₁ 2 Al ₃ 4 Al ₄ 4 Al ₅ 4 Al ₆ 4 Al ₇ 4 W ₂ 4	
	Al ₂ W				not quoted in [Mas1] nor in [Vill]
	Al ₇ W ₃				not quoted in [Mas1] nor in [Vill]
	Al ₇₇ W ₂₃				not quoted in [Mas1] nor in [Vill]

System Al-Zn

Solution Phases:

(stable) Liquid, fcc-Al, hcp-Zn
 (metastable) hcp-Al

Compounds:

(metastable) AlCu- η , Laves-C14

Modelling:

Liquid : Substitutional, Redlich-Kister
 fcc-Al : Substitutional, Redlich-Kister
 hcp-Al : Substitutional, Redlich-Kister
 hcp-Zn : Substitutional, Redlich-Kister
 AlCu- η : Stoichiometric, (Al)(Zn)
 Laves-C14 : Sublattice model, (Al,Zn)₂(Al,Zn)

Assessor and Date:

S. an Mey (1991)

Publication:

Z. für Metallkde, 84, 7, 451-455 (1993).

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase fcc-Al

$$L_{\text{Al,Zn};\square}^{0,\text{fcc-Al}} = 7297.48 + 0.47512 T$$

$$L_{\text{Al,Zn};\square}^{1,\text{fcc-Al}} = 6612.88 - 4.59110 T$$

$$L_{\text{Al,Zn};\square}^{2,\text{fcc-Al}} = -3097.19 + 3.30635 T$$

Phase hcp-A3

$$L_{Al,Zn:\square}^{0,hcp-A3} = 18820.95 - 8.95255 T$$

$$L_{Al,Zn:\square}^{1,hcp-A3} = 1.0E-6$$

$$L_{Al,Zn:\square}^{2,hcp-A3} = 1.0E-6$$

$$L_{Al,Zn:\square}^{3,hcp-A3} = -702.79$$

Phase hcp-Zn

$$L_{Al,Zn:\square}^{0,hcp-Zn} = 18820.95 - 8.95255 T$$

$$L_{Al,Zn:\square}^{1,hcp-Zn} = 1.0E-6$$

$$L_{Al,Zn:\square}^{2,hcp-Zn} = 1.0E-6$$

$$L_{Al,Zn:\square}^{3,hcp-Zn} = -702.79$$

Phase AlCu-η

$$G^\circ(T) - H_{Cu}^{o,fcc-Al}(298.15K) - H_{Zn}^{o,hcp-Zn}(298.15 K) = 15000.0 + GHSER_{Cu} + GHSER_{Zn}$$

Phase Laves-C14

$$G^\circ(T) - 3.0 H_{Cu}^{o,fcc-Al}(298.15K) = G(Al:Al) = 15000.0 + 3.0 GHSER_{Cu}$$

$$G^\circ(T) - 2.0 H_{Cu}^{o,fcc-Al}(298.15K) - H_{Zn}^{o,hcp-Zn}(298.15 K) = G(Al:Zn) = 15000.0 + 2.0 GHSER_{Cu} + GHSER_{Zn}$$

$$G^\circ(T) - H_{Cu}^{o,fcc-Al}(298.15K) - 2.0 H_{Zn}^{o,hcp-Zn}(298.15 K) = G(Zn:Al) = 15000.0 + GHSER_{Cu} + 2.0 GHSER_{Zn}$$

$$G^\circ(T) - 3.0 H_{Zn}^{o,hcp-Zn}(298.15 K) = G(Zn:Zn) = 15000.0 + 3.0 GHSER_{Zn}$$

$$L_{Al:Al,Zn:\square}^{0,Laves-C14} = L_{Zn:Al,Zn:\square}^{0,Laves-C14} = -7500 - 18 T$$

Phase liquid

$$L_{Al,Zn}^{0,liquid} = 10465.55 - 3.39259 T$$

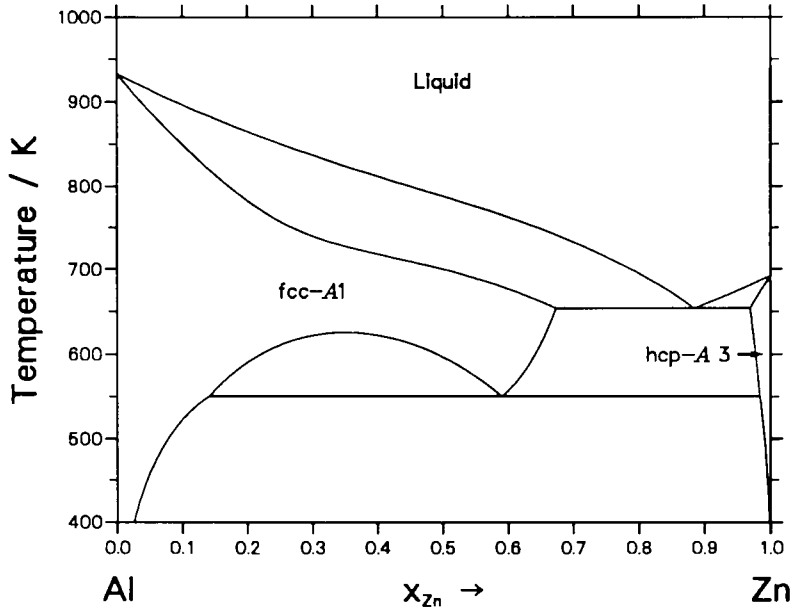


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zn}	T / K
Liquid \rightleftharpoons fcc-Al + hcp-A3	Eutectic	.884 .673 .969	654.0
fcc-Al' \rightleftharpoons fcc-Al'' + hcp-A3	Monotectic	.590 .141 .984	550.4

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Al-Zn	(Al)	Cu	$cF4$ $Fm\bar{3}m$
	(Zn)	Mg	$hP2$ $P6_3/mmc$

System Al-Zr

Solution Phases:

Liquid, bcc-A2, fcc-A1, hcp-A3

Compounds:

Al₂Zr, Al₂Zr₃, Al₃Zr, Al₃Zr₂, Al₃Zr₅,
Al₄Zr₅, AlZr, AlZr₂, AlZr₃

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Al ₂ Zr	:	Stoichiometric, (Al) ₂ (Zr)
Al ₂ Zr ₃	:	Stoichiometric, (Al) ₂ (Zr) ₃
Al ₃ Zr	:	Stoichiometric, (Al) ₃ (Zr)
Al ₃ Zr ₂	:	Stoichiometric, (Al) ₃ (Zr) ₂
Al ₃ Zr ₅	:	Stoichiometric, (Al) ₃ (Zr) ₅
Al ₄ Zr ₅	:	Stoichiometric, (Al) ₄ (Zr) ₅
AlZr	:	Stoichiometric, (Al)(Zr)
AlZr ₂	:	Stoichiometric, (Al)(Zr) ₂
AlZr ₃	:	Stoichiometric, (Al)(Zr) ₃

Assessor and Date:

N. Saunders (1991)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₂Zr

$$G^{\circ}T - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$- 137430.0 + 25.44 T + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Zr}}$$

Phase Al₂Zr₃

$$G^{\circ}T - 2.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$- 192135.0 + 33.0 T + 2.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Zr}}$$

Phase Al₃Zr

$$G^{\circ}T - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 162500.0 + 28.92 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Zr}}$$

Phase Al₃Zr₂

$$G^{\circ}T - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 234700.0 + 44.1 T + 3.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Zr}}$$

Phase Al₃Zr₅

$$G^{\circ}T - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 217488.0 + 48.72 T + 3.0 \text{ GHSER}_{\text{Al}} + 5.0 \text{ GHSER}_{\text{Zr}}$$

Phase Al₄Zr₅

$$G^{\circ}T - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 369000.0 + 62.55 T + 4.0 \text{ GHSER}_{\text{Al}} + 5.0 \text{ GHSER}_{\text{Zr}}$$

Phase AlZr

$$G^{\circ}T - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 89000.0 + 17.0384 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Zr}}$$

Phase AlZr₂

$$G^{\circ}T - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 100125.0 + 17.553 T + \text{GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Zr}}$$

Phase AlZr₃

$$G^{\circ}T - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 108000.0 + 22.38 T + \text{GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Zr}}$$

Phase bcc-A2

$$L_{\text{Al,Zr};\square}^{0,\text{bcc}-A2} = - 122300 + 32 T$$

$$L_{\text{Al,Zr};\square}^{1,\text{bcc}-A2} = - 11000$$

$$L_{\text{Al,Zr};\square}^{2,\text{bcc}-A2} = 15000$$

Phase fcc-A1

$$L_{\text{Al,Zr};\square}^{0,\text{fcc-A1}} = -120000 + 30 T$$

$$L_{\text{Al,Zr};\square}^{1,\text{fcc-A1}} = -10000$$

$$L_{\text{Al,Zr};\square}^{2,\text{fcc-A1}} = 15000$$

Phase hcp-A3

$$L_{\text{Al,Zr};\square}^{0,\text{hcp-A3}} = -122300 + 32 T$$

$$L_{\text{Al,Zr};\square}^{1,\text{hcp-A3}} = -8000$$

$$L_{\text{Al,Zr};\square}^{2,\text{hcp-A3}} = 17000$$

Phase liquid

$$L_{\text{Al,Zr}}^{0,\text{liquid}} = -125000 + 35 T$$

$$L_{\text{Al,Zr}}^{1,\text{liquid}} = -10000 + 5.57 T$$

$$L_{\text{Al,Zr}}^{2,\text{liquid}} = 15750$$

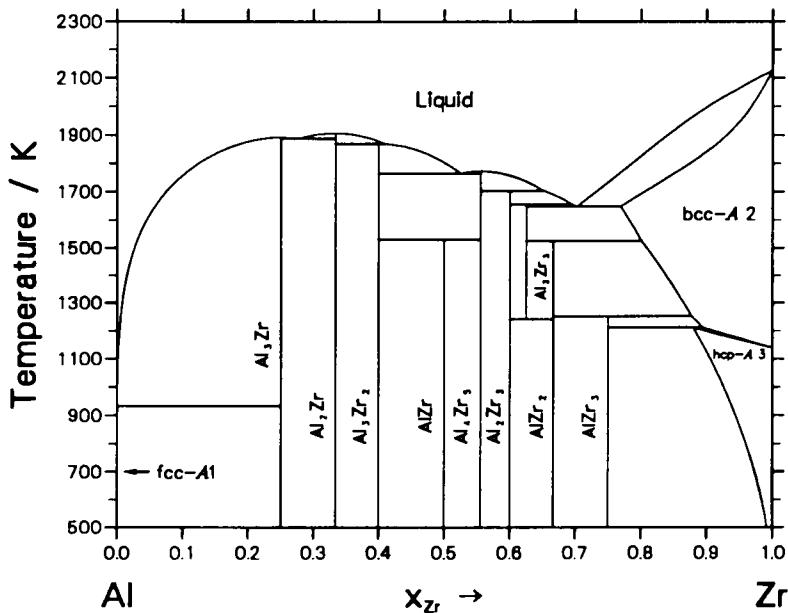


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zr}			T / K
Liquid \rightleftharpoons fcc-Al + Al ₃ Zr	Peritectic	.0002	.0008	.250	933.8
Al ₃ Zr \rightleftharpoons Liquid	Congruent	.250	.250	...	1893.0
Liquid \rightleftharpoons Al ₃ Zr + Al ₂ Zr	Eutectic	.277	.250	.333	1888.0
Al ₂ Zr \rightleftharpoons Liquid	Congruent	.333	.333	...	1907.0
Liquid + Al ₂ Zr \rightleftharpoons Al ₃ Zr ₂	Peritectic	.410	.333	.400	1869.1
Liquid \rightleftharpoons Al ₃ Zr ₂ + Al ₄ Zr ₅	Eutectic	.525	.400	.556	1765.3
Al ₄ Zr ₅ \rightleftharpoons Liquid	Congruent	.555	.555	...	1773.0
Liquid + Al ₄ Zr ₅ \rightleftharpoons Al ₂ Zr ₃	Peritectic	.653	.556	.600	1701.8
Liquid + Al ₂ Zr ₃ \rightleftharpoons Al ₃ Zr ₅	Peritectic	.696	.600	.625	1655.8
Liquid \rightleftharpoons Al ₃ Zr ₅ + bcc-A2	Eutectic	.702	.625	.768	1648.7
Al ₂ Zr ₃ + bcc-A2 \rightleftharpoons AlZr ₂	Peritectoid	.600	.801	.666	1524.2
Al ₃ Zr ₅ \rightleftharpoons Al ₂ Zr ₃ + AlZr ₂	Eutectoid	.625	.600	.666	1241.7
AlZr ₂ + bcc-A2 \rightleftharpoons AlZr ₃	Peritectoid	.667	.877	.750	1252.3
AlZr ₃ + bcc-A2 \rightleftharpoons hcp-A3	Peritectoid	.750	.894	.879	1212.2
Al ₃ Zr ₂ + Al ₄ Zr ₅ \rightleftharpoons AlZr	Peritectoid	.400	.556	.500	1529.5

Table II:a - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Zr	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	(Zr)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Zr)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M 4	
	AlZr	BCr	<i>oC8</i> <i>Cmcm</i>	Al 4 Zr 4	
	AlZr ₂	InNi ₂	<i>hP6</i> <i>P6₃/mmc</i>	Al 2 Zr ₁ 2 Zr ₂ 4	

Table II:b - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
	AlZr ₃	AuCu ₃	<i>cP4</i> <i>Pm3m</i>	Al 1 Zr 3	
	Al ₂ Zr	MgZn ₂	<i>hP12</i> <i>P6₃/mmc</i>		
	Al ₂ Zr ₃	Al ₂ Zr ₃	<i>tP20</i> <i>P4₂/mnm</i>	Al 8 Zr ₁ 4 Zr ₂ 4 Zr ₃ 4	
	Al ₃ Zr	Al ₃ r	<i>tI16</i> <i>I4/mmm</i>	Al ₁ 4 Al ₂ 4 Al ₃ 4 Zr 4	
	Al ₃ Zr ₂	Al ₃ Zr ₂	<i>oF40</i> <i>Fdd2</i>	Al ₁ 8 Al ₂ 16 Al ₃ 16	
	Al ₃ Zr ₄	Al ₃ Zr ₄	<i>hP7</i> <i>P6̄</i>	Al 3 Zr ₁ 1 Zr ₂ 1 Zr ₃ 2	
	Al ₃ Zr ₅	Mn ₅ Si ₃	<i>hP16</i> <i>P6₃/mcm</i>	Al 6 Zr ₁ 4 Zr ₂ 6	not in MasI
	Al ₃ Zr ₅	Si ₃ W ₅	<i>tI32</i> <i>I4/mcm</i>	Al ₁ 4 Al ₁ 8 Zr ₁ 4 Zr ₂ 16	
	Al ₄ Zr ₅	Ga ₄ Ti ₅	<i>hP18</i> <i>P6₃/mcm</i>	Al ₁ 2 Al ₂ 6 Zr ₁ 4 Zr ₂ 6	not in MasI

System B-C

Solution Phases:

Liquid, graphite, β -rhombo-B, B_4C

Modelling:

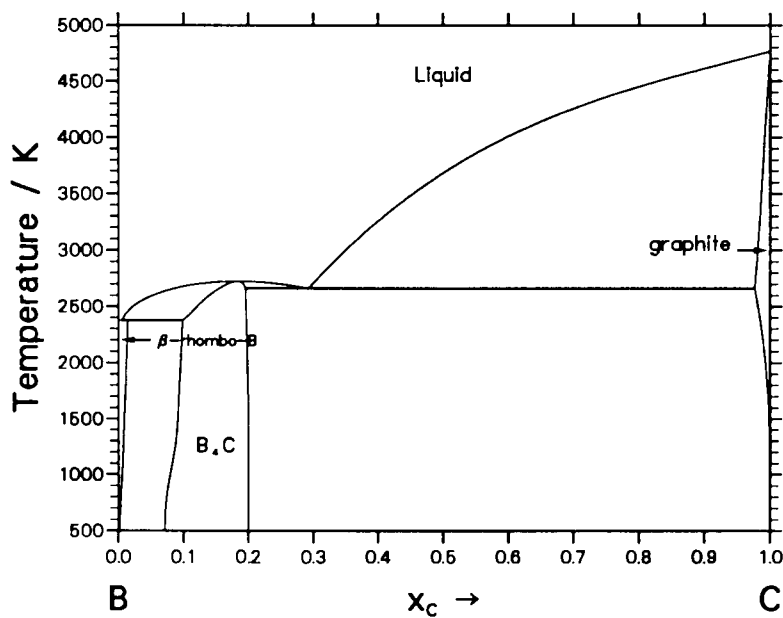
Liquid	:	Substitutional, Redlich-Kister
graphite	:	Substitutional, Redlich-Kister
β -rhombo-B	:	Sublattice model $(B)_{93}(B,C)_{12}$
B_4C	:	Sublattice model $(B_{11},B_{12})(B_2,C_2B,CB_2)$

Assessor and Date:

B. Kasper, H.L. Lukas, (1992).

Publication:

B. Kasper, Thesis, Univ. Stuttgart (Germany).



Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase B₄C

$$\begin{aligned}
 G^\circ(T) - 13.0 \quad H_B^{\circ,\beta\text{-rhombo-B}}(298.15 \text{ K}) - H_C^{\circ,\text{graphite}}(298.15 \text{ K}) &= G(\text{B}_{11}:\text{B}_2) = \\
 & -170978.12 + 22.909095 \quad T + 16.0 \quad \text{GHSER}_B + \text{GHSER}_C \\
 G^\circ(T) - 14.0 \quad H_B^{\circ,\beta\text{-rhombo-B}}(298.15 \text{ K}) &= G(\text{B}_{12}:\text{B}_2) = \\
 & 10000 + 22.909095 \quad T + 14.0 \quad \text{GHSER}_B \\
 G^\circ(T) - 12.0 \quad H_B^{\circ,\beta\text{-rhombo-B}}(298.15 \text{ K}) - 3.0 \quad H_C^{\circ,\text{graphite}}(298.15 \text{ K}) &= G(\text{B}_{11}:\text{C}_2\text{B}) = \\
 & -347121.82 + 22.909095 \quad T + 12.0 \quad \text{GHSER}_B + 3.0 \quad \text{GHSER}_C \\
 G^\circ(T) - 13.0 \quad H_B^{\circ,\beta\text{-rhombo-B}}(298.15 \text{ K}) - 2.0 \quad H_C^{\circ,\text{graphite}}(298.15 \text{ K}) &= G(\text{B}_{12}:\text{C}_2\text{B}) = \\
 & -294040.52 + 22.909095 \quad T + 13.0 \quad \text{GHSER}_B + 2.0 \quad \text{GHSER}_C \\
 G^\circ(T) - 13.0 \quad H_B^{\circ,\beta\text{-rhombo-B}}(298.15 \text{ K}) - 2.0 \quad H_C^{\circ,\text{graphite}}(298.15 \text{ K}) &= G(\text{B}_{11}:\text{CB}_2) = \\
 & -304040.52 + 22.909095 \quad T + 13.0 \quad \text{GHSER}_B + 2.0 \quad \text{GHSER}_C \\
 G^\circ(T) - 14.0 \quad H_B^{\circ,\beta\text{-rhombo-B}}(298.15 \text{ K}) - H_C^{\circ,\text{graphite}}(298.15 \text{ K}) &= G(\text{B}_{12}:\text{CB}_2) = \\
 & -169978.12 + 22.909095 \quad T + 14.0 \quad \text{GHSER}_B + \text{GHSER}_C \\
 I_{\text{B}_{11}\text{C,B}_{12}:\text{B}_2}^{0,\text{B}_4\text{C}} &= 1.0\text{E-}4
 \end{aligned}$$

Phase β -rhombo-B

$$\begin{aligned}
 G^\circ(T) - 105.0 \quad H_B^{\circ,\beta\text{-rhombo-B}}(298.15 \text{ K}) &= G(\text{B}:\text{B}) = \\
 & 105 \quad \text{GHSER}_B \\
 G^\circ(T) - 93.0 \quad H_B^{\circ,\beta\text{-rhombo-B}}(298.15 \text{ K}) - 12.0 \quad H_C^{\circ,\text{graphite}}(298.15 \text{ K}) &= G(\text{B}:\text{C}) = \\
 & 1000000 + 93.0 \quad \text{GHSER}_B + 12.0 \quad \text{GHSER}_C \\
 I_{\text{B}:\text{B,C}}^{0,\beta\text{-rhombo-B}} &= -2769690.3
 \end{aligned}$$

Phase graphite

$$I_{\text{B,C}}^{0,\text{graphite}} = 34385.95 + 8.6792 \quad T$$

Phase liquid

$$I_{\text{B,C}}^{0,\text{liquid}} = -67045.16 + 4.46969 \quad T$$

$$I_{\text{B,C}}^{1,\text{liquid}} = -36682.57 + 2.44551 \quad T$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_C	T / K
Liquid \rightleftharpoons B ₄ C + graphite	Eutectic	.292 .195 .977	2663.4
Liquid + B ₄ C \rightleftharpoons β -rhombo-B	Peritectic	.0056 .099 .010	2375.9
B ₄ C \rightleftharpoons Liquid	Congruent	.184 .184	2725.3

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
B-C	(B)	β -rhombo-B			
	(C)	graphite			
	B ₄ C	B ₄ C	<i>hR15</i> <i>R$\bar{3}m$</i>	B ₁ 3 B ₂ 18 B ₃ 18 C 6	B ₁₃ C ₂ in [91Vil]

System B–Hf

Solution Phases:

Liquid, bcc–A2, hcp–A3

Compounds:

(stable)

BHf, B₂Hf

(metastable)

B₄Hf₃

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc–A2	:	Substitutional, Redlich–Kister
hcp–A3	:	Substitutional, Redlich–Kister
BHf	:	Stoichiometric, (B)(Hf)
B ₂ Hf	:	Stoichiometric, (B) ₂ (Hf)
B ₄ Hf ₃	:	Stoichiometric, (B) ₄ (Hf) ₃

Assessor and Date:

II. Bitterman, Univ. Vienna, Austria

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase BHf

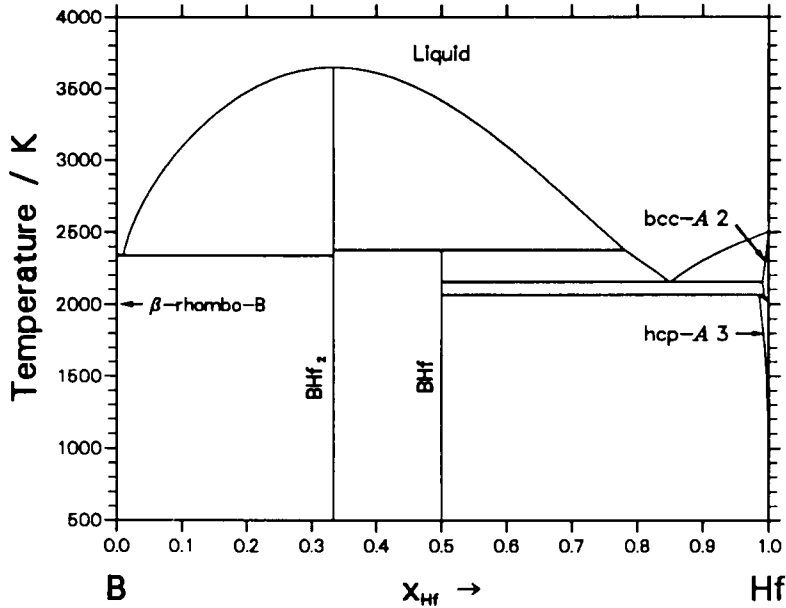
$$G^{\circ}(T) - H_{\text{B}}^{\circ, \beta\text{-rhomb-B}}(298.15\text{K}) - H_{\text{Hf}}^{\circ, \text{hcp-A3}}(298.15\text{K}) = \\ -159810 + 4.98602 T + \text{GHSER}_{\text{B}} + \text{GHSER}_{\text{Hf}}$$

Phase B₄Hf₃

$$G^{\circ}(T) - 4.0 H_{\text{B}}^{\circ, \beta\text{-rhomb-B}}(298.15\text{K}) - 3.0 H_{\text{Hf}}^{\circ, \text{hcp-A3}}(298.15\text{K}) = \\ -535000 - 14.5754 T + 4.0 \text{GHSER}_{\text{B}} + 3.0 \text{GHSER}_{\text{Hf}}$$

Phase B₂Hf

$$G^{\circ}(T) - 2.0 H_{\text{B}}^{\circ, \beta\text{-rhomb-B}}(298.15\text{K}) - H_{\text{Hf}}^{\circ, \text{hcp-A3}}(298.15\text{K}) = \\ -351445 + 469.146 T - 73.868 T \cdot \ln T - 0.0036789 T^2 \\ + 1517800 T^{-1} - 5.2\text{E}+09T^{-3}$$



Phase bcc-A2

$$G^{\circ}(T) - 3.0 H_B^{\circ, \beta\text{-rhombo-B}}(298.15\text{K}) - H_{\text{Hf}}^{\circ, \text{hcp-A3}}(298.15\text{K}) =$$

$$- 137926 + 3.0 \text{ GHSER}_B + \text{GHSER}_{\text{Hf}}$$

$$I_{\text{Hf:B},\text{O}}^{0, \text{bcc-A2}} = 1.0\text{E-4}$$

Phase hcp-A3

$$G^{\circ}(T) - 0.5 H_B^{\circ, \beta\text{-rhombo-B}}(298.15\text{K}) - H_{\text{Hf}}^{\circ, \text{hcp-A3}}(298.15\text{K}) =$$

$$- 44765.7 + 0.5 \text{ GHSER}_B + \text{GHSER}_{\text{Hf}}$$

$$I_{\text{Hf:B},\text{O}}^{0, \text{hcp-A3}} = 1.0\text{E-4}$$

Phase liquid

$$I_{\text{B,Hf}}^{0, \text{liquid}} = - 170625 - 4.85541 T$$

$$I_{\text{B,Hf}}^{1, \text{liquid}} = - 39128$$

$$I_{\text{B,Hf}}^{2, \text{liquid}} = 16331.1$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Hf}			T / K
Liquid \rightleftharpoons β -rhomb-B + B ₂ Hf	Eutectic	.010	.000	.333	2337.9
Liquid + B ₂ Hf \rightleftharpoons + BHf	Peritectic	.780	.333	.500	2377.1
Liquid \rightleftharpoons BHf + bcc-A2	Eutectic	.850	.500	.990	2153.6
bcc-A2 + BHf \rightleftharpoons hcp-A3	Peritectic	.993	.500	.985	2063.8
B ₂ Hf \rightleftharpoons Liquid	Congruent	.333	.333	3650.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
B-Hf	(B)	β -rhomb-B			
	(Hf)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Hf)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	BHf	BFe	<i>oP8</i> <i>Pnma</i>	B 4 Hf 4	
	B ₂ Hf	AlB ₂	<i>hP3</i> <i>P6/mmm</i>	B 2 Hf 1	
	B ₄ Hf ₃	B ₄ Ta ₃	<i>oI14</i> <i>Immm</i>		(metastable)

System B-N

Solution Phases:

Liquid, gas

Compound:

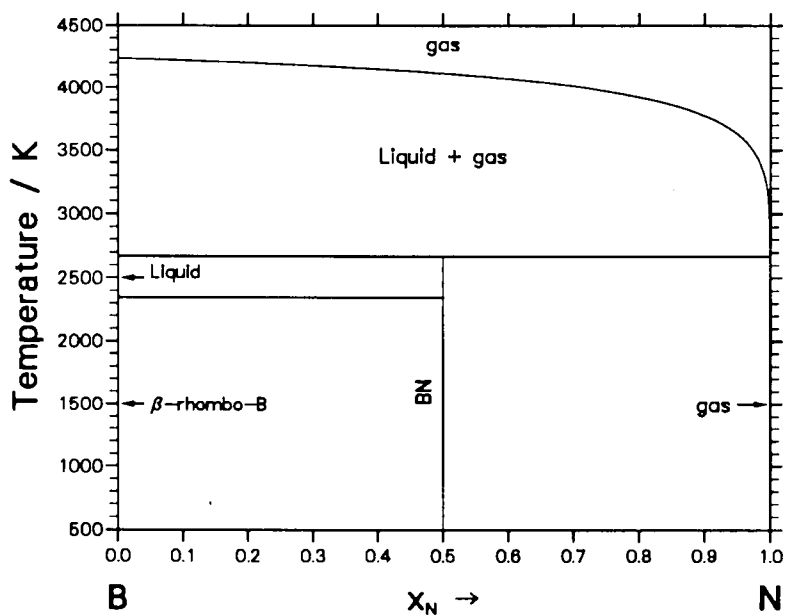
BN

Modelling:

Liquid : Substitutional, Redlich-Kister
gas : ideal (B, B₂, N, N₂, N₃, BN)
BN : Stoichiometric (B)(N)

Assessor and Date:

H. Wen, and H.L. Lukas 1992



Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase BN**

$$G^{\circ}(T) - H_{\text{B}}^{\circ,\beta\text{-rhombio-B}}(298.15 \text{ K}) - H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = \\ - 250600 + 91.281942 T + \text{GHSER}_{\text{B}} + \text{GHSER}_{\text{N}}$$

Phase liquid

$$L_{\text{B,N}}^{0,\text{liquid}} = 30000.0 - 4.0 T$$

Phase gas(B,B₂,N,N₂,N₃,BN) (P = 0.1MPa)

$$G_{\text{B}}^{\circ,\text{gas}}(T) - H_{\text{B}}^{\circ,\beta\text{-rhombio-B}} = R T \ln P + \\ 298.15 < T < 700.00 : 564913.402 - 13.9693124 T \\ + 1.6646044\text{E-}05 T^2 - 20.80858 T \cdot \ln T \\ 700.00 < T < 2800.00 : 564920.973 - 14.1156663 T - 20.786112 T \cdot \ln T \\ 2800.00 < T < 4075.00 : 565086.023 - 15.0515115 T - 20.6682069 T \cdot \ln T \\ - 2.10566\text{E-}05 T^2$$

$$G_{\text{B}_2}^{\circ,\text{gas}}(T) - 2.0 H_{\text{B}}^{\circ,\beta\text{-rhombio-B}} = R T \ln P + \\ 298.15 < T < 550.00 : 824867.604 - 125.766398 T - 8.168 T \cdot \ln T \\ - 0.0430888612 T^2 + 1.00098016\text{E-}05 T^3 \\ - 136465.972 T^{-1} \\ 550.00 < T < 2150.00 : 809306.765 + 132.643168 T - 48.851589 T \cdot \ln T \\ + 0.00423205742 T^2 - 3.22751598\text{E-}07 T^3 \\ + 980387.558 T^{-1} \\ 2150.00 < T < 6000.00 : 826793.716 + 32.6504991 T - 35.6295549 T \cdot \ln T \\ - 4.58209505\text{E-}04 T^2 + 1.70149264\text{E-}10 T^3 \\ - 3665441.32 T^{-1}$$

$$G_{\text{N}}^{\circ,\text{gas}}(T) - 2.0 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = R T \ln P + \\ 298.15 < T < 2950.00 : 466446.153 + 2788.78662 T^{-1} - 13.2660528 T \\ - 20.8939295 T \cdot \ln T + 8.4552092\text{E-}05 T^2 \\ - 1.00186856\text{E-}08 T^3 \\ 2950.00 < T < 6000.00 : 481259.023 - 7559107.28 T^{-1} - 52.4348889 T \\ - 16.3761342 T \cdot \ln T - 2.28373808\text{E-}04 T^2 \\ - 2.78997209\text{E-}08 T^3$$

$$G_{\text{N}_2}^{\circ,\text{gas}}(T) - 2.0 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = 2.0 \text{GHSER}_{\text{N}} + R T \ln P$$

$$G_{N_3}^{o, gas}(T) - 3.0 H_{0.5N_2}^{o, gas}(298.15 \text{ K}) = R T \ln P +$$

298.15 < T < 800.00 : 403075.636 - 14.3245228 T - 29.5595416 T · lnT
- 0.02413122 T² + 3.6156036E-06 T³
+ 55714.144 T⁻¹

800.00 < T < 2000.00 : 388937.207 + 158.809275 T - 55.404528 T · lnT
- 0.0026570492 T² + 1.9365644E-07 T³
+ 1536448.48 T⁻¹

2000.00 < T < 6000.00 : 380898.006 + 210.207464 T - 62.295576 T · lnT
+ 6.5726456E-06 T² - 7.868012E-10 T³
+ 3336949.2 T⁻¹

$$G_{BN}^{o, gas}(T) - H_B^{o, \beta\text{-rhombo-B}}(298.15 \text{ K}) - H_{0.5N_2}^{o, gas}(298.15 \text{ K}) = R T \ln P +$$

298.15 < T < 1000.00 : 469920.773 - 57.4937871 T - 22.339422 T · lnT
- 0.0105569014 T² + 1.41488236E-06 T³
- 69873.2184 T⁻¹

1000.00 < T < 3500.00 : 462619.822 + 28.1899597 T - 35.0100802 T · lnT
- 7.99851096E-04 T² + 1.10267925E-08 T³
+ 719942.972 T⁻¹

3500.00 < T < 6000.00 : 449529.29 + 65.7741362 T - 39.4662494 T · lnT
- 1.95814338E-04 T² - 9.14385307E-10 T³
+ 7491452 T⁻¹

Table I - Invariant Reactions.

Reaction	Type	Compositions x_N	T / K
Liquid + gas \rightleftharpoons BN	Peritectic-like	.000 1.000 .500	2670.0
Liquid \rightleftharpoons BN + gas	Degenerate	.000 .000 .500	2670.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
B-N	β -rhombo-B	β -rhombo-B	<i>hR108</i> <i>R$\bar{3}m$</i>	<i>hR105</i> in [91Vil]
	BN	<i>hP4</i> <i>P$\bar{6}_3mc$</i>	

System B–Si

Solution Phases:

Liquid, diamond, β -rhombo-B, B_nSi , B_3Si , B_6Si

Modelling:

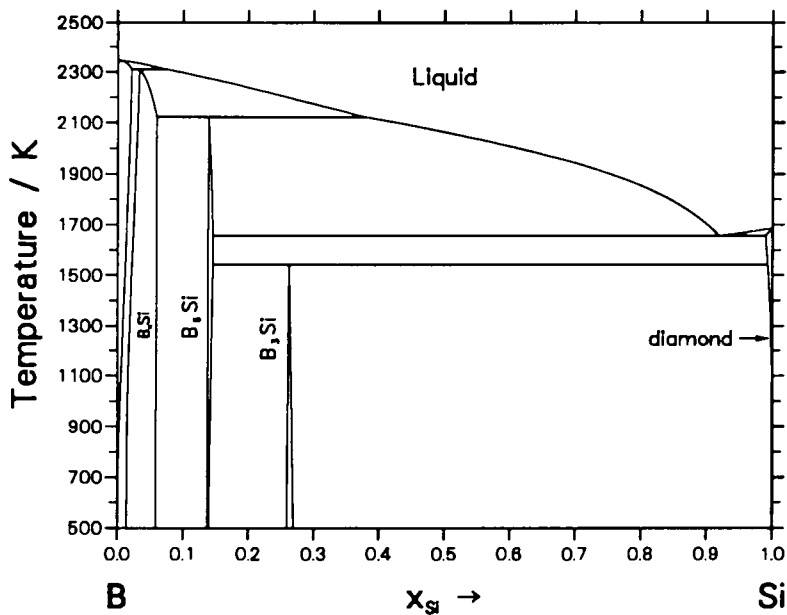
Liquid	:	Substitutional, Redlich–Kister
diamond	:	Substitutional, Redlich–Kister
β rhombo-B	:	Sublattice model $(B)_{93}(B,Si)_{12}$
B_nSi	:	Sublattice model $(B)_{61}(Si)(B,Si)_8$
B_3Si	:	Sublattice model $(B)_6(Si)_2(B,Si)_6$
B_6Si	:	Sublattice model $(B)_{210}(Si)_{23}(B,Si)_{48}$

Assessor and Date:

S. Fries, and H.L. Lukas,

Publication:

"Cost507 New Light Alloys", Leuven Proceedings,
Ed. G. Effenberg (1991)



Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase B₃Si**

$$G^{\circ}(T) - 12.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15 \text{ K}) - 2.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:B}) = 112000 + 12.0 \text{ GHSER}_{\text{B}} + 2.0 \text{ GHSER}_{\text{Si}}$$

$$G^{\circ}(T) - 6.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15 \text{ K}) - 8.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:Si}) = 112000 + 6.0 \text{ GHSER}_{\text{B}} + 8.0 \text{ GHSER}_{\text{Si}}$$

$$L_{\text{B:Si:B, Si}}^{0, \text{B}_3\text{Si}} = -2400475 + 240.0475 T$$

Phase B₆Si

$$G^{\circ}(T) - 258.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15 \text{ K}) - 23.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:B}) = 729824.4 - 72.98244 T + 258.0 \text{ GHSER}_{\text{B}} + 23.0 \text{ GHSER}_{\text{Si}}$$

$$G^{\circ}(T) - 210.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15 \text{ K}) - 71.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:Si}) = 5454560 - 545.456 T + 210.0 \text{ GHSER}_{\text{B}} + 71.0 \text{ GHSER}_{\text{Si}}$$

$$L_{\text{B:Si:B, Si}}^{0, \text{B}_6\text{Si}} = -15715630 + 1571.563 T$$

Phase B_nSi

$$G^{\circ}(T) - 69.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:B}) = -89819.86 + 8.981986 T + 69.0 \text{ GHSER}_{\text{B}} + \text{GHSER}_{\text{Si}}$$

$$G^{\circ}(T) - 61.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15 \text{ K}) - 9.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:Si}) = -176659.7 + 17.66597 T + 61.0 \text{ GHSER}_{\text{B}} + 9.0 \text{ GHSER}_{\text{Si}}$$

$$L_{\text{B:Si:B, Si}}^{0, \text{B}_n\text{Si}} = -281573.6 + 28.15736 T$$

Phase β -rhomb-B

$$G^{\circ}(T) - 93.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15 \text{ K}) - 12.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{B:Si}) = -6160.245 + 0.6160245 T + 93.0 \text{ GHSER}_{\text{B}} + 12.0 \text{ GHSER}_{\text{Si}}$$

$$L_{\text{B:B, Si}}^{0, \beta\text{-rhomb}\text{-B}} = -725614.0 + 72.5614 T$$

Phase diamond

$$L_{\text{B, Si:}\square}^{0, \text{diamond}} = 57978.16$$

Phase liquid

$$L_{\text{B, Si}}^{0, \text{liquid}} = 17631.92 - 1.76321 T$$

$$L_{\text{B, Si}}^{1, \text{liquid}} = -3526.99 + 0.3527 T$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Si}			T / K
$B_6Si + \text{diamond} \rightleftharpoons B_3Si$	Peritectoid	.145	.993	.262	1543.0
Liquid $\rightleftharpoons B_6Si + \text{diamond}$	Eutectic	.919	.146	.989	1657.6
Liquid + $B_nSi \rightleftharpoons B_6Si$	Peritectic	.379	.059	.138	2123.0
Liquid + β -rhombo-B $\rightleftharpoons B_nSi$	Peritectic	.074	.021	.033	2310.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
B-Si	(B)	β -rhombo-B			
	(Si)	diamond	<i>cF8</i> <i>Fd$\bar{3}m$</i>	M 8	
	B_nSi	B	<i>hR12</i> <i>P$\bar{3}m$</i>		
	B_3Si	B_4C	<i>hR15</i> <i>R$\bar{3}m$</i>	B 18 M 18 Si ₁ 6 Si ₂ 3	<i>hR14</i> in [91Vil]
	B_6Si	B_6Si	<i>oP280</i> <i>Pnm</i>		<i>oP340</i> in [Vil91]

System B–Ti

Solution Phases:

Liquid, bcc-A2, hcp-A3

Compounds:

BTi, B₄Ti₃, B₂Ti

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
BTi	:	Stoichiometric, (B)(Ti)
B ₄ Ti ₃	:	Stoichiometric, (B) ₄ (Ti) ₃
B ₂ Ti	:	Stoichiometric, (B) ₂ (Ti)

Assessor and Date:

C. Bätzner, June 1994

Publication:

Thesis, Univ. Stuttgart, Germany (1994)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase BTi

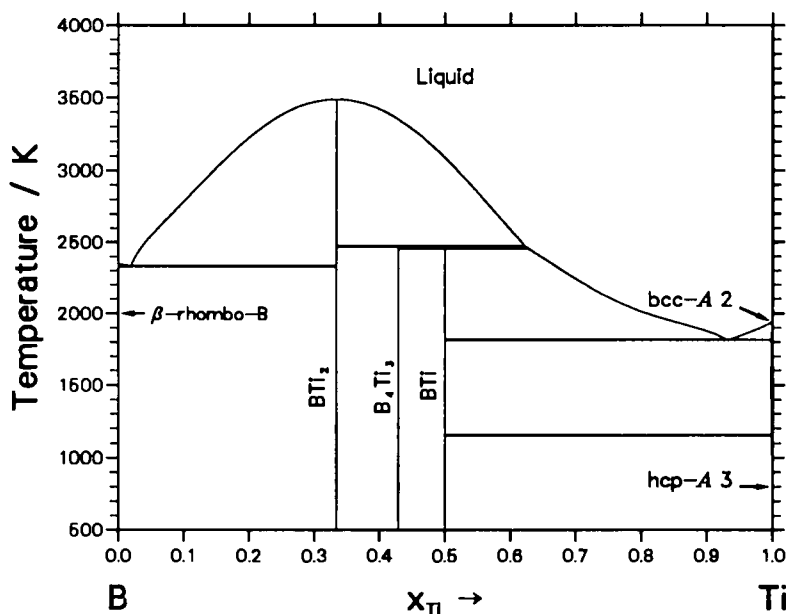
$$G^{\circ}(T) - H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15\text{K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15\text{K}) = \\ - 166196.8 + 3.2968 T + \text{GHISER}_{\text{B}} + \text{GHISER}_{\text{Ti}}$$

Phase B₄Ti₃

$$G^{\circ}(T) - 4.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15\text{K}) - 3.0 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15\text{K}) = \\ - 660745.8 + 4.3472923 T + 2.162216 T \cdot \ln T \\ + 4.0 \text{GHISER}_{\text{B}} + 3.0 \text{GHISER}_{\text{Ti}}$$

Phase B₂Ti

$$G^{\circ}(T) - 2.0 H_{\text{B}}^{\circ, \beta\text{-rhomb}\text{-B}}(298.15\text{K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15\text{K}) = \\ - 318253.47 - 2.5557 T + 0.799221 T \cdot \ln T \\ + 0.002843367 T^2 + 2.0 \text{GHISER}_{\text{B}} + \text{GHISER}_{\text{Ti}}$$



Phase bcc-A2

$$G^{\circ}(T) - 3.0 H_B^{\circ, \beta\text{-rhombo-B}}(298.15\text{K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15\text{K}) =$$

$$- 200000 + 14.0 T + 3.0 \text{ GHSER}_B + \text{GHSER}_{\text{Ti}}$$

$$L_{\text{Ti};B,\square}^{0, \text{bcc-A2}} = - 260162.96 + 156.48207 T$$

Phase hcp-A3

$$G^{\circ}(T) - 0.5 H_B^{\circ, \beta\text{-rhombo-B}}(298.15\text{K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15\text{K}) =$$

$$- 50000 + 15.0 T + 0.5 \text{ GHSER}_B + \text{GHSER}_{\text{Ti}}$$

$$L_{\text{Ti};B,\square}^{0, \text{hcp-A3}} = - 21213.442$$

Phase liquid

$$L_{B,\text{Ti}}^{0, \text{liquid}} = - 265414.4 + 15.543418 T$$

$$L_{B,\text{Ti}}^{1, \text{liquid}} = - 134303.03 + 17.709482 T$$

$$L_{B,\text{Ti}}^{2, \text{liquid}} = 61691.479$$

$$L_{B,\text{Ti}}^{3, \text{liquid}} = 52656.13$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Ti}			T / K
Liquid \rightleftharpoons β -rhombo-B + B ₂ Ti	Eutectic	.019	.000	.333	2332.5
Liquid + B ₂ Ti \rightleftharpoons B ₄ Ti ₃	Peritectic	.578	.333	.428	2474.0
Liquid + B ₄ Ti ₃ \rightleftharpoons BTi	Peritectic	.627	.428	.500	2456.0
Liquid \rightleftharpoons BTi + bcc-A2	Eutectic	.931	.500	.997	1814.1
bcc-A2 \rightleftharpoons BTi + hcp-A3	Transformation	.998	.500	1.000	1156.1
B ₂ Ti \rightleftharpoons Liquid	Congruent	.333	.333	3490.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	
B-Ti	(B)	β -rhombo-B			
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M	2
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M	2
	BTi	BFe	<i>oP8</i> <i>Pnma</i>	B	4
	B ₂ Ti	AlB ₂	<i>hP3</i> <i>P6/mmm</i>	B	2
	B ₄ Ti ₃	B ₄ Ta ₃	<i>oI14</i> <i>Immm</i>	Ti	1

System C–Si

Solution Phases:

Liquid, diamond

Compounds:

SiC, Si₄C₃ (metastable)

Modelling:

Liquid	:	Substitutional, Redlich–Kister
diamond	:	Substitutional, Redlich–Kister
SiC	:	Stoichiometric, (Si)(C)
Si ₄ C ₃	:	Stoichiometric, (Si) ₄ (C) ₃

Assessor and Date:

J. Gröbner, H. L. Lukas, and F. Aldinger.

Publication:

Calphad **20**, 2 (1996) 247-254.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase SiC

$$\begin{aligned}
 G^{\circ}(T) - H_C^{\circ,\text{graphite}}(298.15\text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15\text{ K}) = \\
 - 88583.96 + 271.1462 T - 41.27945 T \cdot \ln T \\
 - 0.00436266 T^2 + 2\text{E-}07 T^3 + 800000 T^{-1}
 \end{aligned}$$

Phase Al₄C₃ (metastable)

$$\begin{aligned}
 G^{\circ}(T) - 3.0 H_C^{\circ,\text{graphite}}(298.15\text{ K}) - 4.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15\text{ K}) = \\
 - 135043.86 + 949.01177 T - 144.478096 T \cdot \ln T \\
 - 0.01527 T^2 + 7\text{E-}07 T^3 + 2800000 T^{-1}
 \end{aligned}$$

Phase liquid

$$L_{\text{C,Si}}^{0,\text{liquid}} = 25644.97 - 6.381115 T$$

Phase diamond

$$L_{\text{C,Si}}^{0,\text{diamond}} = 93386.78$$

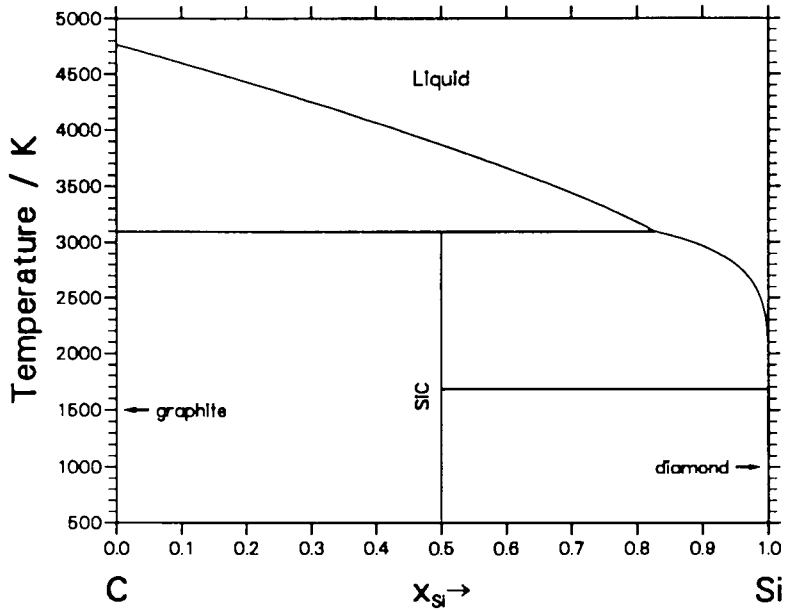


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Si}			T / K
Liquid \rightleftharpoons diamond + SiC	Degenerate	1.000	1.000	.500	1687.0
Liquid + graphite \rightleftharpoons SiC	Peritectic	.826	.000	.500	3096.4

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
C-Si	(C)	graphite		
	(Si)	diamond	$cF8$ $Fd\bar{3}m$	M 8
	SiC- β	ZnS (sphalerite)	$cF8$ $F\bar{4}3m$	C 4 Si 4

System C–Ti

Solution Phases:

Liquid, bcc–A2, fcc–A1, hcp–A3

Modelling:

Liquid : Substitutional, Redlich–Kister
 bcc–A2 : Sub-lattice, (Ti)(C,□)
 fcc–A1 : Sub-lattice, (Ti)(C,□)
 hcp–A3 : Sub-lattice, (Ti)(C,□)

Assessor and Date:

S. Jonsson

Publication:

Thesis, Royal Institute of Technology, Stockholm, Sweden (1993)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase fcc–A1

$$G^{\circ}(T) - H_{\text{C}}^{\circ,\text{graphite}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:C}) =$$

$$- 207709.0 + 307.438 T - 48.0195 T \cdot \ln T - 0.00272 T^2$$

$$- 2.03\text{E}+09 T^{-3} + 819000 T^{-1}$$

$$I_{\text{Ti:C}\square}^{0,\text{fcc-A1}} = - 85115 + 6.756 T$$

$$I_{\text{Ti:C}\square}^{1,\text{fcc-A1}} = - 129429 + 31.79 T$$

Phase bcc–A2

$$G^{\circ}(T) - 3.0 H_{\text{C}}^{\circ,\text{graphite}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:C})$$

$$2295533 + \text{GHSE}_{\text{TiC}} + 2.0 \text{GHSE}_{\text{C}}$$

$$I_{\text{Ti:C}\square}^{0,\text{bcc-A2}} = - 2590609$$

Phase hcp–A3

$$G^{\circ}(T) - 0.5 H_{\text{C}}^{\circ,\text{graphite}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:C})$$

$$- 1432 - 4.1241 T + 0.5 \text{GHSE}_{\text{TiC}} + 0.5 \text{GHSE}_{\text{C}}$$

Phase liquid

$$I_{\text{C,Ti}}^{0,\text{liquid}} = - 214678 - 14.314 T$$

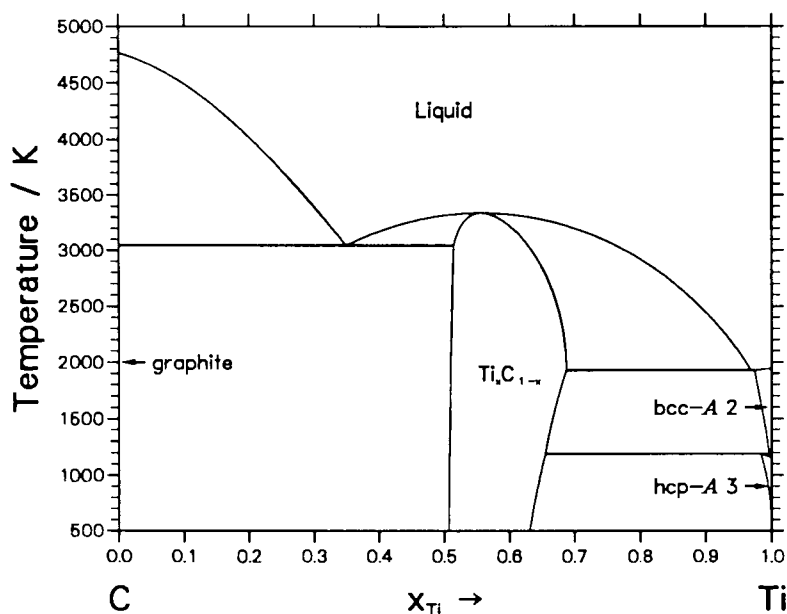


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Ti}	T / K
Liquid \rightleftharpoons fcc-A1* + bcc-A2	Eutectic	.968 .687 .974	1925.2
fcc-A1* + bcc-A2 \rightleftharpoons hcp-A3	Peritectoid	.655 .996 .984	1190.0
Liquid \rightleftharpoons graphite + fcc-A1	Eutectic	.349 .000 .515	3044.0
fcc-A1 \rightleftharpoons Liquid	Congruent	.554 .554 ...	3338.0

* fcc-A1 \equiv Ti_rC_{1-r}

Table II:a - Crystal Structure and Phase Description.

System	Phase	Structural Type	Pearson Symbol Space Group	Sub-lattices	Comments
C-Ti	(C)	graphite			
	(Ti)	Mg	$hP2$ $P6_3/mmc$	M 2	
	(Ti)	W	$I2$ $Im\bar{3}m$	M 2	

Table II:b - Crystal Structure and Phase Description.

System	Phase	Structural Type	Pearson Symbol Space Group	Sub-lattices	Comments
	CTi	CINa	<i>cF8</i> <i>Fm$\bar{3}m$</i>	M ₁ 4 M ₂ 4	
	CTi ₂	Ca ₃₃ Ge	<i>cF48</i> <i>Fd$\bar{3}m$</i>	C 16 Ti 32	Ca ₃₃ Ge in [91Vil] ord. TiC _{1-x} phase not considered

System Ce-Mg

Solution Phases:

Liquid, bcc-A2, fcc-A1, hcp-A3

Compounds:

CeMg, CeMg₂, CeMg₃, Ce₅Mg₄₁, Ce₂Mg₁₇, CeMg₁₂

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
CeMg	:	Stoichiometric, (Ce)(Mg)
CeMg ₂	:	Stoichiometric, (Ce)(Mg) ₂
CeMg ₃	:	Stoichiometric, (Ce)(Mg) ₃
Ce ₅ Mg ₄₁	:	Stoichiometric, (Ce) ₅ (Mg) ₄₁
Ce ₂ Mg ₁₇	:	Stoichiometric, (Ce) ₂ (Mg) ₁₇
CeMg ₁₂	:	Stoichiometric, (Ce)(Mg) ₁₂

Assessor and Date:

G. Cacciamani, A. Saccone, and R. Ferro,
Calphad XXII - Salou, Spain (1993).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Ce₂Mg₁₇

$$G^{\circ}(T) - 2.0 H_{\text{Ce}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 17.0 H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 217170.0 + 104.5 T + 2.0 \text{ GHSER}_{\text{Ce}} + 17.0 \text{ GHSER}_{\text{Mg}}$$

Phase Ce₅Mg₄₁

$$G^{\circ}(T) - 5.0 H_{\text{Ce}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 41.0 H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 575000.0 + 299.0 T + 5.0 \text{ GHSER}_{\text{Ce}} + 41.0 \text{ GHSER}_{\text{Mg}}$$

Phase CeMg

$$G^{\circ}(T) - H_{\text{Ce}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 46000.0 + 23.32 T + \text{GHSER}_{\text{Ce}} + \text{GHSER}_{\text{Mg}}$$

Phase CeMg₁₂

$$G^{\circ}(T) - H_{\text{Ce}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 12.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = -139880.0 + 84.5 T + \text{GHSER}_{\text{Ce}} + 12.0 \text{GHSER}_{\text{Mg}}$$

Phase CeMg₂

$$G^{\circ}(T) - H_{\text{Ce}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = -52744.6 + 15.163 T + \text{GHSER}_{\text{Ce}} + 2.0 \text{GHSER}_{\text{Mg}}$$

Phase CeMg₃

$$G^{\circ}(T) - H_{\text{Ce}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = -76800.0 + 26.5 T + \text{GHSER}_{\text{Ce}} + 3.0 \text{GHSER}_{\text{Mg}}$$

Phase bcc-A2

$$L_{\text{Ce,Mg};\square}^{0,\text{bcc}-A2} = -27000 + 3.3 T$$

$$L_{\text{Ce,Mg};\square}^{1,\text{bcc}-A2} = 25338.56 - 11.86885 T$$

$$L_{\text{Ce,Mg};\square}^{2,\text{bcc}-A2} = -15106.9$$

Phase fcc-A1

$$L_{\text{Ce,Mg};\square}^{0,\text{fcc}-A1} = -15000 + 0.5 T$$

Phase hcp-A3

$$L_{\text{Ce,Mg};\square}^{0,\text{hcp}-A3} = -94337.51 + 79.95155 T$$

Phase Liquid

$$L_{\text{Ce,Mg}}^{0,\text{liquid}} = -39381.19 + 16.34052 T$$

$$L_{\text{Ce,Mg}}^{1,\text{liquid}} = 25338.56 - 11.86885 T$$

$$L_{\text{Ce,Mg}}^{2,\text{liquid}} = -15106.9$$

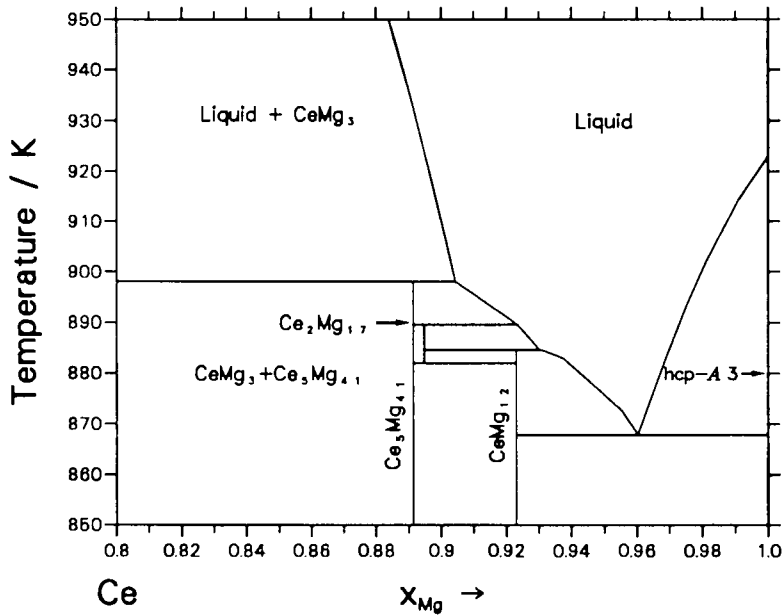
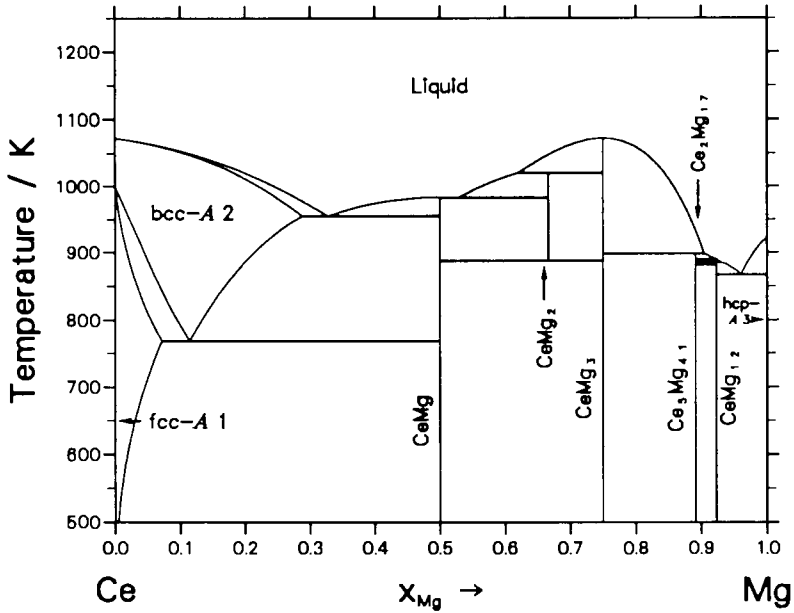


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Mg}	T / K
Liquid \rightleftharpoons bcc-A2 + CeMg	Eutectic	.328 .288 .500	955.1
Liquid \rightleftharpoons CeMg + CeMg ₂	Eutectic	.528 .500 .667	982.9
Liquid + CeMg ₃ \rightleftharpoons CeMg ₂	Peritectic	.620 .750 .667	1020.1
Liquid + CeMg ₃ \rightleftharpoons Ce ₅ Mg ₄₁	Peritectic	.904 .750 .891	898.1
Liquid + Ce ₅ Mg ₄₁ \rightleftharpoons Ce ₂ Mg ₁₇	Peritectic	.923 .891 .895	889.6
Liquid + Ce ₂ Mg ₁₇ \rightleftharpoons CeMg ₁₂	Peritectic	.930 .895 .923	884.7
Liquid \rightleftharpoons CeMg ₁₂ + hcp-A3	Eutectic	.960 .923 1.000	867.9
Ce ₂ Mg ₁₇ \rightleftharpoons Ce ₅ Mg ₄₁ + CeMg ₁₂	Eutectoid	.895 .891 .923	882.0
CeMg ₂ \rightleftharpoons CeMg + CeMg ₃	Eutectoid	.667 .500 .750	888.0
bcc-A2 \rightleftharpoons fcc-A1 + CeMg	Eutectoid	.114 .072 .500	768.7
CeMg \rightleftharpoons Liquid	Congruent	.500 .500	983.8
CeMg ₃ \rightleftharpoons Liquid	Congruent	.750 .750	1073.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Ce-Mg	(Ce)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>		
	(Ce)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>		
	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>		
	CeMg	CsCl	<i>cP2</i> <i>Pm$\bar{3}m$</i>	Ce 1 Mg 1	
	CeMg ₂	Cu ₂ Mg	<i>cF24</i> <i>Fd$\bar{3}m$</i>	Ce 8 Mg 16	
	CeMg ₃	BiF ₃	<i>cF16</i> <i>Fm$\bar{3}m$</i>	Ce 4 Mg ₁ 4 Mg ₂ 8	
	Ce ₅ Mg ₄₁	Ce ₅ Mg ₄₁	<i>tI92</i> <i>I4/m</i>		10 sublattices [91Vil]
	CeMg _{10.3}	Th ₂ Ni ₁₇	<i>hP38</i> <i>P6₃/mmc</i>		6 sublattices [91Vil] Ce ₂ Mg ₁₇
	CeMg ₁₂ (I)	ThMg ₁₂	<i>tI26</i> <i>I4/mmm</i>		ThMn ₁₂ in [91Vil]
	CeMg ₁₂ (II)	CeMg ₁₂ (II)	<i>oI338</i> <i>(Immm)</i>		not considered

System Cr–Cu

Solution Phases:

(stable) Liquid, bcc-A2, fcc-A1
 (metastable) hcp-A3

Modelling:

Liquid : Substitutional, Redlich–Kister
 bcc-A2 : Substitutional, Redlich–Kister
 fcc-A1 : Substitutional, Redlich–Kister
 hcp-A3 : Substitutional, Redlich–Kister

Assessor and Date:

K. Zeng and M. Hämmäläinen

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Cr,Cu};\square}^{0,\text{bcc-A2}} = 200000$$

Phase fcc-A1

$$L_{\text{Cr,Cu};\square}^{0,\text{fcc-A1}} = 88112 - 30.38315 T$$

Phase hcp-A3

$$L_{\text{Cr,Cu};\square}^{0,\text{hcp-A3}} = 60000$$

Phase liquid

$$L_{\text{Cr,Cu}}^{0,\text{liquid}} = 35495.913 - 2.958 T$$

$$L_{\text{Cr,Cu}}^{1,\text{liquid}} = -1001.1765$$

$$L_{\text{Cr,Cu}}^{2,\text{liquid}} = 5704.648$$

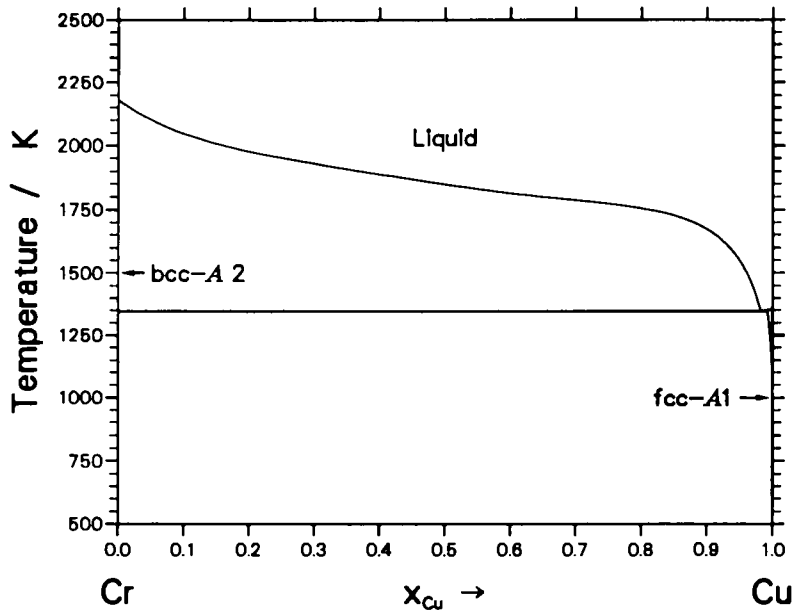


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Cu}	T / K
Liquid \rightleftharpoons bcc-A2 + fcc-A1	Eutectic	.982 .000 .992	1347.9

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cr-Cu	(Cr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>
	(Cu)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>

System Cr-Mg

Solution Phases:

(stable) Liquid, bcc-A2, hcp-A3
 (metastable) cbcc-A12, fcc-A1, hcp-Zn

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 cbcc-A12 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 hcp-Zn : Substitutional, Redlich-Kister

Assessor and Date:

I. Ansara, 1991

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$L_{Cr,Mg;\square}^{0,bcc-A2} = 80 T$$

Phase cbcc-A12

$$L_{Cr,Mg;\square}^{0,cbcc-A12} = 80 T$$

Phase fcc-A1

$$L_{Cr,Mg;\square}^{0,fcc-A1} = 80 T$$

Phase hcp-A3

$$L_{Cr,Mg;\square}^{0,hcp-A3} = 80 T$$

Phase hcp-Zn

$$L_{Cr,Mg;\square}^{0,hcp-Zn} = 80 T$$

Phase liquid

$$L_{Cr,Mg}^{0,liquid} = 94500.0$$

$$L_{Cr,Mg}^{1,liquid} = 12500.0$$

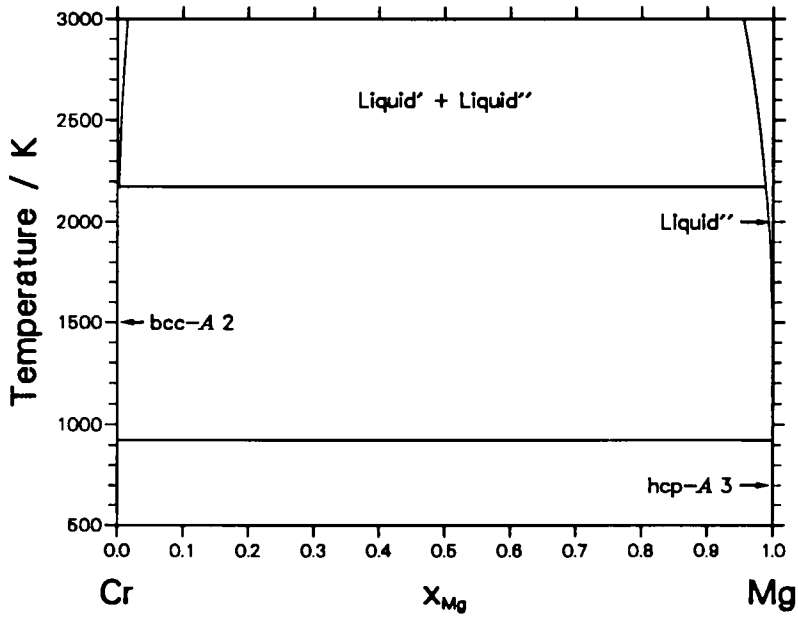


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Mg}	T / K
Liquid' \rightleftharpoons Liquid'' + bcc-A2	monotectic	.000 .003 .988	2174.9
Liquid'' \rightleftharpoons bcc-A2 + hcp-A3	Degenerate	.000 1.000 1.000	923.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cr-Mg	(Cr)	W	$cI2$ $Im\bar{3}m$
	(Mg)	Mg	$hP2$ $P6_3/mmc$

System Cr-Mn

Solution Phases:

Liquid, bcc-A2, fcc-A1, hcp-A3, cbcc-A12, cub-A13, σ -I, σ -II

Compound:

Cr_3Mn_5

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
cbcc-A12	:	Substitutional, Redlich-Kister
cub-A13	:	Substitutional, Redlich-Kister
σ I	:	Sublattice model, $(\text{Mn})_8(\text{Cr})_4(\text{Cr},\text{Mn})_{18}$
σ II	:	Sublattice model, $(\text{Mn})_8(\text{Cr})_4(\text{Cr},\text{Mn})_{18}$
Cr_3Mn_5	:	Stoichiometric, Cr_3Mn_5

Publication:

Scientific Group Thermodata Europe Database

Thermodynamic properties of the solution and compound phases ($\text{J}\cdot\text{mol}^{-1}$)

Phase Cr_3Mn_5

$$G^\circ(T) - 3.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 5.0 H_{\text{Mn}}^{\circ, \text{cbcc-A12, para}}(298.15 \text{ K}) = -72550.0 + 21.1732 T + 3.0 \text{GISER}_{\text{Cr}} + 5.0 \text{GISER}_{\text{Mn}}$$

Phase fcc-A1

$$L_{\text{Cr, Mn}; \square}^{0, \text{fcc-A1}} = -19088 + 17.5423 T$$

Phase cbcc-A12

$$L_{\text{Cr, Mn}; \square}^{0, \text{cbcc-A12}} = -36796 + 20.385 T$$

Phase liquid

$$L_{\text{Cr, Mn}}^{0, \text{liquid}} = -15009 + 13.6587 T$$

$$L_{\text{Cr, Mn}}^{1, \text{liquid}} = 504 + 0.9479 T$$

Phase cub-A13

$$L_{Cr,Mn:\square}^{0,cub-A13} = -31260 + 16.4919 T$$

Phase bcc-A2

$$L_{Cr,Mn:\square}^{0,bcc-A2} = -20328 + 18.7339 T$$

$$L_{Cr,Mn:\square}^{0,bcc-A2} = -9162 + 4.4183 T$$

$$\beta_{Cr,Mn:\square}^{0,bcc-A2,mag} = 0.48643$$

$$\beta_{Cr,Mn:\square}^{2,bcc-A2,mag} = -0.72035$$

$$\beta_{Cr,Mn:\square}^{4,bcc-A2,mag} = -1.93265$$

$$T_{c,Cr,Mn:\square}^{0,bcc-A2} = -1325$$

$$T_{c,Cr,Mn:\square}^{2,bcc-A2} = -1133$$

$$T_{c,Cr,Mn:\square}^{4,bcc-A2} = -10294$$

$$T_{c,Cr,Mn:\square}^{6,bcc-A2} = 26706$$

$$T_{c,Cr,Mn:\square}^{8,bcc-A2} = -28117$$

Phase σ -L

$$G^\circ(T) - 8.0 H_{Cr}^{\circ,bcc-A2,para}(298.15 K) - 22.0 H_{Mn}^{\circ,cbcc-A12,para}(298.15 K) =$$

$$G(Mn:Cr:Cr) = 65859.5 + 8.0 GFCC_{Mn} + 22.0 GHSER_{Cr}$$

$$G^\circ(T) - 26.0 H_{Cr}^{\circ,bcc-A2,para}(298.15 K) - 4.0 H_{Mn}^{\circ,cbcc-A12,para}(298.15 K) =$$

$$G(Mn:Cr:Mn) = -172946.0 + 69.0245 T + 8.0 GFCC_{Mn} + 4.0 GHSER_{Cr}$$

$$+ 18.0 GBCC_{Mn}$$

$$L_{Mn:Cr:Cr,Mn}^{0,\sigma-L} = -1095771 + 862.0312 T$$

Phase σ -H

$$G^\circ(T) - 8.0 H_{Cr}^{\circ,bcc-A2,para}(298.15 K) - 22.0 H_{Mn}^{\circ,cbcc-A12,para}(298.15 K) =$$

$$G(Mn:Cr:Cr) = -192369.0 + 152.4742 T + 8.0 GFCC_{Mn} + 22.0 GHSER_{Cr}$$

$$G^\circ(T) - 26.0 H_{Cr}^{\circ,bcc-A2,para}(298.15 K) - 4.0 H_{Mn}^{\circ,cbcc-A12,para}(298.15 K) =$$

$$G(Mn:Cr:Mn) = -74263.0 - 10.7082 T + 18.0 GBCC_{Mn} + 8.0 GFCC_{Mn}$$

$$+ 4.0 GHSER_{Cr}$$

$$L_{Mn:Cr:Cr,Mn}^{0,\sigma-H} = 90000$$

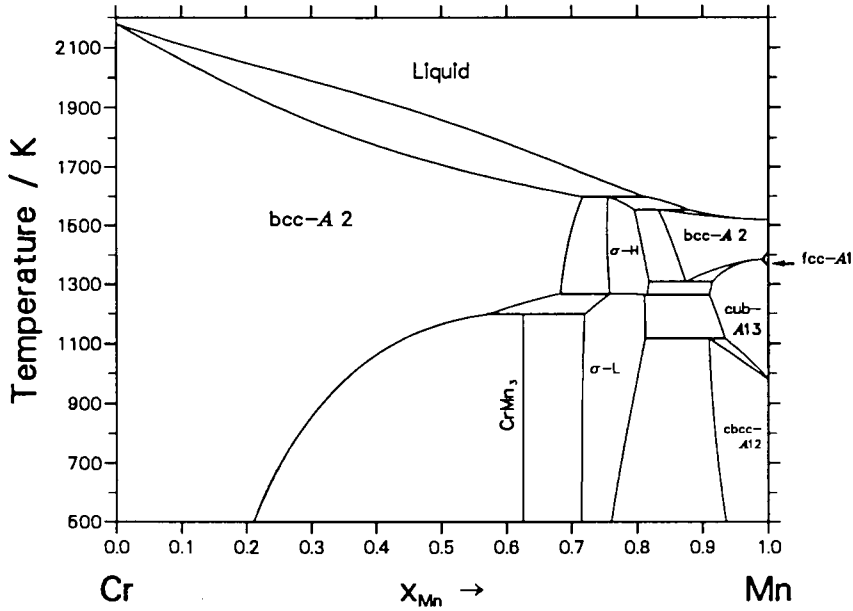


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Mn}	T / K
$bcc-A2 + \sigma-L \rightleftharpoons Cr_3Mn_5$	Peritectoid	.570 .719 .625	1197.8
$\sigma-H \rightleftharpoons bcc-A2 + \sigma-L$	Eutectoid	.758 .683 .760	1268.1
$Liquid + bcc-A2 \rightleftharpoons \sigma-H$	Peritectic	.813 .717 .755	1598.4
$Liquid + \sigma-H \rightleftharpoons bcc-A2$	Peritectic	.876 .794 .831	1556.2
$bcc-A2 \rightleftharpoons cub-A13 + \sigma-H$	Eutectoid	.880 .873 .894	1293.6
$bcc-A2 + fcc-A1 \rightleftharpoons cub-A13$	Peritectoid	.898 .993 .913	1382.1
$\sigma-H \rightleftharpoons \sigma-L + cub-A13$	Eutectoid	.815 .811 .910	1264.4
$\sigma-L + cub-A13 \rightleftharpoons cbcc-A12$	Peritectoid	.812 .934 .910	1117.4

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Cr-Mn	(Cr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	
	α -Mn	α -Mn	<i>c58</i> <i>I$\bar{4}3m$</i>	bcc-A12
	β -Mn	β -Mn	<i>cP20</i> <i>P$_4$323m</i>	cub-A13
	γ -Mn	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	fcc-A1
	δ -Mn	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	bcc-A2
	α' Cr _x Mn _{1-x} HT	α -Mn		
	α'' Cr _x Mn _{1-x} LT	α -Mn		
	σ Cr _x Mn _{1-x} HT	σ CrFe	<i>tP30</i> <i>P$_4$$_2$/mnm</i>	
	σ Cr _x Mn _{1-x} MT	σ CrFe	<i>tP30</i> <i>P$_4$$_2$/mnm</i>	
	σ Cr _x Mn _{1-x} LT	σ CrFe	<i>tP30</i> <i>P$_4$$_2$/mnm</i>	

System Cr–Si

Solution Phases:

Liquid, bcc-A2

Compounds:

Cr₅Si₃, CrSi, Cr₃Si-A15, CrSi₂

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc-A2	:	Substitutional, Redlich–Kister
Cr ₃ Si-A15	:	Sublattice model, (Cr,Si) ₃ (Cr,Si)
CrSi ₂	:	Sublattice model, (Cr,Si)(Cr,Si) ₂
Cr ₅ Si ₃	:	Stoichiometric, (Cr) ₅ (Si) ₃
CrSi	:	Stoichiometric, (Cr)(Si)

Assessor and Date:

C.A. Coughnanowr, I. Ansara, and H.L. Lukas,

Publication:

Calphad, 18, 2, 125–140 (1994).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase liquid

$$L_{\text{Cr,Si}}^{0,\text{liquid}} = -119216.90 + 16.11445 T$$

$$L_{\text{Cr,Si}}^{1,\text{liquid}} = -47614.70 + 12.17363 T$$

Phase bcc-A2

$$L_{\text{Cr,Si}}^{0,\text{bcc-A2}} = -104537.94 + 10.69527 T$$

$$L_{\text{Cr,Si}}^{1,\text{bcc-A2}} = -47614.70 + 12.17363 T$$

Phase Cr₃Si-A15

$$G^\circ(T) - 4.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 20000.0 + 10.000 T + 4.0 \text{ GHSEr}_{\text{Cr}}$$

$$G^\circ(T) - 3.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Cr:Si}) = -126369.35 + 4.15051 T + 3.0 \text{ GHSEr}_{\text{Cr}} + \text{GHSEr}_{\text{Si}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 3.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Cr:Si}) = 233507.47 - 74.15051 T + \text{GHSEr}_{\text{Cr}} + 3.0 \text{ GHSEr}_{\text{Si}}$$

$$G^\circ(T) - 4.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si}) = 208000.0 - 80.000 T + 4.0 \text{ GHSEr}_{\text{Si}}$$

$$L_{\text{Cr, Si:Cr}}^{0, \text{Cr}_3\text{Si}} = L_{\text{Cr, Si:Si}}^{0, \text{Cr}_3\text{Si}} = -107840.95$$

$$L_{\text{Cr:Cr, Si}}^{0, \text{Cr}_3\text{Si}} = L_{\text{Si:Cr, Si}}^{0, \text{Cr}_3\text{Si}} = -13020.93$$

Phase Cr₅Si₃

$$G^\circ(T) - 5.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 3.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = -316433.0 + 1065.82816 T - 182.578184 T \cdot \ln T - 23.919688\text{E-}3 T^2 - 2.31728\text{E-}06 T^3$$

Phase CrSi

$$G^\circ(T) - H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = -78732.28 + 311.58392 T - 51.62865 T \cdot \ln T - 4.47355\text{E-}03 T^2 + 391330 T^{-1}$$

Phase CrSi₂

$$G^\circ(T) - 3.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 10000.00 - 1.0 T + 3.0 \text{ GHSEr}_{\text{Cr}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 2.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Cr:Si}) = -96694.43 + 333.33835 T - 57.855747 T \cdot \ln T - 13.22769\text{E-}03 T^2 - 0.43203\text{E-}06 T^3$$

$$G^\circ(T) - 2.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Si:Cr}) = 148569.93 - 12.65342 T + 2.0 \text{ GHSEr}_{\text{Cr}} + \text{GHSEr}_{\text{Si}}$$

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si}) = 78860.26 - 15.77206 T + 3.0 \text{ GHSEr}_{\text{Si}}$$

$$L_{\text{Cr:Cr, Si}}^{0, \text{CrSi}_2} = L_{\text{Si:Cr, Si}}^{0, \text{CrSi}_2} = -35879.97 + 7.17599 T$$

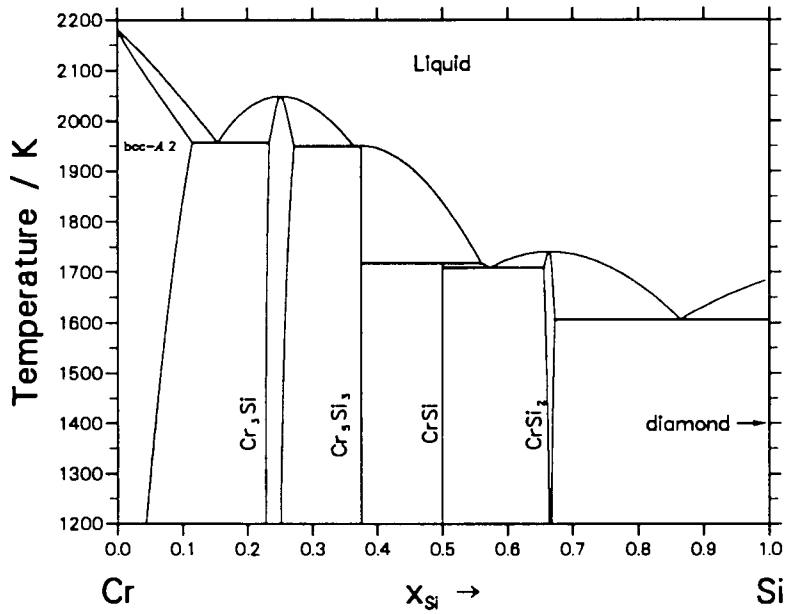


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Si}	T / K
Liquid \rightleftharpoons bcc-A2 + Cr ₃ Si-A15	Eutectic	.154 .115 .233	1957.4
Liquid \rightleftharpoons Cr ₃ Si-A15 + Cr ₅ Si ₃	Eutectic	.364 .272 .375	1950.0
Liquid + Cr ₅ Si ₃ \rightleftharpoons CrSi	Peritectic	.560 .375 .500	1718.5
Liquid \rightleftharpoons CrSi + CrSi ₂	Eutectic	.574 .500 .656	1708.8
Liquid \rightleftharpoons CrSi ₂ + diamond	Eutectic	.864 .673 1.000	1606.7
Cr ₃ Si-A15 \rightleftharpoons Liquid	Congruent	.025 .025 ...	2049.5
Cr ₅ Si ₃ \rightleftharpoons Liquid	Congruent	.375 .375 ...	1951.0
Cr ₂ Si \rightleftharpoons Liquid	Congruent	.666 .666 ...	1741.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Cr-Si	(Cr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	(Si)	diamond-A4	<i>cF8</i> <i>Fd$\bar{3}m$</i>		
	CrSi	FeSi	<i>cP8</i> <i>P2$_1$3</i>	Cr 4 Si 4	
	CrSi ₂	CrSi ₂	<i>hP9</i> <i>P6$_2$22</i>	Cr 3 Si 6	
	Cr ₃ Si	Cr ₃ Si	<i>cP8</i> <i>Pm$\bar{3}n$</i>	Cr 6 Si 2	Cr ₃ Si-A15
	Cr ₅ Si ₃	Si ₃ W ₅	<i>tI32</i> <i>I4/mcm</i>	Cr ₁ 4 Cr ₂ 16 Si ₁ 4 Si ₂ 8	<i>tI38</i> in Mas1
	Cr ₅ Si ₃	Mn ₅ Si ₃	<i>hP16</i> <i>P6$_3$/mcm</i>		not considered

System Cr-Ti

Solution Phases:

Liquid, bcc-A2, hcp-A3

Compounds:

Laves-C14, Laves-C15

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 Laves-C14 : Sublattice model, (Cr,Ti)₂ (Cr,Ti)
 Laves-C15 : Sublattice model, (Cr,Ti)₂ (Cr,Ti)

Assessor and Date:

N. Saunders, 1992

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Laves-C14

$$G^{\circ}(T) - 3.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Cr}}$$

$$G^{\circ}(T) - 2.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cr:Ti}) = \\ - 1440.0 - 6.75 T + 2.0 \text{ GHSER}_{\text{Cr}} + \text{GHSER}_{\text{Ti}}$$

$$G^{\circ}(T) - H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Cr}) = \\ 15000.0 + \text{GHSER}_{\text{Cr}} + 2.0 \text{ GHSER}_{\text{Ti}}$$

$$G^{\circ}(T) - 3.0 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = \\ 15000.0 + 3.0 \text{ GHSER}_{\text{Ti}}$$

$$L_{\text{Cr:Cr,Ti}}^{0, \text{Laves-C14}} = L_{\text{Ti:Cr,Ti}}^{0, \text{Laves-C14}} = 60000.0$$

$$L_{\text{Cr,Ti:Cr}}^{0, \text{Laves-C14}} = L_{\text{Cr,Ti:Ti}}^{0, \text{Laves-C14}} = 60000.0$$

Phase Laves-C15

$$G^{\circ}(T) - 3.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Cr}}$$

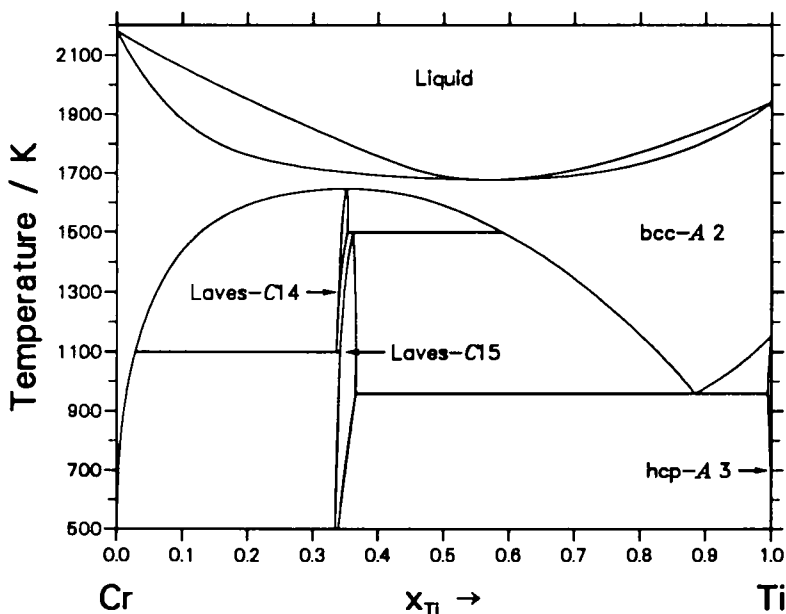
$$G^{\circ}(T) - 2.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cr:Ti}) = -1780.0 - 6.3 T + 2.0 \text{ GHSE}_{\text{Cr}} + \text{GHSE}_{\text{Ti}}$$

$$G^{\circ}(T) - H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Cr}) = 15000.0 + \text{GHSE}_{\text{Cr}} + 2.0 \text{ GHSE}_{\text{Ti}}$$

$$G^{\circ}(T) - 3.0 H_{\text{Ti}}^{\circ, \text{hcp-A2}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Ti}}$$

$$L_{\text{Cr:Cr,Ti}}^{0, \text{Laves-C15}} = L_{\text{Ti:Cr,Ti}}^{0, \text{Laves-C15}} = 50000.0$$

$$L_{\text{Cr,Ti:Cr}}^{0, \text{Laves-C15}} = L_{\text{Cr,Ti:Ti}}^{0, \text{Laves-C15}} = 10800.0 + 27 T$$



Phase liquid

$$L_{\text{Cr,Ti}}^{0, \text{liquid}} = 5250$$

$$L_{\text{Cr,Ti}}^{1, \text{liquid}} = 1500$$

Phase hcp-A3

$$L_{\text{Cr,Ti};\square}^{0, \text{hcp-A3}} = 32500$$

Phase bcc-A2

$$I_{Cr,Ti;\square}^{0,bcc-A2} = 19100$$

$$I_{Cr,Ti;\square}^{1,bcc-A2} = 5500$$

$$I_{Cr,Ti;\square}^{2,bcc-A2} = 1750$$

Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Ti}	T / K
$bcc-A2 \rightleftharpoons Laves-C15 + hcp-A3$	Eutectoid	.884 .365 .994	959.7
$bcc-A2 + Laves-C15 \rightleftharpoons Laves-C14$	Peritectoid	.593 .353 .362	1495.3
$Laves-C14 \rightleftharpoons bcc-A2 + Laves-C15$	Eutectoid	.336 .027 .342	1093.4
$Laves-C14 \rightleftharpoons bcc-A2$	Congruent	.333 .333	1645.0
$bcc-A2 \rightleftharpoons Liquid$	Congruent	.563 .563	1677.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Cr-Ti	(Cr)	W	$cI2$ $Im\bar{3}m$	
	(Ti)	Mg	$hP2$ $P6_3/mmc$	
	(Ti)	W	$cI2$ $Im\bar{3}m$	
	α Cr ₂ Ti	Cu ₂ Mg	$cF24$ $Fd\bar{3}m$	Laves-C15
	β Cr ₂ Ti	MgZn ₂	$hP12$ $P6_3/mmc$	Laves-C14
	γ Cr ₂ Ti	MgNi ₂	$hP24$ $P6_3/mmc$	Laves-C36

System Cr–V

Solution Phases:

Liquid, bcc-A2

Modelling:

Liquid : Substitutional, Redlich–Kister
bcc-A2 : Substitutional, Redlich–Kister

Publication:

Scientific Group Thermodata Europe Database

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Cr,V};\square}^{0,\text{bcc-A2}} = -9874 - 2.6964 T$$

$$L_{\text{Cr,V};\square}^{1,\text{bcc-A2}} = -1720 - 2.5237 T$$

Phase liquid

$$L_{\text{Cr,V}}^{0,\text{liquid}} = -9874 - 2.6964 T$$

$$L_{\text{Cr,V}}^{1,\text{liquid}} = -1720 - 2.5237 T$$

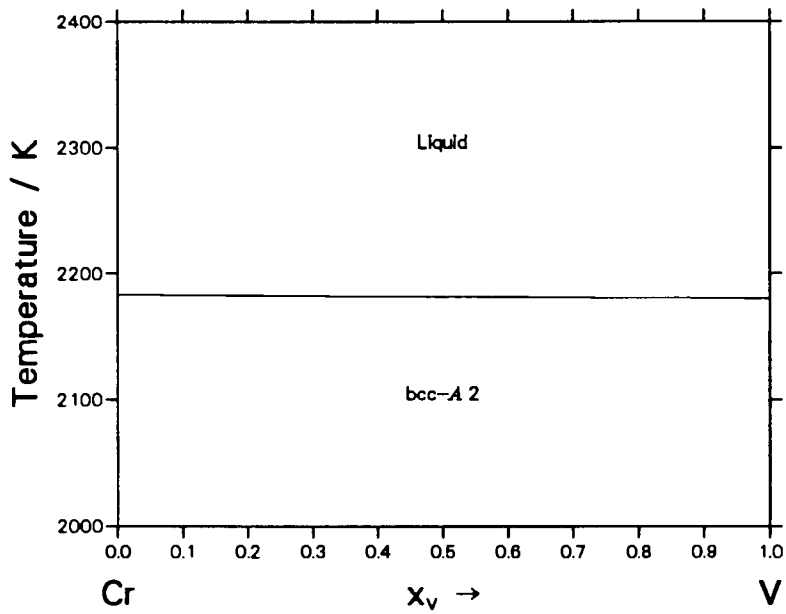


Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cr-V	(Cr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>
	(V)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>

System Cr–Zn

Solution Phases:

(stable) Liquid, bcc-A2, hcp-Zn
 (metastable) fcc-A1

Compounds:

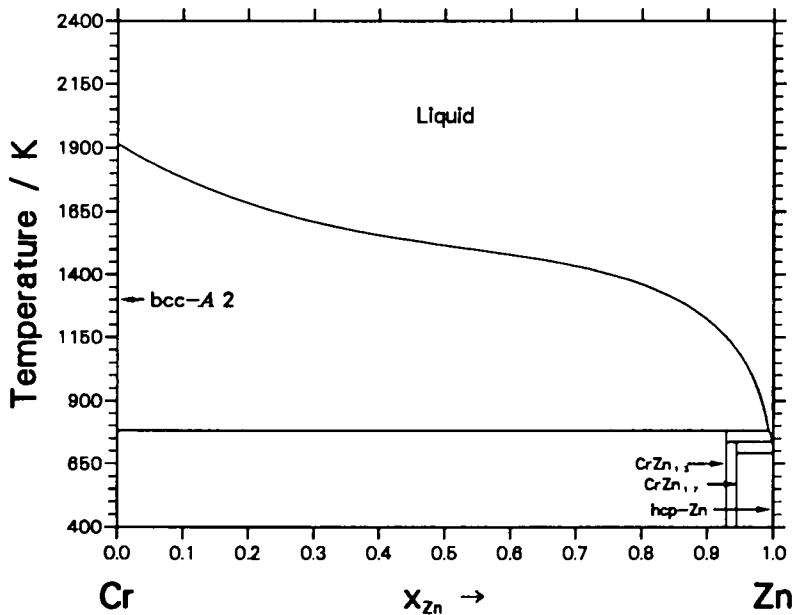
CrZn₁₃, CrZn₁₇

Modelling:

bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-Zn : Substitutional, Redlich-Kister
 Liquid : Substitutional, Redlich-Kister
 CrZn₁₃ : Stoichiometric, (Cr)(Zn)₁₃
 CrZn₁₇ : Stoichiometric, (Cr)(Zn)₁₇

Assessor and Date:

I. Ansara, 1992



Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-A2

$$L_{Cr,Zn;\square}^{0,bcc-A2} = 80 T$$

Phase fcc-A1

$$L_{Cr,Zn;\square}^{0,fcc-A1} = 80 T$$

Phase hcp-Zn

$$L_{Cr,Zn;\square}^{0,hcp-Zn} = 80 T$$

Phase liquid

$$L_{Cr,Zn}^{0,liquid} = 19000$$

$$L_{Cr,Zn}^{1,liquid} = -1000$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zn}	T / K
Liquid + bcc-A2 \rightleftharpoons CrZn ₁₃ *	Peritectic	0.996 0.000 0.928	761.4
Liquid + CrZn ₁₃ \rightleftharpoons CrZn ₁₇	Peritectic	0.998 0.928 0.944	736.5
Liquid \rightleftharpoons CrZn ₁₇ + hcp-Zn	Degenerate	0.999 0.944 0.999	692.5

* Reaction uncertain

Phase CrZn₁₃

$$G^{\circ}(T) - H_{Cr}^{\circ,bcc-A2,para}(298.15 K) - 13.0 H_{Zn}^{\circ,hcp-A3}(298.15K) \\ - 9800.0 + GHSER_{Cr} + 13.0 GHSER_{Zn}$$

Phase CrZn₁₇

$$G^{\circ}(T) - H_{Cr}^{\circ,bcc-A2,para}(298.15 K) - 17.0 H_{Zn}^{\circ,hcp-A3}(298.15K) \\ - 11700.0 + GHSER_{Cr} + 17.0 GHSER_{Zn}$$

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cr-Zn	(Cr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>
	(Zn)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>
	CrZn ₁₃	CoZn ₁₃	
	CrZn ₁₇		

System Cr-Zr

Solution Phases:

(stable) Liquid, bcc-A2, hcp-A3
 (metastable) fcc-A1

Compounds:

Laves-C14, Laves-C15, Laves-C36

Modelling:

bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 Liquid : Substitutional, Redlich-Kister
 Laves-C14 : Sublattice model, (Cr,Zr)₂(Cr,Zr)
 Laves-C15 : Sublattice model, (Cr,Zr)₂(Cr,Zr)
 Laves-C36 : Sublattice model, (Cr,Zr)₂(Cr,Zr)

Assessor and Date:

K. Zeng, M. Hämmäläinen, and I. Ansara (1993)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Laves-C14

$$G^{\circ}(T) - 3.0 H_{Cr}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 15000.0 + 3.0 \text{ GHSER}_{Cr}$$

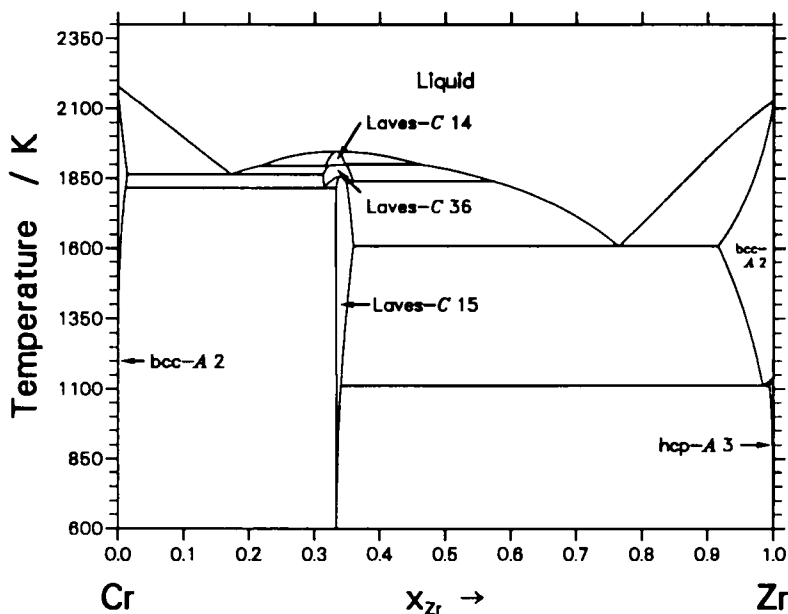
$$G^{\circ}(T) - 2.0 H_{Cr}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cr:Zr}) = -8114 - 11.652 T + 2.0 \text{ GHSER}_{Cr} + \text{GHSER}_{Zr}$$

$$G^{\circ}(T) - H_{Cr}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 2.0 H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Zr:Cr}) = 38114 + 11.652 T + \text{GHSER}_{Cr} + 2.0 \text{ GHSER}_{Zr}$$

$$G^{\circ}(T) - 3.0 H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Zr:Zr}) = 15000.0 + 3.0 \text{ GHSER}_{Zr}$$

$$L_{Cr,Zr:Cr}^{0, \text{Laves-C14}} = L_{Cr,Zr:Zr}^{0, \text{Laves-C14}} = 52300$$

$$L_{Cr:Cr,Zr}^{0, \text{Laves-C14}} = L_{Zr:Cr,Zr}^{0, \text{Laves-C14}} = 26060$$



Phase Laves-C15

$$G^{\circ}(T) - 3.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Cr}}$$

$$G^{\circ}(T) - 2.0 H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cr:Zr}) = -87273 + 29.915 T + 2.0 \text{ GHSE}_{\text{Cr}} + \text{GHSE}_{\text{Zr}}$$

$$G^{\circ}(T) - H_{\text{Cr}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 2.0 H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Zr:Cr}) = 387273 - 29.915 T + \text{GHSE}_{\text{Cr}} + 2.0 \text{ GHSE}_{\text{Zr}}$$

$$G^{\circ}(T) - 3.0 H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Zr:Zr}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Zr}}$$

$$L_{\text{Cr,Zr:Cr}}^{0, \text{Laves-C15}} = 70328$$

$$L_{\text{Cr,Zr:Zr}}^{0, \text{Laves-C15}} = 70328$$

$$L_{\text{Cr:Cr,Zr}}^{0, \text{Laves-C15}} = 62910$$

$$L_{\text{Zr:Cr,Zr}}^{0, \text{Laves-C15}} = 62910$$

Phase Laves-C36

$$G^{\circ}(T) - 3.0 H_{Cr}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 15000.0 + 3.0 \text{ GHSE}_{Cr}$$

$$G^{\circ}(T) - 2.0 H_{Cr}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cr:Zr}) = -70026 + 20.901 T + 2.0 \text{ GHSE}_{Cr} + \text{GHSE}_{Zr}$$

$$G^{\circ}(T) - H_{Cr}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 2.0 H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Zr:Cr}) = 100026.08 - 20.901 T + \text{GHSE}_{Cr} + 2.0 \text{ GHSE}_{Zr}$$

$$G^{\circ}(T) - 3.0 H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Zr:Zr}) = 15000.0 + 3.0 \text{ GHSE}_{Zr}$$

$$I_{Cr,Zr:Cr}^{0, \text{Laves-C36}} = 52614$$

$$I_{Cr,Zr:Zr}^{0, \text{Laves-C36}} = 52614$$

$$I_{Cr:Cr,Zr}^{0, \text{Laves-C36}} = 29400$$

$$I_{Zr:Cr,Zr}^{0, \text{Laves-C36}} = 2940$$

Phase liquid

$$I_{Cr,Zr}^{0, \text{liquid}} = -12971.34 + 1.20015 T$$

$$I_{Cr,Zr}^{1, \text{liquid}} = 8025.96 - 0.74259 T$$

$$I_{Cr,Zr}^{2, \text{liquid}} = -9984.87 + 0.92383 T$$

Phase bcc-A2

$$I_{Cr,Zr:\square}^{0, \text{bcc-A2}} = 16555.47 + 4.92028 T$$

$$I_{Cr,Zr:\square}^{1, \text{bcc-A2}} = 11365.57$$

Phase fcc-A1

$$I_{Cr,Zr:\square}^{0, \text{fcc-A1}} = 20000$$

Phase hcp-A3

$$I_{Cr,Zr:\square}^{0, \text{hcp-A3}} = 15800$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zr}	T / K
Liquid \rightleftharpoons Laves-C15 + bcc-A2	Eutectic	.765 .359 .916	1607.9
Laves-C36 \rightleftharpoons Laves-C15 + Liquid	Metatectic	.359 .348 .573	1839.6
Liquid + Laves-C14 \rightleftharpoons Laves-C36	Peritectic	.461 .346 .348	1900.0
Laves-C36 \rightleftharpoons Liquid + Laves-C14	Metatectic	.316 .218 .321	1895.9
Liquid \rightleftharpoons bcc-A2 + Laves-C36	Eutectic	.173 .014 .313	1864.6
Laves-C36 \rightleftharpoons bcc-A2 + Laves-C15	Eutectoid	.314 .012 .333	1816.1
bcc-A2 \rightleftharpoons Laves-C15 + hcp-A3	Eutectoid	.984 .340 .994	1112.3
Laves-C14 \rightleftharpoons Liquid	Congruent	.333 .333	1946.5
Laves-C15 \rightleftharpoons Laves-C36	Congruent	.340 .340	1858.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Cr-Zr	(Cr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	(Zr)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2	
	(Zr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 4	
	α -Cr ₂ Zr	Cu ₂ Mg	<i>cF24</i> <i>Fd$\bar{3}m$</i>	M ₁ 8 M ₂ 16	Laves-C15
	β -Cr ₂ Zr	MgNi ₂	<i>hP24</i> <i>P6$_3$/mmc</i>	Cr ₁ 6 Cr ₂ 6 Zr ₁ 3 Zr ₂ 3	Laves-C36
	γ -Cr ₂ Zr	MgZn ₂	<i>hP12</i> <i>P6$_3$/mmc</i>	Cr 2 Cr 6 Zr 4	Laves-C14

System Cu-Fe

Solution Phases:

(stable) : Liquid, fcc-A1, bcc-A2
 (metastable) : hcp-A3

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister

Assessor and Date:

I. Ansara, and Å. Jansson

Publication:

Trita-Mac-0533, Dec. 1993, Materials Research Center,
 The Royal Institute of Technology, Stockholm (Sweden)

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Cu,Fe};\square}^{0,\text{bcc-A2}} = 39258.0 - 4.14983 T$$

Phase fcc-A1

$$L_{\text{Cu,Fe};\square}^{0,\text{fcc-A1}} = 48232.5 - 8.60954 T$$

$$L_{\text{Cu,Fe};\square}^{1,\text{fcc-A1}} = 8861.88 - 5.28975 T$$

Phase hcp-A3

$$L_{\text{Cu,Fe};\square}^{0,\text{hcp-A3}} = 48232.5 - 8.60954 T$$

$$L_{\text{Cu,Fe};\square}^{1,\text{hcp-A3}} = 8861.88 - 5.28975 T$$

Phase liquid

$$I_{\text{Cu,Fe}}^{0,\text{liquid}} = 36088.0 - 2.32968 T$$

$$I_{\text{Cu,Fe}}^{1,\text{liquid}} = 324.53 - 0.03270 T$$

$$I_{\text{Cu,Fe}}^{2,\text{liquid}} = 10355.40 - 3.60297 T$$

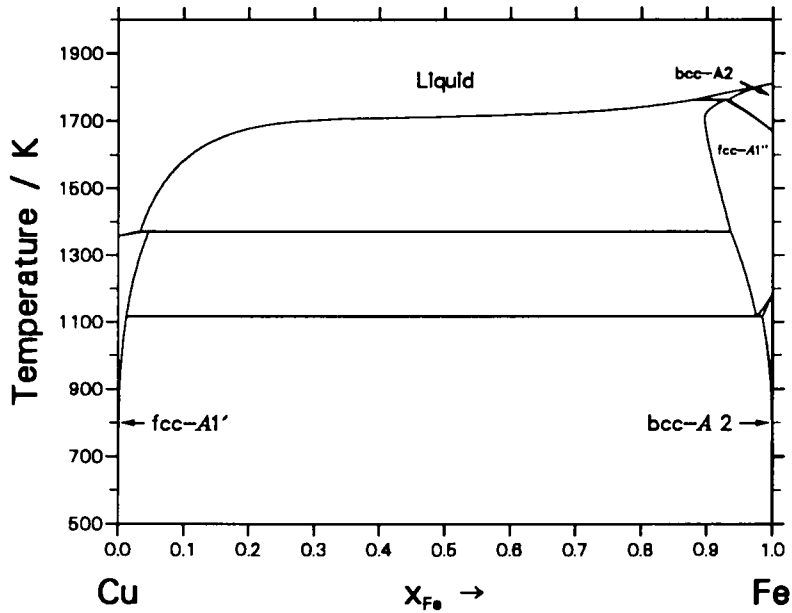


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Fe}	T / K
Liquid + bcc-A2 \rightleftharpoons fcc-A1''	Peritectic	.880 .933 .927	1762.4
Liquid + fcc-A1'' \rightleftharpoons fcc-A1'	Peritectic	.034 .936 .047	1371.4
fcc-A1'' \rightleftharpoons fcc-A1' + bcc-A2	Eutectoid	.975 .012 .984	1115.9

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cu-Fe	(Cu)	Cu	$cF4$ $Fm\bar{3}m$
	(Fe)	Cu	$cF4$ $Fm\bar{3}m$
	(Fe)	W	$cI2$ $Im\bar{3}m$

System Cu–Li

Solution Phases:

(stable) Liquid, bcc-A2, fcc-A1

Solution Phases:

(metastable) hcp-A3

Modelling:

Liquid : Substitutional, Redlich–Kister
 bcc-A2 : Substitutional, Redlich–Kister
 fcc-A1 : Substitutional, Redlich–Kister
 hcp-A3 : Substitutional, Redlich–Kister

Assessor and Date:

N. Saunders, 1991

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$I_{\text{Cu,Li};\square}^{0,\text{bcc-A2}} = 50000$$

Phase fcc-A1

$$I_{\text{Cu,Li};\square}^{0,\text{fcc-A1}} = 2750 + 13.0 T$$

$$I_{\text{Cu,Li};\square}^{1,\text{fcc-A1}} = -1000$$

Phase hcp-A3

$$I_{\text{Cu,Li};\square}^{0,\text{hcp-A3}} = 2042 + 10.9617 T$$

Phase liquid

$$I_{\text{Cu,Li}}^{0,\text{liquid}} = 66000 - 44.723 T$$

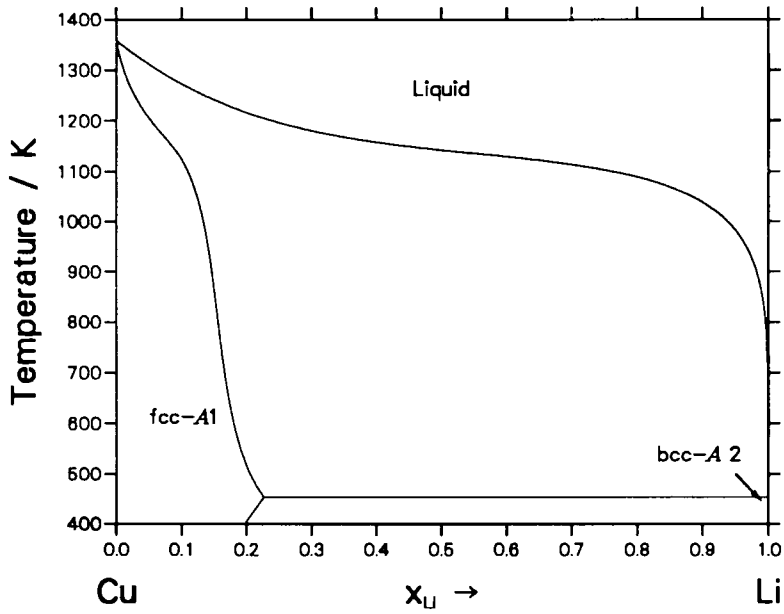


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Li}	T / K
Liquid \rightleftharpoons fcc-A1 + bcc-A2	Degenerate	1.000 0.228 1.000	453.6

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pears. Symb. Space Group
Cu-Li	(Cu)	Cu	$cF4$ $Fm\bar{3}m$
	(Li)	W	$cI2$ $Im\bar{3}m$

System Cu–Mg

Solution Phases:

(stable) : Liquid, fcc-A1, hcp-A3
 (metastable) : bcc-B2, hcp-Zn

Compound:

(stable) Laves-C15, CuMg₂
 (metastable) Laves-C14, Laves-C36, CuZn- γ
 MgZn, Mg₂Zn₃, Mg₂Zn₁₁

Modelling:

Liquid : Substitutional, Redlich–Kister
 fcc-A1 : Substitutional, Redlich–Kister
 hcp-A3 : Substitutional, Redlich–Kister
 Laves-C15 : Sublattice-model, Cu,Mg)_{0.5}(Cu,Mg)_{0.5}(\square)₃
 CuMg₂ : Stoichiometric, CuMg₂
 bcc-A2 : see below
 bcc-B2 : Sublattice model, (Cu,Mg)_{0.5}(Cu,Mg)_{0.5}
 Two descriptions of the bcc-A2: bcc-B2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
 hcp-Zn : Substitutional, Redlich–Kister
 CuZn- γ : Stoichiometric, (Cu)₂(Cu)₂(Cu)₃(Mg)₆
 Mg₂Zn₁₁ : Stoichiometric, (Cu)₁₁(Mg)₂
 Mg₂Zn₃ : Stoichiometric, (Cu)₃(Mg)₂
 MgZn : Stoichiometric, (Cu)₁₃(Mg)₁₂
 Laves-C14 : Sublattice-model, (Cu,Mg)₂(Cu,Mg)
 Laves-C36 : Sublattice-model, (Cu,Mg)₂(Cu,Mg)

Assessor and Date:

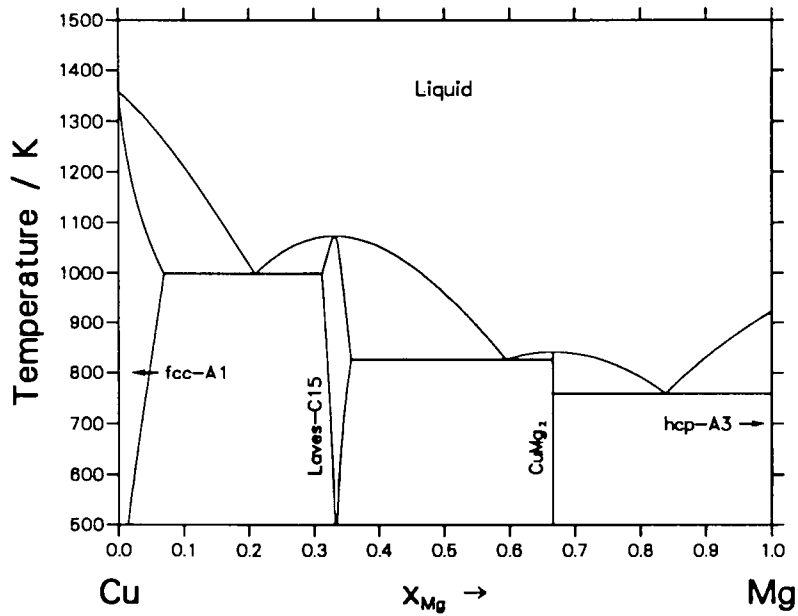
C.A. Coughnanowr, I. Ansara, R. Luoma,
 M. Hämäläinen, and H.L. Lukas

Publication:

Z. für Metallkde., 82, 7, 574-581 (1991).

Comments:

A new assessment was performed where the lattice stabilities of Cu and Mg in the Laves-C15 structure were taken equal to 15kJ/formula unit, in order to ensure consistency in the database.



Thermodynamic properties of the solution and compound phases ($\text{J}\cdot\text{mol}^{-1}$)

Phase liquid

$$L_{\text{Cu,Mg}}^{0,\text{liquid}} = -36962.71 + 4.74394 T$$

$$L_{\text{Cu,Mg}}^{1,\text{liquid}} = -8182.19$$

Phase fcc-A1

$$L_{\text{Cu,Mg};\square}^{0,\text{fcc-A1}} = -22059.61 + 5.63232 T$$

Phase hcp-A3

$$L_{\text{Cu,Mg};\square}^{0,\text{hcp-A3}} = 22500.0 - 3.0 T$$

Phase hcp-Zn

$$L_{\text{Cu,Mg};\text{Zn}}^{0,\text{hcp-Zn}} = 22500.0 - 3.0 T$$

Phase Laves-C14

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Mg}) = \\ - 24691.0 + 364.73085 T - 69.276417 T \cdot \ln T - 5.19246\text{E-}04 T^2 \\ + 143502 T^{-1} - 5.65953\text{E-}6 T^3$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Cu}) = \\ 74970.96 - 16.46448 T + \text{GHSE}_{\text{Cu}} + 2.0 \text{ GHSE}_{\text{Mg}}$$

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Mg}}$$

$$L_{\text{Cu,Mg};\text{Cu}}^{0,\text{Laves-C14}} = L_{\text{Cu,Mg};\text{Mg}}^{0,\text{Laves-C14}} = 13011.35$$

$$L_{\text{Cu:Cu};\text{Mg}}^{0,\text{Laves-C14}} = L_{\text{Mg:Cu};\text{Mg}}^{0,\text{Laves-C14}} = 6599.45$$

Phase Laves-C15

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Mg}) = \\ - 54691.0 + 364.73085 T - 69.276417 T \cdot \ln T - 5.19246\text{E-}04 T^2 \\ + 143502 T^{-1} - 5.65953\text{E-}6 T^3$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Cu}) = \\ 104970.96 - 16.46448 T + \text{GHSE}_{\text{Cu}} + 2.0 \text{ GHSE}_{\text{Mg}}$$

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Mg}}$$

$$L_{\text{Cu,Mg};\text{Cu}}^{0,\text{Laves-C15}} = L_{\text{Cu,Mg};\text{Mg}}^{0,\text{Laves-C15}} = 13011.35$$

$$L_{\text{Cu:Cu};\text{Mg}}^{0,\text{Laves-C15}} = L_{\text{Mg:Cu};\text{Mg}}^{0,\text{Laves-C15}} = 6599.45$$

Phase Laves-C36

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Mg}) = \\ - 34691.0 + 364.73085 T - 69.276417 T \cdot \ln T - 5.19246\text{E-}04 T^2 \\ + 143502 T^{-1} - 5.65953\text{E-}6 T^3$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = 84970.96 - 16.46448 T + \text{GHSER}_{\text{Cu}} + 2.0 \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \text{GHSER}_{\text{Mg}}$$

$$L_{\text{Cu,Mg:Cu}}^{0,\text{Laves-C36}} = L_{\text{Cu,Mg:Mg}}^{0,\text{Laves-C36}} = 13011.35$$

$$L_{\text{Cu:Cu,Mg}}^{0,\text{Laves-C36}} = L_{\text{Mg:Cu,Mg}}^{0,\text{Laves-C36}} = 6599.45$$

Phase CuMg₂

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = -28620.0 + 1.86456 T + \text{GHSER}_{\text{Cu}} + 2.0 \text{GHSER}_{\text{Mg}}$$

Phase CuZn- γ

$$K4 = -11552.71 - 1.67824 T$$

$$K5 = 15732.3 - 10.26575 T$$

$$K7 = 9000.0 - 1.5 T$$

$$G^\circ(T) - 7.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Cu:Cu:Mg}) = 13.0 K4 + 2.0 K5 + 6.0 K7 + 7.0 \text{GHSER}_{\text{Cu}} + 6.0 \text{GHSER}_{\text{Mg}}$$

Phase Mg₂Zn₁₁

$$G^\circ(T) - 11.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = 0.0 + 11.0 \text{GHSER}_{\text{Cu}} + 2.0 \text{GHSER}_{\text{Mg}}$$

Phase Mg₂Zn₃

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = 0.0 + 3.0 \text{GHSER}_{\text{Cu}} + 2.0 \text{GHSER}_{\text{Mg}}$$

Phase MgZn

$$G^\circ(T) - 13.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 12.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = 0.0 + 13.0 \text{GHSER}_{\text{Cu}} + 12.0 \text{GHSER}_{\text{Mg}}$$

Phase bcc-B2

$$G^*\text{Cu : Mg} = 0.0$$

$$L^0\text{Cu, Mg} = -2500$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = \text{GBCC}_{\text{Cu}}$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Mg}) = G^*\text{Cu : Mg} + 0.5 L_{\text{Cu,Mg}}^0 + 0.5 \text{GBCC}_{\text{Cu}} + 0.5 \text{GBCC}_{\text{Mg}}$$

$$G^{\circ}(T) - 0.5 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = G^{\circ}\text{Cu : Mg} + L_{\text{Cu, Mg}}^0 + 0.5 \text{ GBCC}_{\text{Cu}} + 0.5 \text{ GBCC}_{\text{Mg}}$$

$$G^{\circ}(T) - H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = \text{GBCC}_{\text{Mg}}$$

$$L_{\text{Cu, Mg:Cu:}\square}^{0, \text{bcc}-B2} = L_{\text{Cu, Mg:Mg:}\square}^{0, \text{bcc}-B2} = -G^{\circ}\text{Cu : Mg} + L^0\text{Cu, Mg}$$

$$L_{\text{Cu:Cu, Mg:}\square}^{0, \text{bcc}-B2} = L_{\text{Mg:Cu, Mg:}\square}^{0, \text{bcc}-B2} = -G^{\circ}\text{Cu : Mg} + L^0\text{Cu, Mg}$$

Phase bcc-B2

$$G_{\text{Cu:Mg}}^{\circ} = 0.0$$

$$L_{\text{Cu, Mg}}^0 = -2500$$

$$G^{\circ}(T) - H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 0.0$$

$$G^{\circ}(T) - 0.5 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Mg}) = 2.0 G^{\circ}\text{Cu : Mg}$$

$$G^{\circ}(T) - 0.5 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = 2.0 G^{\circ}\text{Cu : Mg}$$

$$G^{\circ}(T) - H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 0.0$$

Phase bcc-A2

$$L_{\text{Cu, Mg:}\square}^{0, \text{bcc}-A2} = 4.0 L^0\text{Cu, Mg}$$

Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Mg}			T / K
Liquid \rightleftharpoons fcc-A1 + Laves-C15	Eutectic	.209	.069	.313	998.6
Liquid \rightleftharpoons Laves-C15 + CuMg ₂	Eutectic	.595	.356	.667	825.5
Liquid \rightleftharpoons CuMg ₂ + hcp-A3	Eutectic	.839	.667	1.000	759.7
CuMg ₂ \rightleftharpoons Liquid	Congruent	0.666	0.666	...	841.0
Laves-C15 \rightleftharpoons Liquid	Congruent	0.333	0.333	...	1073.5

System Cu-Ni

Solution Phases:

(stable) Liquid, fcc-A1
 (metastable) bcc-A2, hcp-A3

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister

Assessor and Date:

S. an Mey

Publication:

Calphad, **16**, (3), 255-260 (1992).

Thermodynamic properties of the solution phases (J.mol⁻¹)

$$I_{\text{Cu,Ni};\square}^{0,\text{bcc-A2}} = 8047.72 + 3.42217 T$$

$$I_{\text{Cu,Ni};\square}^{1,\text{bcc-A2}} = -2041.3 + 0.99714 T$$

Phase fcc-A1

$$I_{\text{Cu,Ni};\square}^{0,\text{fcc-A1}} = 8047.72 + 3.42217 T$$

$$I_{\text{Cu,Ni};\square}^{1,\text{fcc-A1}} = -2041.3 + 0.99714 T$$

$$T_{\text{c,Cu,Ni};\square}^{0,\text{fcc-A1}} = -935.5$$

$$T_{\text{c,Cu,Ni};\square}^{1,\text{fcc-A1}} = -594.9$$

$$\beta_{\text{Cu,Ni};\square}^{0,\text{mag,fcc-A1}} = -0.7316$$

$$\beta_{\text{Cu,Ni};\square}^{1,\text{mag,fcc-A1}} = -0.3174$$

Phase hcp-A3

$$L_{\text{Cu,Ni};\square}^{0,\text{hcp-A3}} = 8047.72 + 3.42217 T$$

$$L_{\text{Cu,Ni};\square}^{1,\text{hcp-A3}} = -2041.3 + 0.99714 T$$

Phase liquid

$$L_{\text{Cu,Ni}}^{0,\text{liquid}} = 12048.61 + 1.29893 T$$

$$L_{\text{Cu,Ni}}^{1,\text{liquid}} = -1861.61 + 0.94201 T$$

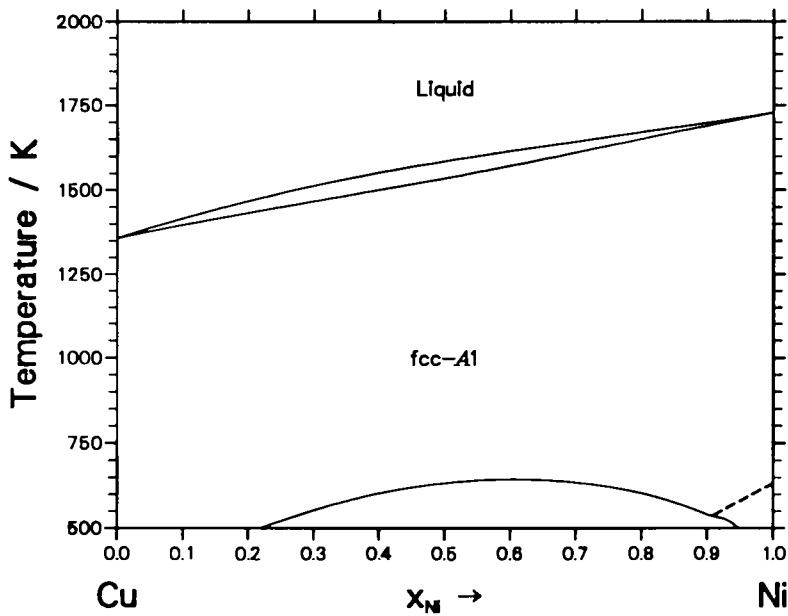


Table I – Invariant Reaction.

Reaction	Type	Compositions x_{Ni}	T / K
$\text{fcc-A1}' \rightleftharpoons \text{fcc-A1}''$	Critical Temp.	0.600 0.600	641.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cu-Ni	(Cu)	Cu	$cF4$ $Fm\bar{3}m$
	(Ni)	Cu	$cF4$ $Fm\bar{3}m$

System Cu–Si

Solution Phases:

(stable) Liquid, bcc-A2, fcc-A1
 (metastable) hcp-A3

Compounds:

(stable) Cu₅₆Si₁₁-γ, Cu₄Si-ε, Cu₁₉Si₆-η, Cu₃₃Si₇-δ
 (metastable) Laves-C15

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 Cu₅₆Si₁₁-γ : Stoichiometric, (Cu)₅₆(Si)
 Cu₄Si-ε : Stoichiometric, (Cu)₄(Si)
 Cu₁₉Si₆-η : Stoichiometric, (Cu)₁₉(Si)₆
 Cu₃₃Si₇-δ : Stoichiometric, (Cu)₃₃(Si)₇
 Laves-C15 : Sublattice model, (Cu,Si)₂(Cu,Si)

Assessor and Date:

M. Jacobs, 1991. Revised by T. Bühler et al. 1997

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-A2

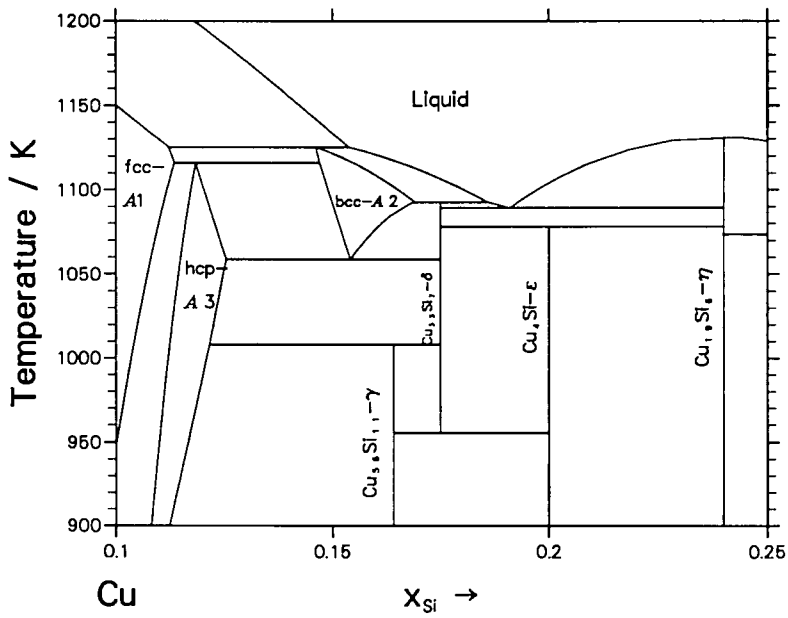
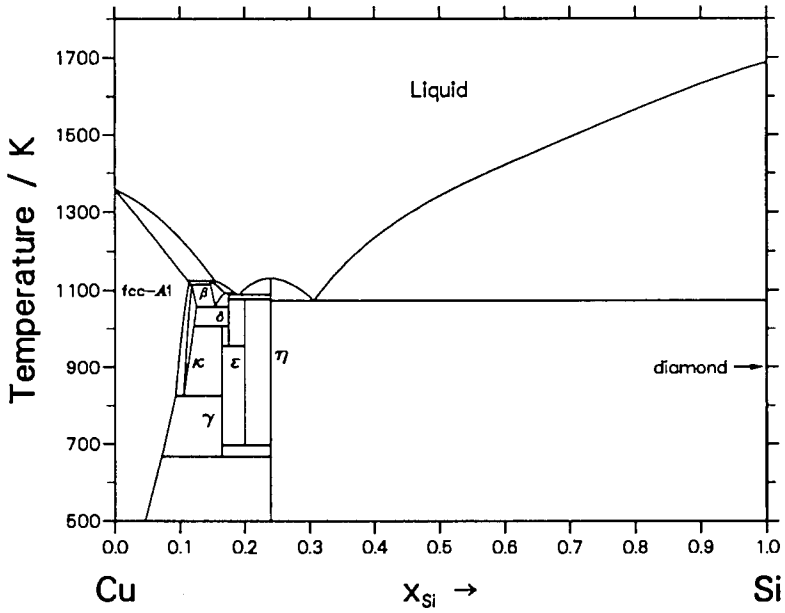
$$L_{\text{Cu,Si};\text{O}}^{0,\text{bcc-A2}} = -21740 + 3.9 T$$

$$L_{\text{Cu,Si};\text{O}}^{1,\text{bcc-A2}} = -40000 - 4.39 T$$

$$L_{\text{Cu,Si};\text{O}}^{2,\text{bcc-A2}} = -100$$

Phase fcc-A1

$$L_{\text{Cu,Si};\text{O}}^{0,\text{fcc-A1}} = -34105.96 - 1.908 T$$



Phase hcp-A3

$$L_{\text{Cu,Si};\square}^{0,\text{hcp-A3}} = -19948 - 2.356 T$$

$$L_{\text{Cu,Si};\square}^{1,\text{hcp-A3}} = -23800 - 1.97 T$$

$$L_{\text{Cu,Si};\square}^{2,\text{hcp-A3}} = -20$$

Phase liquid

$$L_{\text{Cu,Si}}^{0,\text{liquid}} = -39688.86 + 14.27467 T$$

$$L_{\text{Cu,Si}}^{1,\text{liquid}} = -49937.13 + 29.78960 T$$

$$L_{\text{Cu,Si}}^{2,\text{liquid}} = -31810.16 + 18.00804 T$$

Phase Cu₃₃Si₇-δ

$$G^\circ(T) - 33.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 7.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ -200372.4 + 4985.675 T - 955.5312 T \cdot \ln T - 0.101066 T^2 \\ + 4.2396E-06 T^3 + 2968440 T^{-1}$$

Phase Cu₅₆Si₁₁-γ

$$G^\circ(T) - 56.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 11.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 69000 + 405 T - 107.73 T \cdot \ln T + 46.0 \text{GHSER}_{\text{Cu}} \\ + 11.0 \text{GHSER}_{\text{Si}}$$

Phase Cu₄Si-ε

$$G^\circ(T) - 4.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ -39974.35 + 858.5047 T - 154.6764 T \cdot \ln T \\ + 0.01074864 T^2 + 5.1335E-07 T^3 + 386580 T^{-1}$$

Phase Cu₁₉Si₆-η

$$G^\circ(T) - 19.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 6.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ -137488.5 + 3119.537 T - 595.1259 T \cdot \ln T - 0.0619575 T^2 \\ + 2.434E-06 T^3 + 2057075 T^{-1}$$

Phase Laves-C15

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = \\ 15000.0 + 3.0 \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Cu:Si}) \\ 15000.0 + 2.0 \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Cu}) \\ 15000.0 + \text{GHSER}_{\text{Cu}} + 2.0 \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si}) \\ 15000.0 + 3.0 \text{GHSER}_{\text{Si}}$$

$$L_{\text{Cu,Si;Cu}}^{0,\text{Laves-C15}} = L_{\text{Cu,Si;Si}}^{0,\text{Laves-C15}} = 15305 + 20.69 T$$

Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Si}	T / K
Liquid + fcc-A1 \rightleftharpoons β^*	Peritectic	.154 .112 .146	1125.4
fcc-A1 + β^* \rightleftharpoons β^{**}	Peritectoid	.113 .147 .118	1115.9
β^* \rightleftharpoons β^{**} + δ	Eutectoid	.154 .125 .175	1058.6
Liquid + β^* \rightleftharpoons δ	Peritectic	.186 .169 .175	1092.7
Liquid \rightleftharpoons δ + η	Eutectic	.191 .175 .240	1089.2
η + δ \rightleftharpoons ϵ	Peritectoid	.175 .240 .200	1077.9
δ \rightleftharpoons β^{***} + ϵ	Eutectoid	.175 .164 .200	955.6
β^{**} + δ \rightleftharpoons β^{***}	Peritectoid	.121 .175 .164	1008.3
ϵ \rightleftharpoons β^{***} + η	Eutectoid	.200 .164 .240	696.5
β^{**} \rightleftharpoons fcc-A1 + β^{***}	Eutectoid	.105 .093 .164	825.5
β^{***} \rightleftharpoons fcc-A1 + η	Eutectoid	.164 .072 .240	667.8
Liquid \rightleftharpoons η + diamond	Eutectic	.306 .240 1.000	1073.7
η \rightleftharpoons Liquid	Congruent	.240 .240	1132.0

* $\beta \equiv$ bcc-A2, ** $\kappa \equiv$ hcp-A3, *** $\gamma \equiv$ cub-A13

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Cu-Si	(Cu)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Si)	diamond	$cF8$ $Fd\bar{3}m$	M 8	
	κ	Mg	$hP2$ $P6_3/mmc$	M 2	hcp-A3 Cu ₇ Si in [91Vil]
	Cu ₃ Si		t^{**}		η, η', η'' in Mas2 denoted Cu ₄ Si-c
	δ		$hP72$		
	γ	β -Mn	$cP20$ $P4_132$	M ₁ 8 M ₂ 12	
	β	W	$cF2$ $Im\bar{3}m$	M 2	bcc-A2

System Cu–Y

Solution Phases:

Liquid, bcc–A2, hcp–A3, Cu₆Y

Compound:

Cu₄Y, Cu₆Y, Cu₇Y₂, Cu₂Y–R, Cu₂Y–H, CuY

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc–A2	:	Substitutional, Redlich–Kister
hcp–A3	:	Substitutional, Redlich–Kister
Cu ₆ Y	:	Sublattice model, (Cu) ₅ (Cu ₂ ,Y)
Cu ₄ Y	:	Stoichiometric, (Cu) ₄ (Y)
Cu ₇ Y ₂	:	Stoichiometric, (Cu) ₇ (Y) ₂
Cu ₂ Y–R	:	Stoichiometric, (Cu) ₂ (Y)
Cu ₂ Y–H	:	Stoichiometric, (Cu) ₂ (Y)
CuY	:	Stoichiometric, (Cu)(Y)

Assessor and Date:

T. Jantzen, 1997.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc–A2

$$L_{\text{Cu},\text{Y};\square}^{0,\text{bcc-A2}} = 80.0 \text{ T}$$

Phase hcp–A3

$$L_{\text{Cu},\text{Y};\square}^{0,\text{hcp-A3}} = 80.0 \text{ T}$$

Phase liquid

$$L_{\text{Cu},\text{Y}}^{0,\text{liquid}} = -88958.06 + 21.5667 \text{ T}$$

$$L_{\text{Cu},\text{Y}}^{1,\text{liquid}} = -33607.31 + 3.10462 \text{ T}$$

$$L_{\text{Cu},\text{Y}}^{2,\text{liquid}} = 8083.16 - 0.74669 \text{ T}$$

Phase fcc-A1

$$L_{\text{Cu},\text{Y}}^{0,\text{fcc-A1}} = 80.0 T$$

Phase Cu₂Y-R

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Y}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 65324.22 + 6.03462 T + 2.0 \text{ GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Y}}$$

Phase Cu₂Y-H

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Y}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 51788.22 - 5.96538 T + 2.0 \text{ GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Y}}$$

Phase Cu₄Y

$$G^\circ(T) - 4.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Y}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 89328.5 + 8.25205 T + 4.0 \text{ GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Y}}$$

Phase Cu₆Y

$$G^\circ(T) - 7.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}_2) = \\ 35000.0 + 7.0 \text{ GHSER}_{\text{Cu}} \\ G^\circ(T) - 5.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Y}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 89797.58 + 8.2954 T + 5.0 \text{ GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Y}} \\ L_{\text{Cu:Cu}_2,\text{Y}}^{0,\text{Cu}_6\text{Y}} = - 34386.27 + 3.17656 T$$

Phase Cu₇Y₂

$$G^\circ(T) - 7.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Y}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 168519.6 + 15.56757 T + 7.0 \text{ GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Y}}$$

Phase CuY

$$G^\circ(T) - H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Y}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 44616.68 + 4.12162 T + \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Y}}$$

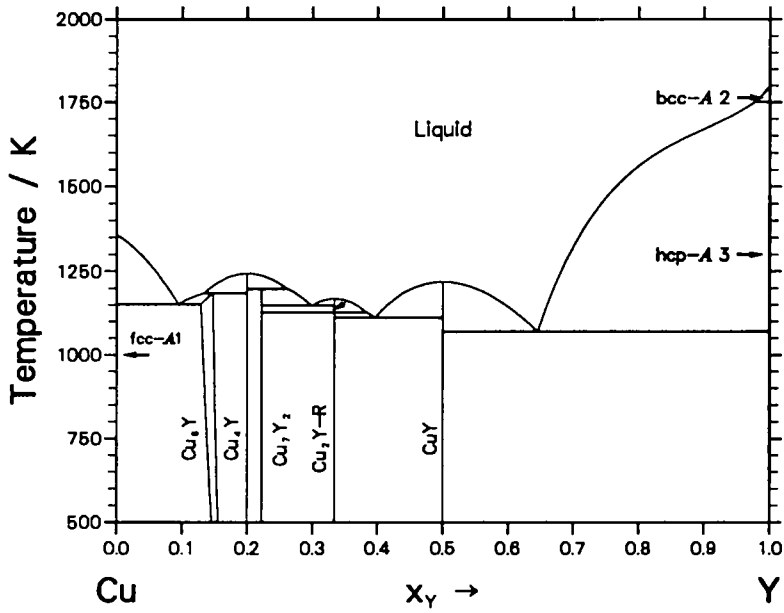


Table I - Invariant Reactions.

Reaction	Type	Compositions x_Y			T / K
Liquid \rightleftharpoons CuY + hcp-A3	Eutectic	.646	.646	1.000	1070.0
Liquid \rightleftharpoons Cu ₂ Y-R + CuY	Eutectic	.396	.333	.500	1113.0
Liquid \rightleftharpoons Cu ₂ Y-H + Cu ₇ Y ₂	Eutectic	.299	.222	.333	1148.6
Liquid \rightleftharpoons Cu ₄ Y + Cu ₇ Y ₂	Peritectic	.262	.200	.222	1198.0
Liquid + Cu ₄ Y \rightleftharpoons Cu ₆ Y	Peritectic	.133	.200	.147	1184.0
Liquid \rightleftharpoons fcc-A1 + Cu ₆ Y	Eutectic	.094	.000	.129	1153.0
hcp-A3 \rightleftharpoons bcc-A2	Polymorphic	1.000	1.000	1752.0
Cu ₂ Y-R \rightleftharpoons Cu ₂ Y-H	Polymorphic	.333	.333	1128.0
Liquid \rightleftharpoons Cu ₄ Y	Congruent	.200	.200	1224.0
Liquid \rightleftharpoons Cu ₂ Y-H	Congruent	.333	.333	1149.0
Liquid \rightleftharpoons CuY	Congruent	.500	.500	1220.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Cu-Y	(Cu)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Y)	W	$cI2$ $Im\bar{3}m$	M 4	
	(Y)	Mg	$hP2$ $P6_3/mmc$	M 2	
	Cu ₆ Y				not in [91Vil]
	Cu ₅ Y	CaCu ₅	$hP6$ $P6/mmm$	Y 1 Cu ₁ 2 Cu ₂ 3	quoted as metastable in 90Mas]
	Cu ₄ Y	CaCu ₅ ?	$hP6$ $P6/mmm$		not quoted in [91Vil]
	Cu ₇ Y ₂				not in [91Vil]
	Cu ₂ Y	CeCu ₂	$oI12$ $Imma$	Y 4 Cu 8	
	CuY	CsCl	$cP2$ $Pm\bar{3}m$	Cu 1 Y 1	bcc-B2

System Cu–Zn

Solution Phases:

(stable) : Liquid, bcc-*A2*, bcc-*B2*, fcc-*A1*, hcp-*A3*(CuZn- ϵ),
hcp-Zn

:

Solution Phases:

(stable) : CuZn- γ
(metastable) : Laves-*C14*, Laves-*C15*, Laves-*C36*

Modelling:

Liquid : Substitutional, Redlich–Kister
 fcc-*A1* : Substitutional, Redlich–Kister
 hcp-*A3*(CuZn- ϵ) : Substitutional, Redlich–Kister
 hcp-Zn : Substitutional, Redlich–Kister
 CuZn- γ : Sublattice, (Cu,Zn)₂(Cu,Zn)₂(Cu)₃(Zn)₆
 bcc-*A2* : see below
 bcc-*B2* : Sublattice model, (Cu,Zn)_{0.5}(Cu,Zn)_{0.5}(\square)₃
 Two descriptions of the bcc-*A2*:bcc-*B2* order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
 Two descriptions of the bcc-*A2*:bcc-*B2* order-disorder
 Laves-*C14* : Sublattice model, (Cu,Zn)₂(Cu,Zn)
 Laves-*C15* : Sublattice model, (Cu,Zn)₂(Cu,Zn)
 Laves-*C36* : Sublattice model, (Cu,Zn)₂(Cu,Zn)

Assessor and Date:

M. Kowalski, and P.J. Spencer,

Publication:

J. Phase Equil., 14, 4, 432-438 (1993).

Comments:

Based on Kowalski's data, a new assessment was performed to differentiate the two hexagonal forms of Zn.

Thermodynamic properties of the solution and compound phases(J.mol⁻¹)**Phase fcc-A1**

$$L_{\text{Cu,Zn};\square}^{0,\text{fcc-A1}} = -42803.75 + 10.02258 T$$

$$L_{\text{Cu,Zn};\square}^{1,\text{fcc-A1}} = 2936.39 - 3.05323 T$$

$$L_{\text{Cu,Zn};\square}^{2,\text{fcc-A1}} = 9034.2 - 5.39314 T$$

Phase hcp-A3

$$L_{\text{Cu,Zn};\square}^{0,\text{hcp-A3}} = -36475 + 4.896 T$$

$$L_{\text{Cu,Zn};\square}^{0,\text{hcp-A3}} = 24790.0 - 10.135 T$$

Phase hcp-Zn

$$L_{\text{Cu,Zn}}^{0,\text{hcp-Zn}} = -14432.17 - 10.7814 T$$

Phase liquid

$$L_{\text{Cu,Zn}}^{0,\text{liquid}} = -40695.54 + 12.65269 T$$

$$L_{\text{Cu,Zn}}^{1,\text{liquid}} = 4402.72 - 6.55425 T$$

$$L_{\text{Cu,Zn}}^{2,\text{liquid}} = 7818.1 - 3.25416 T$$

Phase bcc-B2

$$G_{\text{Cu};\text{Zn};\square}^* = -3085.0$$

$$L_{\text{Cu,Zn}}^0 = -12898.97 + 3.26598 T$$

$$L_{\text{Cu,Zn}}^1 = 945.265 - 0.80679 T$$

$$L_{\text{Cu,Zn}}^2 = 1921.485 - 1.86969 T$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu};\text{Cu};\square) = \text{GBCC}_{\text{Cu}}$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Cu};\text{Zn};\square) = G_{\text{Cu};\text{Zn}}^* + L_{\text{Cu,Zn}}^0 + 0.5 \text{GBCC}_{\text{Cu}} + 0.5 \text{GBCC}_{\text{Zn}}$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Cu:}\square) =$$

$$G_{\text{Cu:Zn:}\square}^* + L_{\text{Cu,Zn}}^0 + 0.5 \text{ GBCC}_{\text{Cu}} + 0.5 \text{ GBCC}_{\text{Zn}}$$

$$G^\circ(T) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn:}\square) = \text{GBCC}_{\text{Zn}}$$

$$L_{\text{Cu,Zn:Cu:}\square}^{0,\text{bcc}-\text{B}2} = L_{\text{Cu:Cu,Zn:}\square}^{0,\text{bcc}-\text{B}2} = -G_{\text{Cu:Zn:}\square}^* + L_{\text{Cu,Zn}}^0 + 3.0 L_{\text{Cu,Zn}}^1 + 3.0 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Cu:}\square}^{1,\text{bcc}-\text{B}2} = L_{\text{Cu:Cu,Zn:}\square}^{1,\text{bcc}-\text{B}2} = L_{\text{Cu,Zn}}^1 + 4.0 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Cu:}\square}^{2,\text{bcc}-\text{B}2} = L_{\text{Cu:Cu,Zn:}\square}^{2,\text{bcc}-\text{B}2} = L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Zn:}\square}^{0,\text{bcc}-\text{B}2} = L_{\text{Zn:Cu,Zn:}\square}^{0,\text{bcc}-\text{B}2} = -G_{\text{Cu:Zn:}\square}^* + L_{\text{Cu,Zn}}^0 - 3.0 L_{\text{Cu,Zn}}^1 + 3.0 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Zn:}\square}^{1,\text{bcc}-\text{B}2} = L_{\text{Zn:Cu,Zn:}\square}^{1,\text{bcc}-\text{B}2} = L_{\text{Cu,Zn}}^1 - 4.0 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Zn:}\square}^{2,\text{bcc}-\text{B}2} = L_{\text{Zn:Cu,Zn:}\square}^{2,\text{bcc}-\text{B}2} = L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Cu,Zn:}\square}^{0,\text{bcc}-\text{B}2} = -24.0 L_{\text{Cu,Zn}}^2$$

Phase bcc-B2

$$G_{\text{Cu:Zn:}\square}^* = -3085.0$$

$$L_{\text{Cu,Zn}}^0 = -12898.97 + 3.26598 T$$

$$L_{\text{Cu,Zn}}^1 = 945.265 - 0.80679 T$$

$$L_{\text{Cu,Zn}}^2 = 1921.485 - 1.86969 T$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Cu:Cu:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn:}\square) = 2.0 G_{\text{Cu:Zn:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Cu:}\square) = 2.0 G_{\text{Cu:Zn:}\square}^*$$

$$G^\circ(T) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Cu,Zn:}\square}^{0,\text{bcc}-\text{A}2} = 4.0 L_{\text{Cu,Zn}}^0$$

$$L_{\text{Cu,Zn:}\square}^{1,\text{bcc}-\text{A}2} = 8.0 L_{\text{Cu,Zn}}^1$$

$$L_{\text{Cu,Zn:}\square}^{2,\text{bcc}-\text{A}2} = 16.0 L_{\text{Cu,Zn}}^2$$

Phase CuZn- γ

$$K4 = -11552.71 - 1.67824 T$$

$$K5 = 15732.3 - 10.26575 T$$

$$K6 = 37289.2 - 13.05259 T$$

$$G^\circ(T) - 7.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu:Cu:Cu:Zn}) = 13.0 K4 + 2.0 K5 + 7.0 \text{GHSER}_{\text{Cu}} + 6.0 \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 5.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 8.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Cu:Cu:Zn}) = 13.0 K4 + 2.0 K5 + 2.0 K6 + 5.0 \text{GHSER}_{\text{Cu}} + 8.0 \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 5.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 8.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn:Cu:Zn}) = 13.0 K4 + 5.0 \text{GHSER}_{\text{Cu}} + 8.0 \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 10.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn:Cu:Zn}) = 13.0 K4 + 2.0 K6 + 3.0 \text{GHSER}_{\text{Cu}} + 10.0 \text{GHSER}_{\text{Zn}}$$

Phase Laves-C14

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn}) = 15000.0 + 2.0 \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Cu}) = 15000.0 + \text{GHSER}_{\text{Cu}} + 2.0 \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn}) = 15000.0 + 3.0 \text{GHSER}_{\text{Zn}}$$

$$L_{\text{Cu,Zn:Cu}}^{0,\text{Laves-C14}} = L_{\text{Cu,Zn:Zn}}^{0,\text{Laves-C14}} = -75305.48$$

Phase Laves-C15

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn}) = 15000.0 + 2.0 \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Cu}) = 15000.0 + \text{GHSER}_{\text{Cu}} + 2.0 \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn}) = 15000.0 + 3.0 \text{GHSER}_{\text{Zn}}$$

$$L_{\text{Cu,Zn:Cu}}^{0,\text{Laves-C15}} = L_{\text{Cu,Zn:Zn}}^{0,\text{Laves-C15}} = -78824.62$$

$$L_{\text{Cu,Zn:Cu}}^{1,\text{Laves-C15}} = L_{\text{Cu,Zn:Zn}}^{0,\text{Laves-C15}} = 25529.06$$

Phase Laves-C36

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ, \text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn}) = 15000.0 + 2.0 \text{ GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ, \text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Cu}) = 15000.0 + \text{GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ, \text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Cu,Zn:Cu}}^{0, \text{Laves-C36}} = L_{\text{Cu,Zn:Zn}}^{0, \text{Laves-C36}} = -90226.26$$

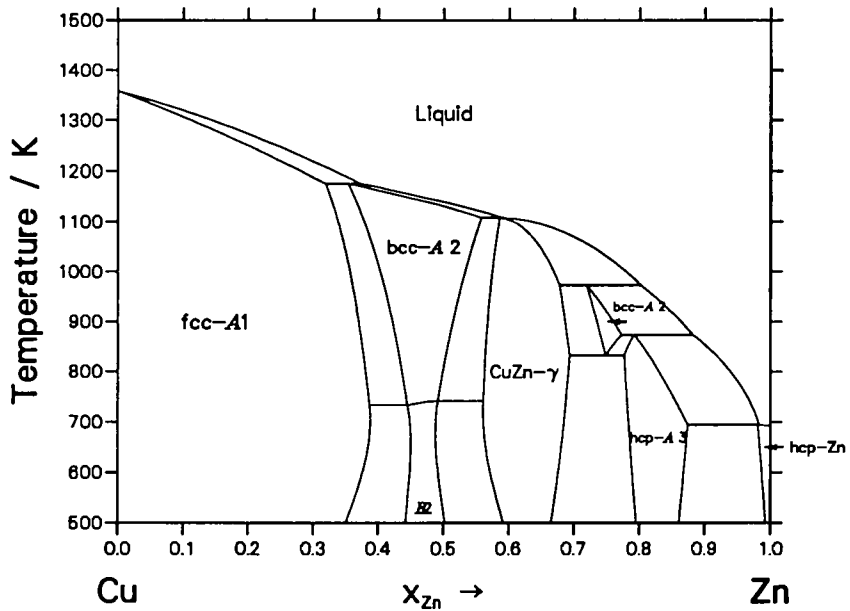


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zn}	T / K
Liquid + fcc-A1 \rightleftharpoons bcc-A2	Peritectic	.373 .319 .353	1175.3
Liquid + bcc-A2 \rightleftharpoons CuZn- γ	Peritectic	.592 .558 .586	1108.3
Liquid + CuZn- γ \rightleftharpoons bcc-A2	Peritectic	.802 .678 .719	972.5
Liquid + bcc-A2 \rightleftharpoons hcp-A3	Peritectic	.882 .773 .792	873.4
bcc-A2 \rightleftharpoons CuZn- γ + hcp-A3	Eutectoid	.748 .693 .777	831.9
Liquid + hcp-A3 \rightleftharpoons hcp-Zn	Peritectic	.983 .874 .981	694.4

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Cu-Zn	(Cu)	Cu	$cF4$ $Pm\bar{3}m$	M 4	
	(Zn)	Mg	$hP2$ $P6_3/mmc$	M 2	
	β	W	$cI2$ $Im\bar{3}m$	M 2	bcc-A2
	β'	CsCl	$cP2$ $Pm\bar{3}m$	Cu 1 Zn 1	bcc-B2
	δ	$CuZn_2$	$hP3$ $P\bar{6}$	Cu 1 Zn ₁ 1 Zn ₂ 1	assumed as bcc-A2
	ϵ	Mg	$hP2$ $P6_3mmc$	M 2	CuZn-A3
	γ	Cu_5Zn_8	$cI52$ $I\bar{4}3m$	Cu ₁ 8 Cu ₂ 12 Zn ₁ 8 Zn ₂ 24	Cu_5Zn

System Cu–Zr

Solution Phases:

Liquid, bcc-A2, hcp-A3

Compounds:

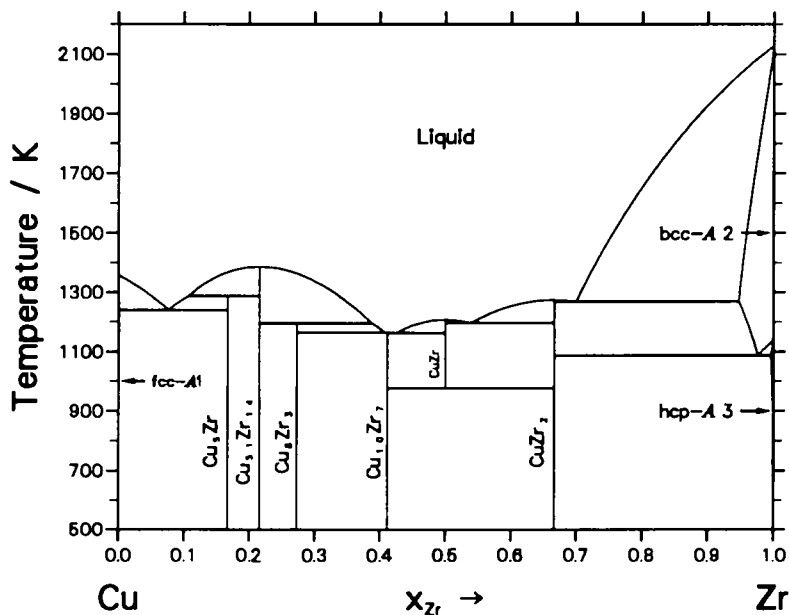
Cu_5Zr , $\text{Cu}_{51}\text{Zr}_{14}$, $\text{Cu}_{10}\text{Zr}_7$, CuZr , CuZr_2 , Cu_8Zr_3

Modelling:

Liquid	:	Substitutional, Redlich–Kister
Cu_5Zr	:	Stoichiometric, $(\text{Cu})_5(\text{Zr})$
$\text{Cu}_{51}\text{Zr}_{14}$:	Stoichiometric, $(\text{Cu})_{51}(\text{Zr})_{14}$
$\text{Cu}_{10}\text{Zr}_7$:	Stoichiometric, $(\text{Cu})_{10}(\text{Zr})_7$
Cu_8Zr_3	:	Stoichiometric, $(\text{Cu})_8(\text{Zr})_3$
CuZr	:	Stoichiometric, $(\text{Cu})(\text{Zr})$
CuZr_2	:	Stoichiometric, $(\text{Cu})(\text{Zr})_2$

Assessor and Date:

K. Zeng, and M. Härmäläinen 1993



Thermodynamic properties of the solution and compound phases (J.mol⁻¹)**Phase bcc-A2**

$$I_{\text{Cu,Zr;O}}^{0,\text{bcc-A2}} = -7381.13$$

Phase fcc-A1

$$I_{\text{Cu,Zr;O}}^{0,\text{fcc-A1}} = 2233$$

Phase hcp-A3

$$I_{\text{Cu,Zr;O}}^{0,\text{hcp-A3}} = 11336.85$$

Phase liquid

$$I_{\text{Cu,Zr}}^{0,\text{liquid}} = -61685.53 + 11.29235 T$$

$$I_{\text{Cu,Zr}}^{1,\text{liquid}} = -8830.66 + 5.04565 T$$

Phase Cu₁₀Zr₇

$$G^\circ(T) - 10.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - 7.0 H_{\text{Zr}}^{0,\text{hcp-A1}}(298.15 \text{ K}) = \\ -241750.0 + 10.0 \text{ GHSE}_{\text{Cu}} + 7.0 \text{ GHSE}_{\text{Zr}}$$

Phase Cu₅₁Zr₁₄

$$G^\circ(T) - 51.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - 14.0 H_{\text{Zr}}^{0,\text{hcp-A1}}(298.15 \text{ K}) = \\ -843412.7 + 51.0 \text{ GHSE}_{\text{Cu}} + 14.0 \text{ GHSE}_{\text{Zr}}$$

Phase Cu₅Zr

$$G^\circ(T) - 5.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Zr}}^{0,\text{hcp-A1}}(298.15 \text{ K}) = \\ -61794 + 5.0 \text{ GHSE}_{\text{Cu}} + \text{GHSE}_{\text{Zr}}$$

Phase Cu₈Zr₃

$$G^\circ(T) - 8.0 H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Zr}}^{0,\text{hcp-A1}}(298.15 \text{ K}) = \\ -148063.1 + 8.0 \text{ GHSE}_{\text{Cu}} + 3.0 \text{ GHSE}_{\text{Zr}}$$

Phase CuZr

$$G^\circ(T) - H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Zr}}^{0,\text{hcp-A1}}(298.15 \text{ K}) = \\ -20104.24 - 7.63196 T + \text{GHSE}_{\text{Cu}} + \text{GHSE}_{\text{Zr}}$$

Phase CuZr₂

$$G^\circ(T) - H_{\text{Cu}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Zr}}^{0,\text{hcp-A1}}(298.15 \text{ K}) = \\ -43904.01 + 5.19051 T + \text{GHSE}_{\text{Cu}} + 2.0 \text{ GHSE}_{\text{Zr}}$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zr}			T / K
Liquid \rightleftharpoons fcc-A1 + Cu ₅ Zr	Eutectic	.078	.001	.167	1240.8
Liquid + Cu ₅₁ Zr ₁₄ \rightleftharpoons Cu ₅ Zr	Peritectic	.107	.215	.167	1287.5
Cu ₅₁ Zr ₁₄ \rightleftharpoons Liquid	Congruent	.215	.215	1386.0
Liquid + Cu ₅₁ Zr ₁₄ \rightleftharpoons Cu ₈ Zr ₃	Peritectic	.388	.273	.215	1195.3
Liquid \rightleftharpoons Cu ₈ Zr ₃ + Cu ₁₀ Zr ₇	Eutectic	.408	.273	.412	1164.2
Cu ₁₀ Zr ₇ \rightleftharpoons Liquid	Congruent	.412	.412	1164.2
Liquid \rightleftharpoons Cu ₁₀ Zr ₇ + CuZr	Eutectic	.425	.412	.500	1163.2
CuZr \rightleftharpoons Cu ₁₀ Zr ₇ + CuZr ₂	Eutectoid	.500	.412	.667	976.7
Liquid \rightleftharpoons CuZr + CuZr ₂	Eutectic	.538	.500	.667	1196.7
CuZr \rightleftharpoons Liquid	Congruent	.500	.500	1208.5
Liquid \rightleftharpoons CuZr ₂ + bcc-A2	Eutectic	.700	.666	.947	1269.5
CuZr ₂ \rightleftharpoons Liquid	Congruent	.666	.666	1275.0
bcc-A2 \rightleftharpoons CuZr ₂ + hcp-A3	Eutectoid	.975	.667	.992	1095.2

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices		Comments
Cu-Zr	(Cu)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M	4	
	(Zr)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M	2	
	(Zr)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M	4	
	CuZr	ClCs	<i>cP2</i> <i>Pm$\bar{3}$m</i>	M ₁ M ₂	1 1	bcc-B2
	CuZr ₂	MoSi ₂	<i>tI6</i> <i>I4/mmm</i>	Cu Zr	2 4	
	Cu ₁₀ Zr ₇	Ni ₁₀ Zr ₇	<i>oC68</i> <i>Aba2</i>			
	Cu ₉ Zr ₂		<i>tP24</i> <i>P4/m</i>			<i>o</i> ** in [91Vil]
	Cu ₅ Zr	AuBe ₅	<i>Cf24</i> <i>F$\bar{4}$3m</i>	Cu ₁ Cu ₂ Zr	4 16 4	
	Cu ₅₁ Zr ₁₄	Ag ₅₁ Gd ₁₄	<i>hP65</i> <i>P6/m</i>			<i>hP68</i> in [91Vil]
	Cu ₈ Zr ₃	Cu ₈ Hf ₃	<i>oP44</i> <i>Pnma</i>			

System Fe-Mg

Solution Phases:

Liquid, fcc-A1, bcc-A2, hcp-A3

Modelling:

Liquid : Substitutional, Redlich-Kister
fcc-A1 : Substitutional, Redlich-Kister
bcc-A2 : Substitutional, Redlich-Kister
hcp-A3 : Substitutional, Redlich-Kister

Assessor and Date:

J. Tibballs (1991)

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Fe,Mg};\square}^{0,\text{bcc-A2}} = 65700.0$$

Phase fcc-A1

$$L_{\text{Fe,Mg};\square}^{0,\text{fcc-A1}} = 65200.0$$

Phase hcp-A3

$$L_{\text{Fe,Mg};\square}^{0,\text{hcp-A3}} = 92400.0$$

Phase liquid

$$L_{\text{Fe,Mg}}^{0,\text{liquid}} = 61343.0 + 1.5 T$$

$$L_{\text{Fe,Mg}}^{1,\text{liquid}} = -2700.0$$

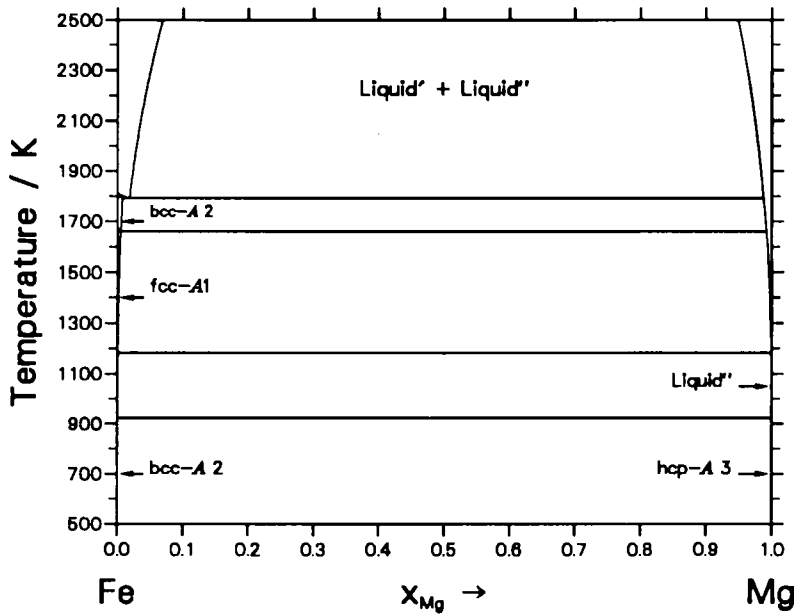


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Mg}	T / K
Liquid' \rightleftharpoons bcc-A2 + Liquid''	Monotectic	.018 .008 .987	1791.4
Liquid'' + bcc-A2 \rightleftharpoons fcc-A1	Degenerate	.992 .005 .005	1661.6
Liquid'' + bcc-A2 \rightleftharpoons fcc-A1	Degenerate	.999 .001 .001	1183.4
Liquid'' + bcc-A2 \rightleftharpoons hcp-A3	Degenerate	1.000 .000 1.000	922.9

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol] Space Group
Fe-Mg	(Fe)	Cu	cF_4 $Pm\bar{3}m$
	(Fe)	W	$cI2$ $Im\bar{3}m$
	(Mg)	Mg	$hP2$ $P6_3/mmc$

System Fe-Mn

Solution Phases:

(stable)

Liquid, bcc-A2, cbcc-A12, cub-A13, fcc-A1

Solution Phases:

(metastable)

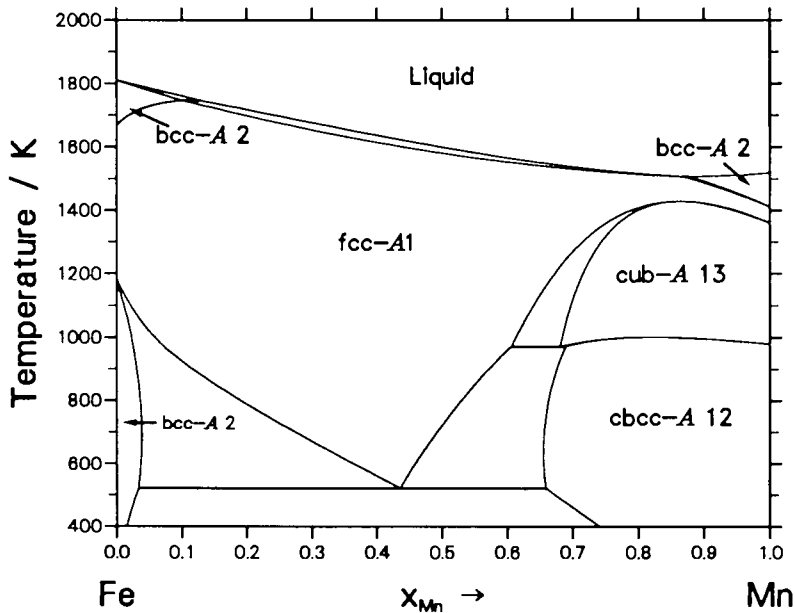
hcp-A3

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
bcc-A12	:	Substitutional, Redlich-Kister
cub-A13	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister

Assessor and Date:

Scientific Group Thermodata Europe Database



Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Fe,Mn};\square}^{0,\text{bcc-A2}} = -2759 + 1.237 T$$

$$T_{\text{c,Fe,Mn};\square}^{0,\text{bcc-A2}} = 123$$

$$\beta_{\text{Fe,Mn};\square}^{0,\text{mag,bcc-A2}} = 0$$

Phase cbcc-A12

$$L_{\text{Fe,Mn};\square}^{0,\text{cbcc-A12}} = -10184$$

Phase cub-A13

$$L_{\text{Fe,Mn};\square}^{0,\text{cub-A13}} = -11518 + 2.819 T$$

Phase fcc-A1

$$L_{\text{Fe,Mn};\square}^{0,\text{fcc-A1}} = -7762 + 3.865 T$$

$$L_{\text{Fe,Mn};\square}^{1,\text{fcc-A1}} = -259$$

$$T_{\text{c,Fe,Mn};\square}^{0,\text{fcc-A1}} = -2282$$

$$T_{\text{c,Fe,Mn};\square}^{1,\text{fcc-A1}} = -2068$$

$$\beta_{\text{Fe,Mn};\square}^{0,\text{mag,fcc-A1}} = 0$$

Phase liquid

$$L_{\text{Fe,Mn}}^{0,\text{liquid}} = -3950 + 0.489 T$$

$$L_{\text{Fe,Mn}}^{1,\text{liquid}} = 1145$$

Phase hcp-A3

$$L_{\text{Fe,Mn}}^{0,\text{hcp-A3}} = -5582 + 3.865 T$$

$$L_{\text{Fe,Mn}}^{1,\text{hcp-A3}} = 273$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Mn}	T / K
$cub-A13 \rightleftharpoons fcc-A1 + cbcc-A12$	Eutectoid	.681 .606 .690	973.2
$fcc-A1 \rightleftharpoons bcc-A2 + cbcc-A12$	Eutectoid	.436 .033 .659	521.3
Liquid + $bcc-A2 \rightleftharpoons fcc-A1$	Peritectic	.100 .129 .129	1746.8
Liquid + $bcc-A2 \rightleftharpoons fcc-A1$	Peritectic	.867 .877 .875	1507.2

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Fe-Mn	(Fe)	Cu	$cF4$ $Pm\bar{3}m$	
	(Fe)	W	$cI2$ $Im\bar{3}m$	
	α -Mn	α -Mn	$c58$ $I\bar{4}3m$	cbcc-A12
	β -Mn	β -Mn	$cP20$ $P4_132$	cub-A13
	γ -Mn	Cu	$cF4$ $Fm\bar{3}m$	
	δ -Mn	W	$cI2$ $Im\bar{3}m$	

System Fe–Si

Solution Phases:

Liquid, bcc-A2, bcc-B2, fcc-A1

Compounds:

Fe₅Si₃, FeSi, Fe₂Si, FeSi₂-L, FeSi₂-H

Modelling:

Liquid	:	Substitutional, Redlich–Kister
fcc-A1	:	Substitutional, Redlich–Kister
bcc-B2	:	Sublattice model , (Fe,Si) _{0.5} (Fe,Si) _{0.5} (□) ₃ Two descriptions of the bcc-A2: bcc-B2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
bcc-A2	:	see bcc-B2
Fe ₂ Si	:	Stoichiometric, (Fe) ₂ (Si)
Fe ₅ Si ₃	:	Stoichiometric, (Fe) ₅ (Si) ₃
FeSi ₂ -L	:	Stoichiometric, (Fe)(Si) ₂
FeSi ₂ -H	:	Stoichiometric, (Fe) ₃ (Si) ₇
FeSi	:	Stoichiometric, (Fe)(Si)

Assessor and Date:

J. Lacaze, and B. Sundman

Publication:

Met. Trans., **22A**, (10), 2211-2223 (1991).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Fe₂Si

$$G^{\circ}(T) - 2.0 H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = -71256.6 - 10.62 T + 2.0 \text{ GHSE}_{\text{Fe}} + \text{GHSE}_{\text{Si}}$$

Phase Fe₅Si₃

$$G^{\circ}(T) - 5.0 H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 3.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = \\ - 241144 + 2.16 T + 5.0 \text{ GHSER}_{\text{Fe}} + 3.0 \text{ GHSER}_{\text{Si}}$$

Phase FeSi₂-L

$$G^{\circ}(T) - H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 2.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = \\ - 82149.0 + 10.44 T + \text{GHSER}_{\text{Fe}} + 2.0 \text{ GHSER}_{\text{Si}}$$

Phase FeSi₂-H

$$G^{\circ}(T) - 3.0 H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 7.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = \\ - 196490 - 9.2 T + 3.0 \text{ GHSER}_{\text{Fe}} + 7.0 \text{ GHSER}_{\text{Si}}$$

Phase FeSi

$$G^{\circ}(T) - H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = \\ - 72761.2 + 4.44 T + \text{GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Si}}$$

Phase liquid

$$L_{\text{Fe, Si}}^{0, \text{liquid}} = - 164434.6 + 41.9773 T$$

$$L_{\text{Fe, Si}}^{1, \text{liquid}} = - 21.523 T$$

$$L_{\text{Fe, Si}}^{2, \text{liquid}} = - 18821.542 + 22.07 T$$

$$L_{\text{Fe, Si}}^{3, \text{liquid}} = 9695.8$$

Phase fcc-A1

$$L_{\text{Fe, Si:}\square}^{0, \text{fcc-A1}} = - 125247.7 + 41.166 T$$

$$L_{\text{Fe, Si:}\square}^{1, \text{fcc-A1}} = - 142707.6$$

$$L_{\text{Fe, Si:}\square}^{2, \text{fcc-A1}} = 89907.3$$

Phase bcc-B2

$$G^{\circ}(T) - H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Fe:Fe:}\square) = \text{GHSER}_{\text{Fe}}$$

$$T_{\text{c, Fe:Fe}\square}^{\text{bcc-B2}} = 1043 \quad \beta_{\text{c, Fe:Fe}\square}^{\text{bcc-B2}} = 2.22$$

$$G^{\circ}(T) - 0.5 H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 0.5 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Fe:Si:}\square) = \\ - 48761.565 + 11.62 T + 0.5 \text{ GHSER}_{\text{Fe}} + 0.5 \text{ GBCC}_{\text{Si}}$$

$$T_{\text{c, Fe:Si}\square}^{0, \text{bcc-B2}} = 521.5 \quad \beta_{\text{c, Si:Fe}\square}^{0, \text{bcc-B2}} = 1.11$$

$$G^\circ(T) - 0.5 H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 0.5 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Si:Fe:}\square) = -48761.565 + 11.62 T + 0.5 \text{ GHSER}_{\text{Fe}} + 0.5 \text{ GBCC}_{\text{Si}}$$

$$T_{\text{c, Si:Fe:}\square}^{0, \text{bcc-B2}} = 521.5 \quad \beta_{\text{c, Si:Fe:}\square}^{0, \text{bcc-B2}} = 1.11$$

$$G^\circ(T) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si:}\square) = \text{GBCC}_{\text{Si}}$$

$$L_{\text{Fe, Si:Fe:}\square}^{0, \text{bcc-B2}} = L_{\text{Fe, Fe, Si:}\square}^{0, \text{bcc-B2}} = -50771 + 11.62 T$$

$$L_{\text{Fe, Si:Fe:}\square}^{1, \text{bcc-B2}} = L_{\text{Fe, Fe, Si:}\square}^{1, \text{bcc-B2}} = 4016$$

$$L_{\text{Fe, Si:Fe:}\square}^{2, \text{bcc-B2}} = L_{\text{Fe, Fe, Si:}\square}^{2, \text{bcc-B2}} = 3890$$

$$L_{\text{Fe, Si:Si}\square}^{0, \text{bcc-B2}} = L_{\text{Si: Fe, Si:}\square}^{0, \text{bcc-B2}} = 18493 + 11.62 T$$

$$L_{\text{Fe, Si:Si}\square}^{1, \text{bcc-B2}} = L_{\text{Si: Fe, Si:}\square}^{1, \text{bcc-B2}} = -27104$$

$$L_{\text{Fe, Si:Si}\square}^{2, \text{bcc-B2}} = L_{\text{Si: Fe, Si:}\square}^{2, \text{bcc-B2}} = 3890$$

$$L_{\text{Fe, Si:Fe, Si:}\square}^{0, \text{bcc-B2}} = -93360$$

$$T_{\text{c, Fe, Si:Fe:}\square}^{0, \text{bcc-B2}} = T_{\text{c, Fe: Fe, Si:}\square}^{0, \text{bcc-B2}} = 189$$

$$T_{\text{c, Fe, Si:Fe:}\square}^{1, \text{bcc-B2}} = T_{\text{c, Fe: Fe, Si:}\square}^{1, \text{bcc-B2}} = 63$$

$$T_{\text{c, Fe, Si:Si:}\square}^{0, \text{bcc-B2}} = T_{\text{c, Si: Fe, Si:}\square}^{0, \text{bcc-B2}} = -189$$

$$T_{\text{c, Fe, Si:Si:}\square}^{1, \text{bcc-B2}} = T_{\text{c, Si: Fe, Si:}\square}^{1, \text{bcc-B2}} = 63$$

$$G_{\text{Fe, Si:}\square}^* = -1260 R \quad (R = 8.31451)$$

$$L_{\text{Fe, Si}}^0 = -27809 + 11.62 T$$

$$L_{\text{Fe, Si}}^1 = -11544$$

$$L_{\text{Fe, Si}}^2 = 3890$$

Phase bcc-B2

$$G^\circ(T) - H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) = G(\text{Fe:Fe:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 0.5 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Fe:Si:}\square) = 2.0 G_{\text{Fe, Si:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - 0.5 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Si:Fe:}\square) = 2.0 G_{\text{Fe, Si:}\square}^*$$

$$G^\circ(T) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Fe, Si:}\square}^{0, \text{bcc-A2}} = 4.0 L_{\text{Fe, Si}}^0$$

$$L_{\text{Fe, Si:}\square}^{1, \text{bcc-A2}} = 8.0 L_{\text{Fe, Si}}^1$$

$$T_{\text{c, Fe, Si:}\square}^{1, \text{bcc-A2}} = 63$$

$$L_{\text{Fe, Si:}\square}^{2, \text{bcc-A2}} = 16.0 L_{\text{Fe, Si}}^2$$

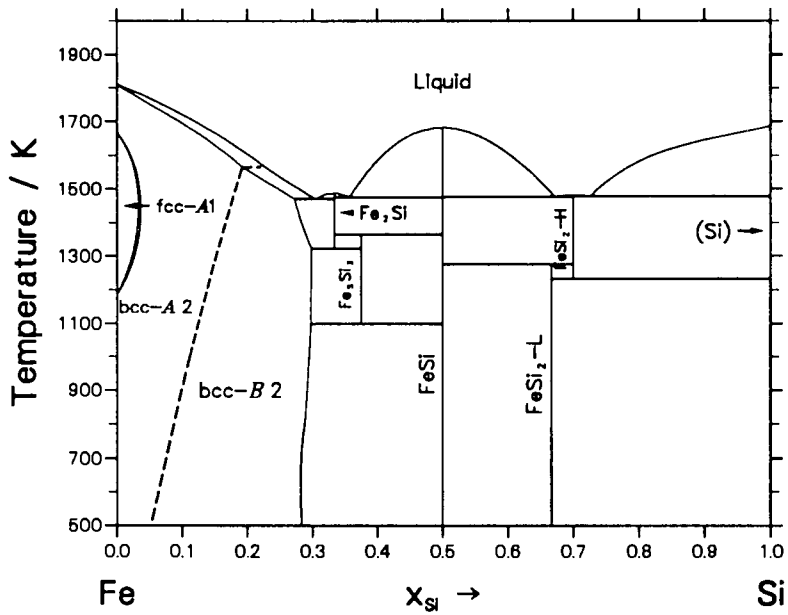


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Si}	Temp. / K
Liquid \rightleftharpoons bcc-B2 + Fe ₂ Si	Eutectic	.273 .267 .333	1470.6
Fe ₂ Si \rightleftharpoons bcc-B2 + Fe ₅ Si ₃	Eutectoid	.333 .299 .375	1322.8
Fe ₅ Si ₃ \rightleftharpoons bcc-B2 + FeSi	Eutectoid	.375 .298 .500	1097.8
Fe ₂ Si + FeSi \rightleftharpoons Fe ₅ Si ₃	Peritectoid	.333 .500 .375	1364.4
Liquid \rightleftharpoons Fe ₂ Si + FeSi	Eutectic	.357 .333 .500	1475.8
Liquid \rightleftharpoons FeSi + FeSi ₂ -H	Eutectic	.672 .500 .700	1477.2
FeSi + FeSi ₂ -H \rightleftharpoons FeSi ₂ -L	Peritectoid	.500 .700 .666	1275.7
FeSi ₂ -H \rightleftharpoons FeSi ₂ -L + (Si)	Eutectoid	.700 .667 1.000	1232.9
Liquid \rightleftharpoons FeSi ₂ -H + (Si)	Eutectic	.725 .700 1.000	1478.3
Fe ₂ Si \rightleftharpoons Liquid	Congruent	.333 .333	1488.0
FeSi \rightleftharpoons Liquid	Congruent	.500 .500	1683.0
FeSi ₂ -H \rightleftharpoons Liquid	Congruent	.700 .700	1482.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Fe-Si	(Fe)	Cu	<i>cF4</i> <i>Pm$\bar{3}m$</i>		
	(Fe)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>		
	(Si)	diamond	<i>cF8</i> <i>Fd$\bar{3}m$</i>		
	FeSi ₂ -L		<i>tP3</i> <i>P4/mmm</i>	Fe 1 Si 2	
	FeSi ₂ -H		<i>oC48</i> <i>Cmca</i>	Fe ₁ 8 Fe ₂ 8 Si ₁ 8 Si ₂ 16	
	Fe ₂ Si		<i>hP6</i> <i>P$\bar{3}m1$</i>	Fe ₁ 1 Fe ₂ 1 Fe ₃ 2 Si 2	
	FeSi		<i>cP8</i> <i>P2₁3</i>	Fe 4 Si 4	
	Fe ₅ Si ₃		<i>hP16</i> <i>P$\bar{6}_3/mmc$</i>	Fe ₁ 4 Fe ₂ 6 Si 6	
	bcc-B2	CsCl	<i>cP2</i> <i>Fm$\bar{3}m$</i>		α_2 in [90MAS]

System Fe-Ti

Solution Phases:

Liquid, bcc-A2, fcc-A1, hcp-A3

Compounds:

FeTi, Laves-C14

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Laves-C14	:	Sublattice model, (Fe,Ti) ₂ (Fe,Ti)
FeTi	:	Sublattice model, (Fe,Ti)(Fe,Ti)

Assessor and Date:

M.II. Rand 1995

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase FeTi

$$G^{\circ}(T) - H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 51584.05 + 238.686 T - 44.858 T \cdot \ln T - 0.008493 T^2 + 100500 T^{-1}$$

Phase Laves-C14

$$G^{\circ}(T) - 3.0 H_{\text{Fe}}^{\circ, \text{bcc-A3, para}}(298.15 \text{ K}) = G(\text{Fe:Fe}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Fe}}$$

$$G^{\circ}(T) - 2.0 H_{\text{Fe}}^{\circ, \text{bcc-A3, para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Fe:Ti}) = \\ - 1440.0 - 6.75 T + 2.0 \text{ GHSE}_{\text{Fe}} + \text{GHSE}_{\text{Ti}}$$

$$G^{\circ}(T) - H_{\text{Fe}}^{\circ, \text{bcc-A3, para}}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Fe}) = \\ 15000.0 + \text{GHSE}_{\text{Fe}} + 2.0 \text{ GHSE}_{\text{Ti}}$$

$$G^{\circ}(T) - 3.0 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = \\ 15000 + 3.0 \text{ GHSE}_{\text{Ti}}$$

$$I_{\text{Fe:Fe, Ti}}^{0, \text{Laves-C14}} = I_{\text{Ti:Fe, Ti}}^{0, \text{Laves-C14}} = 60000$$

$$I_{\text{Fe, Ti:Fe}}^{0, \text{Laves-C14}} = I_{\text{Fe, Ti:Ti}}^{0, \text{Laves-C14}} = 60000$$

Phase liquid

$$L_{\text{Fe,Ti}}^{0,\text{liquid}} = -62273.8 + 5.6939 T$$

$$L_{\text{Fe,Ti}}^{1,\text{liquid}} = -5491.468$$

Phase fcc-A1

$$L_{\text{Fe,Ti};\square}^{0,\text{fcc-A1}} = -42000$$

Phase hcp-A3

$$L_{\text{Fe,Ti};\square}^{0,\text{hcp-A3}} = 18500 - 15 T$$

Phase bcc-A2

$$L_{\text{Fe,Ti};\square}^{0,\text{bcc-A2}} = -52400.65 + 10.7268 T$$

$$L_{\text{Fe,Ti};\square}^{1,\text{bcc-A2}} = -7442 + 0.41968 T$$

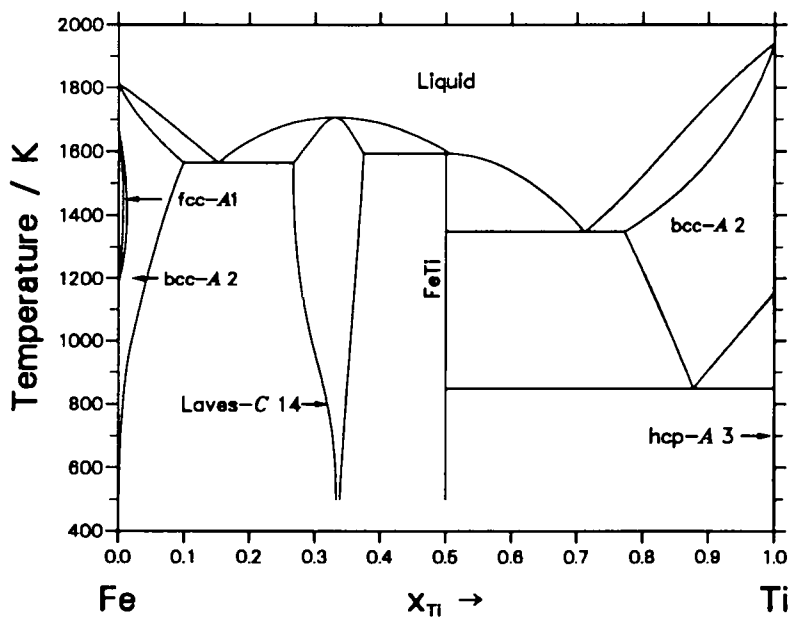


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Ti}			T / K
Liquid \rightleftharpoons FeTi* + bcc-A2	Eutectic	.712	.500	.772	1349.3
bcc-A2 \rightleftharpoons FeTi* + hcp-A3	Eutectoid	.877	.500	.999	849.4
Liquid + Laves-C14 \rightleftharpoons FeTi*	Peritectic	.506	.334	.500	1593.4
Laves-C14 \rightleftharpoons bcc-A2	Congruent	.333	.333	...	1707.0
Liquid \rightleftharpoons bcc-A2 + Laves-C14	Eutectic	.152	.099	0.267	1564.4

* FeTi \equiv bcc-B2

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Fe-Ti	(Fe)	Cu	$cF4$ $Pm\bar{3}m$	
	(Fe)	W	$cI2$ $Im\bar{3}m$	
	(Ti)	Mg	$hP2$ $P6_3/mmc$	
	(Ti)	W	$cI2$ $Im\bar{3}m$	
	FeTi	CsCl	$cP2$ $Pm\bar{3}m$	bcc-B2
	β Fe ₂ Ti	MgZn ₂	$hP12$ $P6_3/mmc$	Laves-C14

System Hf–Ti

Solution Phases:

(stable) Liquid, bcc-A2, hcp-A3
 (metastable) fcc-A1

Modelling:

Liquid : Substitutional, Redlich–Kister
 bcc-A2 : Substitutional, Redlich–Kister
 fcc-A1 : Substitutional, Redlich–Kister
 hcp-A3 : Substitutional, Redlich–Kister

Assessor and Date:

H. Bitterman, Univ. Wien, Austria, 1997

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase liquid

$$L_{\text{Hf,Ti}}^{0,\text{liquid}} = -4993.5 - 7.10316 T$$

Phase fcc-A1

$$L_{\text{Hf,Ti};\square}^{0,\text{fcc-A1}} = 1.0\text{E-4}$$

Phase hcp-A3

$$L_{\text{Hf,Ti};\square}^{0,\text{hcp-A3}} = 13644 - 10.6383 T$$

Phase bcc-A2

$$L_{\text{Hf,Ti};\square}^{0,\text{bcc-A2}} = 3003.24 - 7.4114 T$$

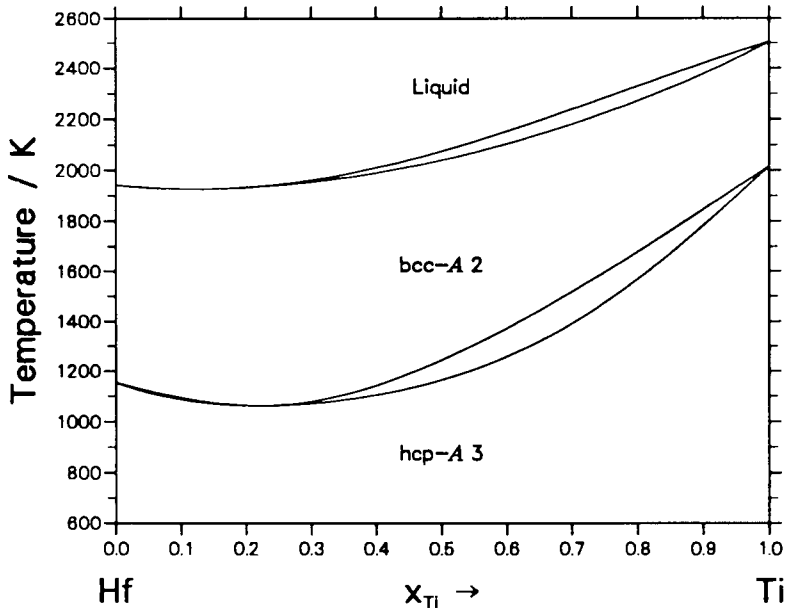


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Ti}	T / K
hcp-A3 \rightleftharpoons bcc-A2	Congruent	.224 .224	1063.3
bcc-A2 \rightleftharpoons Liquid	Congruent	.120 .120	1296.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Hf-Ti	(Hf)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	
	(Hf)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	

System Li–Mg

Solution Phases:

(stable) Liquid, bcc-A2, hcp-A3
 (metastable) fcc-A1

Compounds:

(metastable) Al₁₂Mg₁₇, AlLi

Modelling:

Liquid : Substitutional, Redlich–Kister
 bcc-A2 : Substitutional, Redlich–Kister
 fcc-A1 : Substitutional, Redlich–Kister
 hcp-A3 : Substitutional, Redlich–Kister
 Al₁₂Mg₁₇ : Sublattice model, (Li,Mg)₂₄(Li,Mg)₁₀(Mg)₂₄
 AlLi : Sublattice model, (Li,Mg)(Li,Mg,□)

Assessor and Date:

N. Saunders, 1991

Comments:

The models describing the metastable phases are compatible with the ones used in the Al–Mg system (Version I).

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Li,Mg};\square}^{0,\text{bcc-A2}} = -18335 + 8.49 T$$

$$L_{\text{Li,Mg};\square}^{1,\text{bcc-A2}} = 3481$$

$$L_{\text{Li,Mg};\square}^{2,\text{bcc-A2}} = 2658 - 0.114 T$$

Phase fcc-A1

$$L_{\text{Li,Mg};\square}^{0,\text{fcc-A1}} = -6856.0$$

Phase hcp-A3

$$L_{\text{Li,Mg};\square}^{0,\text{hcp-A3}} = -6856.0$$

$$L_{\text{Li,Mg};\square}^{1,\text{hcp-A3}} = 4000.0$$

$$L_{\text{Li,Mg};\square}^{2,\text{hcp-A3}} = 4000.0$$

Phase liquid

$$L_{\text{Li,Mg}}^{0,\text{liquid}} = -14935 + 10.371 T$$

$$L_{\text{Li,Mg}}^{1,\text{liquid}} = -1789 + 1.143 T$$

$$L_{\text{Li,Mg}}^{2,\text{liquid}} = 6533 - 6.6915 T$$

Phase Al₁₂Mg₁₇

$$G^\circ(T) - 34.0 H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 24.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Li:Li:Mg}) = 290000 + 34.0 \text{ GHSER}_{\text{Li}} + 24.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 10.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 48.0 H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Li:Li:Mg}) = 290000 + 10.0 \text{ GHSER}_{\text{Li}} + 48.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 24.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 34.0 H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Li:Li:Mg}) = 290000 + 24.0 \text{ GHSER}_{\text{Li}} + 34.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 58.0 H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mg:Mg:Mg}) = 0.0$$

Phase AlLi

$$G^\circ(T) - 2.0 H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Li:Li}) = 2.0 \text{ GHSER}_{\text{Li}}$$

$$G^\circ(T) - H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Li:Mg}) = -9168 + 4.2 T + \text{GHSER}_{\text{Li}} + \text{GBCC}_{\text{Mg}}$$

$$G^\circ(T) - H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Li}) = -9168 + 4.2 T + \text{GHSER}_{\text{Li}} + \text{GBCC}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 0.0$$

$$G^\circ(T) - H_{\text{Li}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Li:}\square) = 50000 + \text{GHSER}_{\text{Li}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:}\square) = 0.0$$

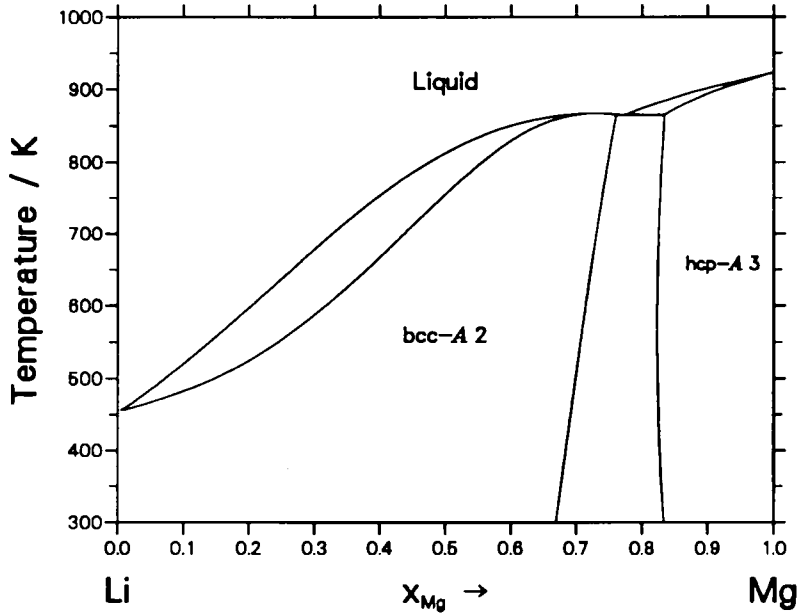


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Mg}	T / K
Liquid \rightleftharpoons bcc-A2 + hcp-A3	Eutectic	.774 .760 .834	865.2
Liquid \rightleftharpoons bcc-A2	Congruent	.727 .727	867.4

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Li-Mg	(Li)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>
	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>

System Li-Zr

Solution Phases:

(stable) Liquid, bcc-A2, hcp-A3
 (metastable) fcc-A1

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister

Assessor and Date:

N. Saunders, 1991

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$I_{Li,Zr;\square}^{0,bcc-A2} = 100000$$

Phase fcc-A1

$$I_{Li,Zr;\square}^{0,fcc-A1} = 100000$$

Phase hcp-A3

$$I_{Li,Zr;\square}^{0,hcp-A3} = 100000$$

Phase liquid

$$I_{Li,Zr}^{0,liquid} = 100000$$

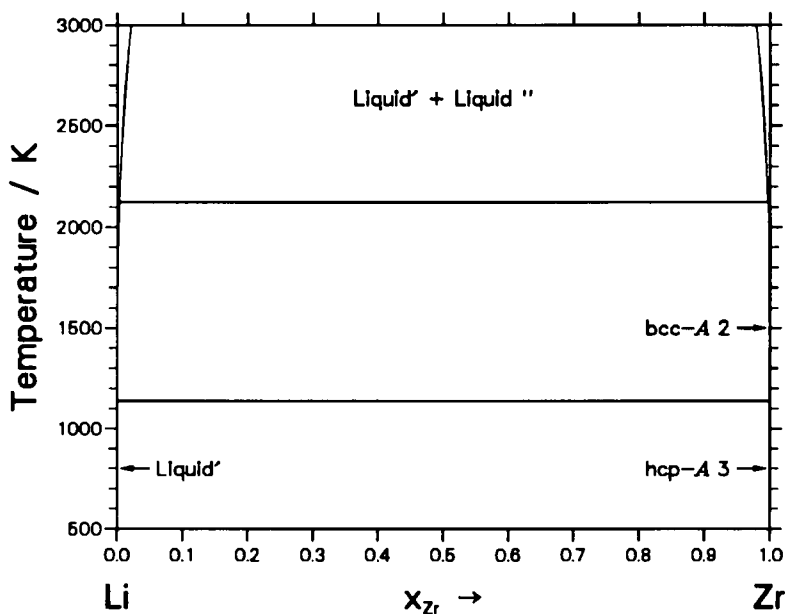


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Zr}	T / K
$hcp-A3 \rightleftharpoons bcc-A2$	Allotropic	1.000 1.000	1139.45
$Liquid'' \rightleftharpoons Liquid' + bcc-A2$	Monotectic	.996 .003 .998	2124.9
$Liquid' \rightleftharpoons bcc-A2 + hcp-A3$	Degenerate	.000 .000 1.000	453.6

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Li-Zr	(Li)	W	$cI2$ $Im\bar{3}m$
	(Zr)	Mg	$hP2$ $P6_3/mmc$
	(Zr)	W	$cI2$ $Im\bar{3}m$

System Mg-Mn

Solution Phases:

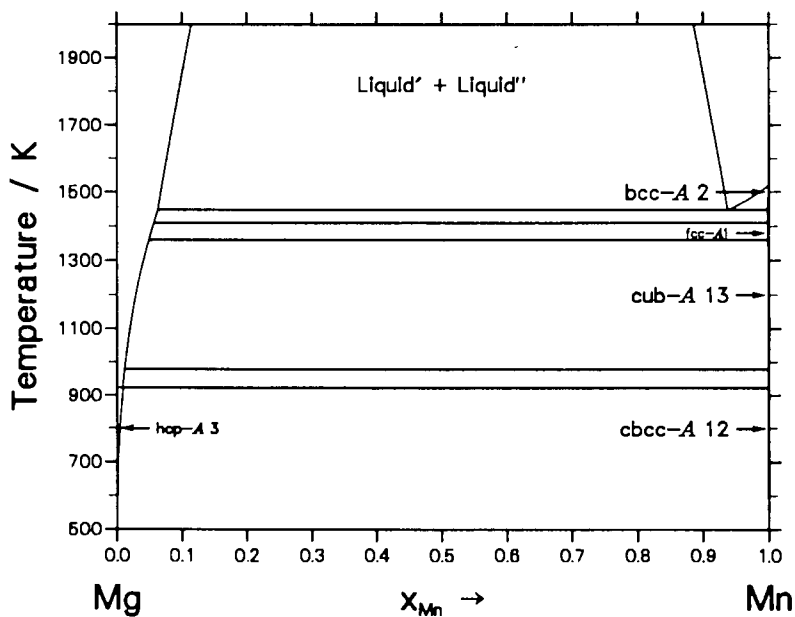
Liquid, bcc-A2, hcp-A3, cbcc-A12, cub-A13, fcc-A1

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
bcc-A12	:	Substitutional, Redlich-Kister
cub-A13	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister

Assessor and Date:

J. Tibballs 1991



Thermodynamic properties of the solution phases (J.mol⁻¹)**Phase bcc-A2**

$$L_{\text{Mg,Mn};\square}^{0,\text{bcc-A2}} = 70000.0$$

Phase cbcc-A12

$$L_{\text{Mg,Mn};\text{Va}}^{0,\text{cbcc-A12}} = 70000.0$$

Phase cub-A13

$$L_{\text{Mg,Mn};\text{Va}}^{0,\text{cub-A13}} = 70000.0$$

Phase fcc-A1

$$L_{\text{Mg,Mn}}^{0,\text{fcc-A1}} = 70000.0$$

Phase hcp-A3

$$L_{\text{Mg,Mn};\text{Va}}^{0,\text{hcp-A3}} = 32985.0 + 2.5 T$$

Phase liquid

$$L_{\text{Mg,Mn}}^{0,\text{liquid}} = 19125.0 + 12.5 T$$

Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Mn}			T / K
Liquid' + cbcc-A12 \rightleftharpoons hcp-A3	Peritectic	.008	1.000	.009	923.8
cub-A13 \rightleftharpoons Liquid' + cbcc-A12	Metatectic	.999	.012	1.000	980.5
fcc-A1 \rightleftharpoons Liquid' + cub-A13	Metatectic	.999	.048	1.000	1351.7
bcc-A2 \rightleftharpoons Liquid' + fcc-A1	Metatectic	.998	.057	.999	1409.6
Liquid'' \rightleftharpoons Liquid' + bcc-A2	Monotectic	.937	.063	.998	1447.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Mg-Mn	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	
	α -Mn	α -Mn	<i>c58</i> <i>I$\bar{4}3m$</i>	cbcc-A12
	β -Mn	β -Mn	<i>cP20</i> <i>P4₁323m</i>	cub-A13
	γ -Mn	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	
	δ -Mn	W	<i>cI2</i> <i>I$\bar{m}\bar{3}m$</i>	

System Mg–Ni

Solution Phases:

Liquid, fcc-A1

Compounds:

Mg₂Ni, Laves-C36

Modelling:

Liquid : Substitutional, Redlich–Kister
 fcc-A1 : Substitutional, Redlich–Kister
 Mg₂Ni : Stoichiometric, (Mg)₂(Ni)
 Laves-C36 : Sublattice model, (Mg,Ni)₂(Mg,Ni)

Comments:

M. Jacobs assumed the Laves-C36 phase to be stoichiometric. The thermodynamic description of that phase was modified and is now consistent with the one in the database.

Assessor and Date:

M. Jacobs September 1991 (Laves-C36 modified by I. Ansara December 1997).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Mg,Ni};\text{O}}^{0,\text{bcc-A2}} = 80 T$$

Phase fcc-A1

$$L_{\text{Mg,Ni};\text{O}}^{0,\text{fcc-A1}} = 80 T$$

Phase hcp-A3

$$L_{\text{Mg,Ni};\text{O}}^{0,\text{hcp-A3}} = 80 T$$

Phase liquid

$$L_{\text{Mg,Ni}}^{0,\text{liquid}} = -42304.49 + 7.45704 T$$

$$L_{\text{Mg,Ni}}^{1,\text{liquid}} = -15611.66 + 9.11885 T$$

Phase Laves-C36

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Mg}) =$$

$$15000.0 + \text{GHSE}_{\text{Mg}} \\ G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 2.0 H_{\text{Ni}}^{\circ,\text{fcc-A1,para}}(298.15 \text{ K}) = \\ -74136.0 + 293.9216 T - 54.35385 T \cdot \ln T - 0.03329235 T^2 \\ + 5.14203\text{E-}06 T^3 - 99.0 T^{-1}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - H_{\text{Ni}}^{\circ,\text{fcc-A1,para}}(298.15 \text{ K}) = \\ 104136.0 - 293.9216 T + 54.35385 T \cdot \ln T + 0.03329235 T^2 \\ - 5.14203\text{E-}06 T^3 + 99.0 T^{-1}$$

$$G^\circ(T) - 3.0 H_{\text{Ni}}^{\circ,\text{fcc-A1,para}}(298.15 \text{ K}) = G(\text{Ni:Ni}) =$$

$$15000.0 + \text{GHSE}_{\text{Ni}} \\ L_{\text{Mg,Ni:Mg}}^{0,\text{Laves-C36}} = L_{\text{Mg,Ni:Ni}}^{0,\text{Laves-C36}} = 50000$$

$$L_{\text{Mg:Mg,Ni}}^{0,\text{Laves-C36}} = L_{\text{Ni:Mg,Ni}}^{0,\text{Laves-C36A}} = 50000$$

Phase Mg₂Ni

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - H_{\text{Ni}}^{\circ,\text{fcc-A1,para}}(298.15 \text{ K}) = \\ -82211.0 + 571.0183 T - 95.992 T \cdot \ln T$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Ni}	T / K
Liquid \rightleftharpoons Laves-C36 + fcc-A1	Eutectic	.802 .666 1.000	1366.6
Liquid \rightleftharpoons MgNi ₂	Congruent	.666 .666	1420.0
Liquid + Mg ₂ Ni \rightleftharpoons Laves-C36	Peritectic	.278 .666 .333	1032.2
Liquid \rightleftharpoons + hcp-A3 Mg ₂ Ni	Eutectic	.101 .000 .333	780.0

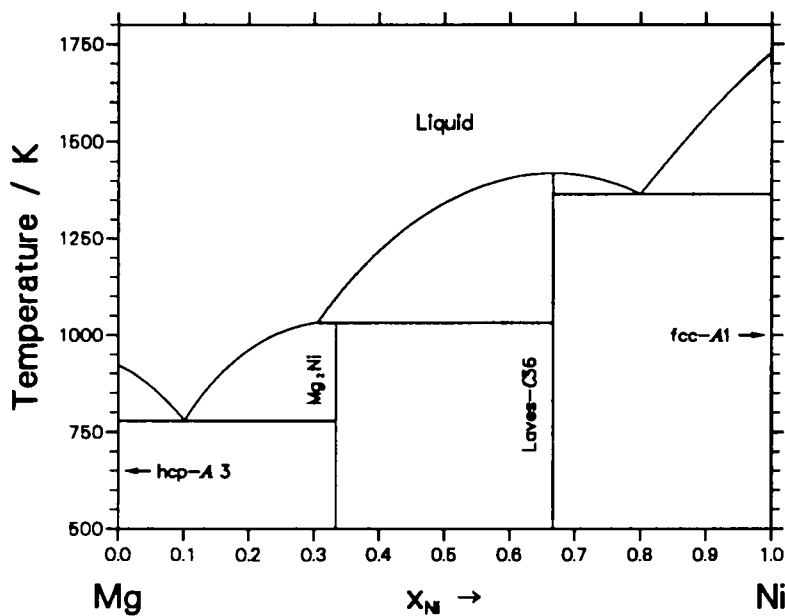


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Mg-Ni	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Ni)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	MgNi ₂	MgNi ₂	<i>hP24</i> <i>P6₃/mmc</i>	Mg ₁ 4 Mg ₂ 4 Ni ₁ 4 Ni ₂ 6 Ni ₃ 6	
	Mg ₂ Ni	Mg ₂ Ni	<i>hP18</i> <i>P6₂22</i>	Mg ₁ 6 Mg ₂ 6 Ni ₁ 3 Ni ₂ 3	in Mas2, Mg ₂ Ni related to Al ₂ Cu-C16 type according to [90Mas]

System Mg-Si

Solution Phases:

(stable) Liquid, hcp-A3
 (metastable) fcc-A1

Compound:

(stable) Mg₂Si
 (metastable) Laves-C15

Modelling:

Liquid : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 Mg₂Si : Stoichiometric, (Mg)₂(Si)
 Laves-C15 : Sublattice model, (Mg,Si)₂(Mg,Si)

Publication:

H. Heufel, T. Gödecke, H.-L. Lukas, and F. Sommer,
 J. Alloys and Comp., **247**, (1-2), 31-42 (1997).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase liquid

$$L_{\text{Mg,Si}}^{0,\text{liquid}} = -83864.26 + 32.44438 T$$

$$L_{\text{Mg,Si}}^{1,\text{liquid}} = 18027.41 - 19.61202 T$$

$$L_{\text{Mg,Si}}^{2,\text{liquid}} = 2486.67 - 0.31084 T$$

$$L_{\text{Mg,Si}}^{3,\text{liquid}} = 18541.17 - 2.317664 T$$

$$L_{\text{Mg,Si}}^{4,\text{liquid}} = -12338.84 + 1.54236 T$$

Phase hcp-A3

$$L_{\text{Mg,Si};\square}^{0,\text{hcp-A3}} = -7148.79 + 0.89361 T$$

Phase fcc-A1

$$I_{\text{Mg,Si};\square}^{0,\text{fcc-A1}} = -7148.79 + 0.89361 T$$

Phase Mg₂Si

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ -92250.0 + 440.4 T - 75.9 T \cdot \ln T - 0.0018 T^2 + 630000 T^{-1}$$

Phase Laves-C15

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Mg:Si}) = \\ 104970.96 - 16.46448 T + 2.0 \text{ GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Mg}) = \\ 41039.0 + 6.25 T + \text{GHSER}_{\text{Mg}} + 2.0 \text{ GHSER}_{\text{Si}}$$

$$I_{\text{Mg,Si};\text{Mg}}^{0,\text{LavesC15}} = 15000.0$$

$$=$$

$$I_{\text{Mg,Si};\text{Si}}^{0,\text{LavesC15}} = 15000.0$$

$$=$$

$$I_{\text{Mg};\text{Mg,Si}}^{0,\text{LavesC15}} = 8000.0$$

$$=$$

$$I_{\text{Si};\text{Mg,Si}}^{0,\text{LavesC15}} = 8000.0$$

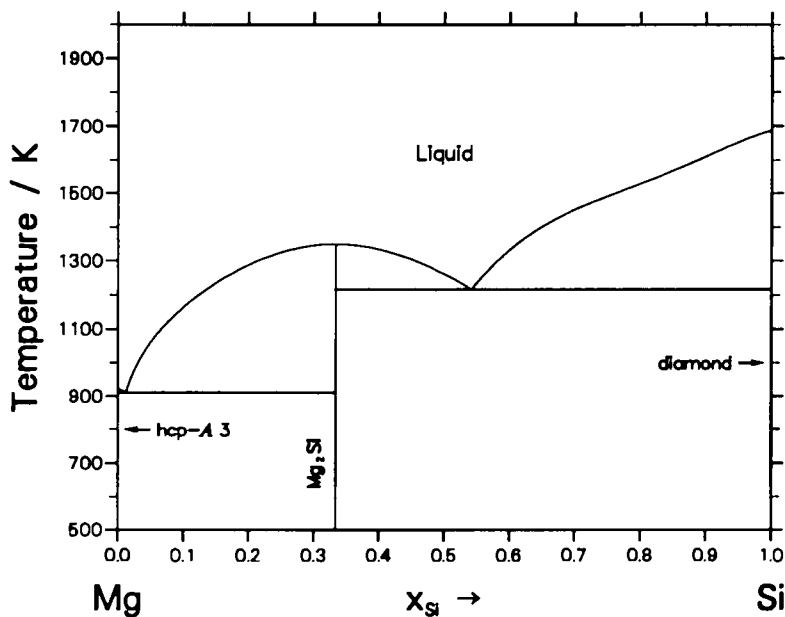


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Si}	T / K
Liquid \rightleftharpoons hcp-A3 + Mg ₂ Si	Eutectic	.013 .000 .333	911.8
Liquid \rightleftharpoons Mg ₂ Si + diamond	Eutectic	.530 .333 1.000	1214.4
Mg ₂ Si \rightleftharpoons Liquid	Congruent	.333 .333 ...	1350.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Mg-Si	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2
	(Si)	diamond	<i>cF8</i> <i>Fd$\bar{3}m$</i>	M 8
	Mg ₂ Si	CaF ₂	<i>cF12</i> <i>Fm$\bar{3}m$</i>	Mg 8 Si 4

System Mg–Y

Solution Phases:

Liquid, bcc-A2, hcp-A3

Compounds:

MgY, Mg₂₄Y₅, Mg₂Y

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc-A2	:	Substitutional, Redlich–Kister
hcp-A3	:	Substitutional, Redlich–Kister
MgY	:	Stoichiometric, (Mg)(Y)
Mg ₂ Y	:	Stoichiometric, (Mg) ₂ (Y)
Mg ₂₄ Y ₅	:	Sublattice model, (Mg) ₂₄ (Mg,Y) ₅

Assessor and Date:

H.L. Lukas, 1991

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-A2

$$I_{\text{Mg,Y};\square}^{0,\text{bcc-A2}} = -38570.0 + 15.0 T$$

$$I_{\text{Mg,Y};\square}^{1,\text{bcc-A2}} = -8204.21$$

Phase hcp-A3

$$I_{\text{Mg,Y};\square}^{0,\text{hcp-A3}} = -16582.94 + 4.77482 T$$

$$I_{\text{Mg,Y};\square}^{1,\text{hcp-A3}} = -7077.87$$

Phase liquid

$$I_{\text{Mg,Y}}^{0,\text{liquid}} = -25802.51 + 4.30042 T$$

$$I_{\text{Mg,Y}}^{1,\text{liquid}} = -19229.76 + 3.20497 T$$

Phase fcc-A1

$$L_{\text{Mg,Y}}^{0,\text{fcc-A1}} = 0.0001$$

Phase Mg_{24}Y_5

$$G^\circ(T) - 24.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 5.0 H_{\text{Y}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Y}) = \\ - 227282.28 + 36.52985 T + 24.0 \text{ GHSER}_{\text{Mg}} + 5.0 \text{ GHSER}_{\text{Y}}$$

Phase Mg_2Y

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - H_{\text{Y}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Y}) = \\ - 39075.78 + 6.51258 T + 2.0 \text{ GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Y}}$$

Phase MgY

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - H_{\text{Y}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Y}) = \\ - 32162.76 + 8.0 T + \text{GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Y}}$$

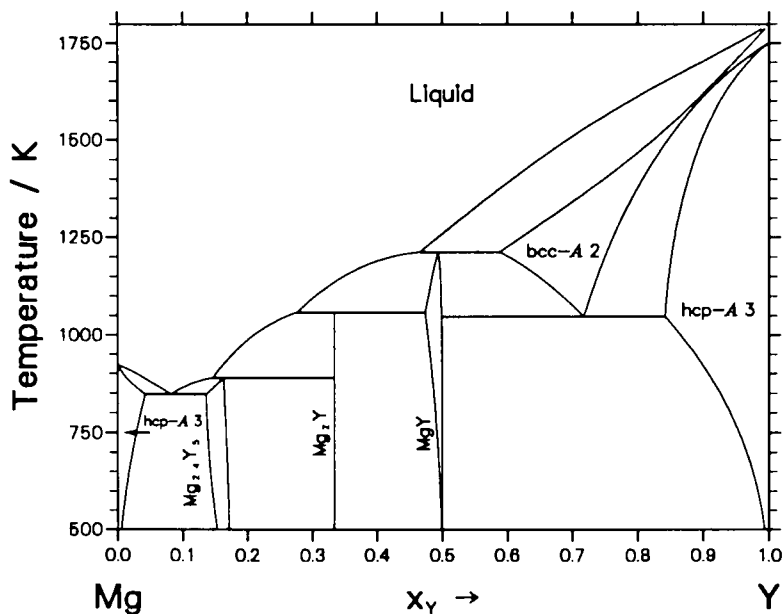


Table I - Invariant Reactions.

Reaction	Type	Compositions x_Y	T / K
Liquid + bcc-A2 \rightleftharpoons MgY	Peritectic	.466 .588 .494	1213.3
Liquid + MgY \rightleftharpoons Mg ₂ Y	Peritectic	.276 .474 .333	1058.5
Liquid + Mg ₂ Y \rightleftharpoons Mg ₂₄ Y ₅	Peritectic	.146 .333 .163	889.4
Liquid \rightleftharpoons hcp-A3 + Mg ₂₄ Y ₅	Eutectic	.082 .042 .136	847.6
bcc-A2 \rightleftharpoons MgY + hcp-A3	Eutectoid	.717 .499 .841	1048.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Mg-Y	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Y)	W	<i>cF2</i> <i>Im$\bar{3}m$</i>	M 4	
	(Y)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	Mg _{24+x} Y ₅	α -Mn	<i>cF58</i> <i>I$\bar{4}3m$</i>	M 2 Mg ₁ 24 Mg ₂ 24 Y 8	cbcc-A12 designated as Mg ₂₄ Y ₅
	Mg ₂ Y	MgZn ₂	<i>hP12</i> <i>P6₃/mmc</i>	Mg ₁ 2 Mg ₂ 6	
	Mg _{1+x} Y	CsCl	<i>cP2</i> <i>Pm$\bar{3}m$</i>	Mg 1 Y 1	bcc-B2 designated as MgY

System Mg-Zn

Solution Phases:

- (stable) : Liquid, hcp-Zn, Laves-C14
 (metastable) : bcc-A2, bcc-B2, fcc-A1, hcp-A3

Compounds:

- (stable) Mg₂Zn₁₁, MgZn, Mg₂Zn₃, Mg₅₁Zn₂₀
 (metastable) : AlMg-β, AlMg-ε, AlMg-γ, AlMgZn-φ
 (metastable) : Laves-C15, Laves-C36

Modelling:

- Liquid : Substitutional, Redlich-Kister
 hcp-Zn : Substitutional, Redlich-Kister
 bcc-A2 : see below
 bcc-B2 : Sublattice model, (Mg,Zn)_{0.5}(Mg,Zn)_{0.5}(□)₃
 Two descriptions of the bcc-A2:bcc-B2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 Mg₂Zn₁₁ : Stoichiometric, (Mg)₂(Zn)₁₁
 MgZn : Stoichiometric, (Mg)₁₂(Zn)₁₃
 Mg₂Zn₃ : Stoichiometric, (Mg)₂(Zn)₃
 Mg₅₁Zn₂₀ : Stoichiometric, (Mg)₅₁(Zn)₂₀
 AlMgZn-φ : Stoichiometric, (Mg)₆(Zn)₅
 AlMg-β : Stoichiometric, (Mg)₈₉(Zn)₁₀₄
 AlMg-ε : Stoichiometric, (Mg)₂₃(Zn)₃₀
 AlMg-γ : Sublattice model, (Mg)₅(Mg,Zn)₁₂(Mg,Zn)₁₂
 Laves-C14 : Sublattice model, (Mg,Zn)₂(Mg,Zn)
 Laves-C15 : Sublattice model, (Mg,Zn)₂(Mg,Zn)
 Laves-C36 : Sublattice model, (Mg,Zn)₂(Mg,Zn)

Assessor and Date:

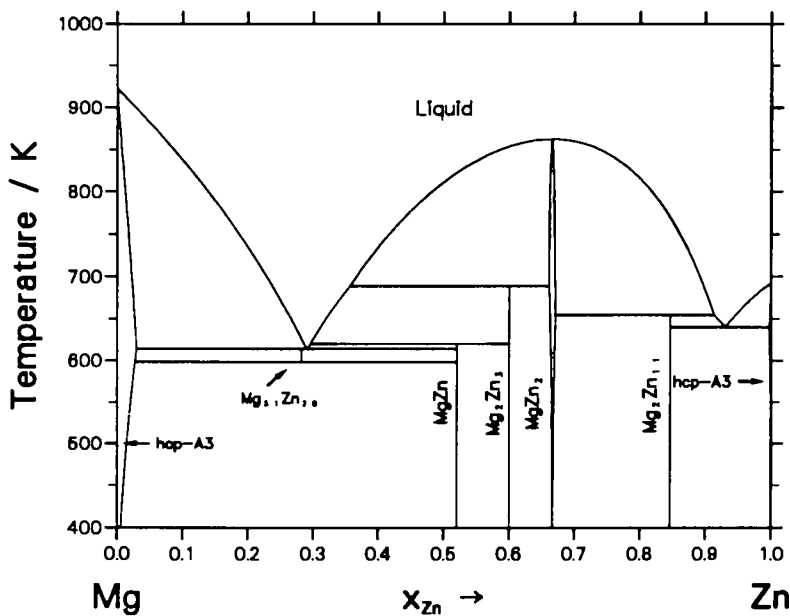
R. Agarwal, S.G. Fries, H.L. Lukas, G. Petzow,
F. Sommer, T.G. Chart, G. Effenberg

Publication:

Z. für Metallkde., 83, 4, 216–223 (1992).

Comments:

A reevaluation was performed in order to take into account the non-stoichiometry of the Laves-C14 phase.



Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase fcc-A1

$$L_{\text{Mg,Zn};\square}^{0,\text{fcc-A1}} = -3056.82 + 5.63801 T$$

$$L_{\text{Mg,Zn};\square}^{1,\text{fcc-A1}} = -3127.26 + 5.65563 T$$

Phase hcp-Zn

$$L_{\text{Mg,Zn};\square}^{0,\text{hcp-Zn}} = -3056.82 + 5.63801 T$$

$$L_{\text{Mg,Zn};\square}^{1,\text{hcp-Zn}} = -3127.26 + 5.65563 T$$

Phase hcp-A3

$$L_{\text{Mg,Zn};\square}^{0,\text{hcp-A3}} = -3056.82 + 5.63801 T$$

$$L_{\text{Mg,Zn};\square}^{1,\text{hcp-A3}} = -3127.26 + 5.65563 T$$

Phase liquid

$$L_{\text{Mg,Zn}}^{0,\text{liquid}} = -77729.24 + 680.52266 T - 95.0 T \cdot \ln T + 0.04 T^2$$

$$L_{\text{Mg,Zn}}^{1,\text{liquid}} = 3674.72 + 0.57139 T$$

$$L_{\text{Mg,Zn}}^{2,\text{liquid}} = -1588.15$$

Phase AlMg- β

$$G^\circ(T) - 89.0 H_{\text{Mg}}^{0,\text{hcp-A3}}(298.15 \text{ K}) - 104.0 H_{\text{Zn}}^{0,\text{hcp-Zn}}(298.15 \text{ K}) = \\ 206100 + 89.0 \text{ GHSER}_{\text{Mg}} + 104.0 \text{ GHSER}_{\text{Zn}}$$

Phase AlMg- ϵ

$$G^\circ(T) - 23.0 H_{\text{Mg}}^{0,\text{hcp-A3}}(298.15 \text{ K}) - 30.0 H_{\text{Zn}}^{0,\text{hcp-Zn}}(298.15 \text{ K}) = \\ -318000 + 63.6 T + 23.0 \text{ GHSER}_{\text{Mg}} + 30.0 \text{ GHSER}_{\text{Zn}}$$

Phase AlMg- γ

$$G^\circ(T) - 17.0 H_{\text{Mg}}^{0,\text{hcp-A3}}(298.15 \text{ K}) - 12.0 H_{\text{Zn}}^{0,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Mg:Zn}) = \\ -145000 + 58 T + 17.0 \text{ GHSER}_{\text{Mg}} + 12.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 17.0 H_{\text{Mg}}^{0,\text{hcp-A3}}(298.15 \text{ K}) - 12.0 H_{\text{Zn}}^{0,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Zn:Mg}) = \\ 87000 + 29 T + 17.0 \text{ GHSER}_{\text{Mg}} + 12.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 5.0 H_{\text{Mg}}^{0,\text{hcp-A3}}(298.15 \text{ K}) - 24.0 H_{\text{Zn}}^{0,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Zn:Zn}) = \\ 290000.0 + 5.0 \text{ GHSER}_{\text{Mg}} + 24.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Mg:Mg,Zn:Mg}}^{0,\text{AlMg-}\gamma} = L_{\text{Mg:Mg,Zn:Zn}}^{0,\text{AlMg-}\gamma} = -116000 + 58 T$$

Phase Mg₅₁Zn₂₀

$$G^\circ(T) - 51.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) - 20.0 H_{\text{Zn}}^{\circ, \text{hcp}-Zn}(298.15 \text{ K}) = \\ - 335741.54 + 35.5 T + 51.0 \text{ GHSE}_{\text{Mg}} + 20.0 \text{ GHSE}_{\text{Zn}}$$

Phase MgZn

$$G^\circ(T) - 12.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) - 13.0 H_{\text{Zn}}^{\circ, \text{hcp}-Zn}(298.15 \text{ K}) = \\ - 236980.84 + 59.24524 T + 12.0 \text{ GHSE}_{\text{Mg}} + 13.0 \text{ GHSE}_{\text{Zn}}$$

Phase Mg₂Zn₃

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) - 3.0 H_{\text{Zn}}^{\circ, \text{hcp}-Zn}(298.15 \text{ K}) = \\ - 54406.20 + 13.60156 T + 2.0 \text{ GHSE}_{\text{Mg}} + 3.0 \text{ GHSE}_{\text{Zn}}$$

Phase Mg₂Zn₁₁

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) - 11.0 H_{\text{Zn}}^{\circ, \text{hcp}-Zn}(298.15 \text{ K}) = \\ - 73818.32 + 18.45457 T + 2.0 \text{ GHSE}_{\text{Mg}} + 11.0 \text{ GHSE}_{\text{Zn}}$$

Phase AlMgZn- ϕ

$$G^\circ(T) - 6.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) - 5.0 H_{\text{Zn}}^{\circ, \text{hcp}-Zn}(298.15 \text{ K}) = \\ - 79530 + 20.9 T + 6.0 \text{ GHSE}_{\text{Mg}} + 5.0 \text{ GHSE}_{\text{Zn}}$$

Phase Laves-C14

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ, \text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Mg:Zn}) = \\ 65355.45 - 8.83886 T + 2.0 \text{ GHSE}_{\text{Mg}} + \text{GHSE}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ, \text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Mg}) = \\ - 35355.45 + 8.83886 T + \text{GHSE}_{\text{Mg}} + 2.0 \text{ GHSE}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ, \text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Zn}) = 15000.0 + 3.0 \text{ GHSE}_{\text{Zn}}$$

$$L_{\text{Mg,Zn:Mg}}^{0, \text{Laves-C14}} = L_{\text{Mg,Zn:Zn}}^{0, \text{Laves-C14}} = 35000.0$$

$$L_{\text{Mg:Mg,Zn}}^{0, \text{Laves-C14}} = L_{\text{Zn:Mg,Zn}}^{0, \text{Laves-C14}} = 8000.0$$

Phase Laves-C15

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Mg}:\text{Mg}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Mg}:\text{Zn}) = \\ 55355.45 - 8.83886 T + 2.0 \text{ GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Mg}) = \\ -25355.45 + 8.83886 T + \text{GHSER}_{\text{Mg}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Mg},\text{Zn}:\text{Mg}}^{0,\text{Laves}-\text{C}15} = L_{\text{Mg},\text{Zn}:\text{Zn}}^{0,\text{Laves}-\text{C}15} = 35000.0$$

$$L_{\text{Mg}:\text{Mg},\text{Zn}}^{0,\text{Laves}-\text{C}15} = L_{\text{Zn}:\text{Mg},\text{Zn}}^{0,\text{Laves}-\text{C}15} = 8000.0$$

Phase Laves-C36

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Mg}:\text{Mg}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Mg}:\text{Zn}) = \\ 65355.45 - 8.83886 T + 2.0 \text{ GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Mg}) = \\ -35355.45 + 8.83886 T + \text{GHSER}_{\text{Mg}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Mg},\text{Zn}:\text{Mg}}^{0,\text{Laves}-\text{C}36} = L_{\text{Mg},\text{Zn}:\text{Zn}}^{0,\text{Laves}-\text{C}36} = 35000.0$$

$$L_{\text{Mg}:\text{Mg},\text{Zn}}^{0,\text{Laves}-\text{C}36} = L_{\text{Zn}:\text{Mg},\text{Zn}}^{0,\text{Laves}-\text{C}36} = 8000.0$$

Phase bcc-B2

$$G_{\text{Mg}:\text{Zn}:\square}^* = 0.0$$

$$L_{\text{Mg},\text{Zn}}^0 = -2500.0$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Mg}:\text{Mg}:\square) = \text{GBCC}_{\text{Mg}}$$

$$G^\circ(T) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Mg}:\text{Zn}:\square) = \\ G_{\text{Mg}:\text{Zn}:\square}^* + L_{\text{Mg},\text{Zn}}^0 + 0.5 \text{ GBCC}_{\text{Mg}} + 0.5 \text{ GBCC}_{\text{Zn}}$$

$$G^\circ(T) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Mg}:\square) = \\ G_{\text{Mg}:\text{Zn}:\square}^* + L_{\text{Mg},\text{Zn}}^0 + 0.5 \text{ GBCC}_{\text{Mg}} + 0.5 \text{ GBCC}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Zn}:\square) = \text{GBCC}_{\text{Zn}}$$

$$L_{\text{Mg},\text{Zn}:\text{Mg}:\square}^{0,\text{bcc}-\text{B}2} = L_{\text{Mg}:\text{Mg},\text{Zn}:\square}^{0,\text{bcc}-\text{B}2} = -G_{\text{Mg}:\text{Zn}:\square}^* + L_{\text{Mg},\text{Zn}}^0$$

$$L_{\text{Mg},\text{Zn}:\text{Zn}:\square}^{0,\text{bcc}-\text{B}2} = L_{\text{Zn}:\text{Mg},\text{Zn}:\square}^{0,\text{bcc}-\text{B}2} = -G_{\text{Mg}:\text{Zn}:\square}^* + L_{\text{Mg},\text{Zn}}^0$$

Phase bcc-B2

$$G_{\text{Mg:Zn}:\square}^* = 0.0$$

$$L_{\text{Mg,Zn}}^0 = -2500.0$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Mg}:\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Zn}:\square) = 2.0 G_{\text{Mg:Zn}:\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Zn:Mg}:\square) = 2.0 G_{\text{Mg:Zn}:\square}^*$$

$$G^\circ(T) - H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn}:\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Mg,Zn}:\square}^{0,\text{bcc-A2}} = 4.0 L_{\text{Mg,Zn}}^0$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zn}			T / K
Liquid + hcp-A3 \rightleftharpoons Mg ₅₁ Zn ₂₀	Peritectic	.295	.029	.289	614.1
Liquid \rightleftharpoons Mg ₅₁ Zn ₂₀ + MgZn	Eutectic	.281	.290	.520	614.1
Liquid + Mg ₂ Zn ₃ \rightleftharpoons MgZn	Peritectic	.196	.600	.520	620.1
Liquid + Laves-C14 \rightleftharpoons Mg ₂ Zn ₃	Peritectic	.356	.661	.600	688.9
Liquid \rightleftharpoons MgZn ₂	Congruent	.667	.667	864.0
Liquid + Laves-C14 \rightleftharpoons Mg ₂ Zn ₁₁	Peritectic	.913	.661	.846	654.4
Liquid \rightleftharpoons Mg ₂ Zn ₁₁ \rightleftharpoons hcp-A3	Eutectic	.926	.846	.997	637.3
Mg ₅₁ Zn ₂₀ \rightleftharpoons hcp-A3 + MgZn	Eutectoid	.282	.027	.520	598.1

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- Model	Comments
Mg-Zn	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Zn)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	MgZn ₂	MgZn ₂	<i>hP12</i> <i>P6₃/mmc</i>	Mg 4 Zn ₁ 2 Zn ₃ 6	Laves-C14
	Mg ₂ Zn ₁₁	Mg ₂ Zn ₁₁	<i>cP39</i> <i>Pm3</i>		
	MgZn				
	Mg ₂ Zn ₃		<i>mC110</i> <i>B2/m</i>		
	Mg ₇ Zn ₃	Ta ₃ B ₄	<i>oI142</i> <i>Immm</i>		designated as Mg ₅₁ Zn ₂₀

System Mg-Zr

Solution Phases:

(stable) Liquid, bcc-A2, hcp-A3
 (metastable) fcc-A1

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister

Assessor and Date:

M. Hämmäläinen 1991

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Mg,Zr},\square}^{0,\text{bcc-A2}} = 5720.44 + 50.11642 T$$

Phase fcc-A1

$$L_{\text{Mg,Zr},\square}^{0,\text{fcc-A1}} = 42063.55 + 1.01789 T$$

$$L_{\text{Mg,Zr},\square}^{1,\text{fcc-A1}} = -2885.9$$

Phase hcp-A3

$$L_{\text{Mg,Zr},\square}^{0,\text{hcp-A3}} = 42063.55 + 1.01789 T$$

$$L_{\text{Mg,Zr},\square}^{1,\text{hcp-A3}} = -2885.9$$

Phase liquid

$$L_{\text{Mg,Zr}}^{0,\text{liquid}} = 14003.84 + 29.34205 T$$

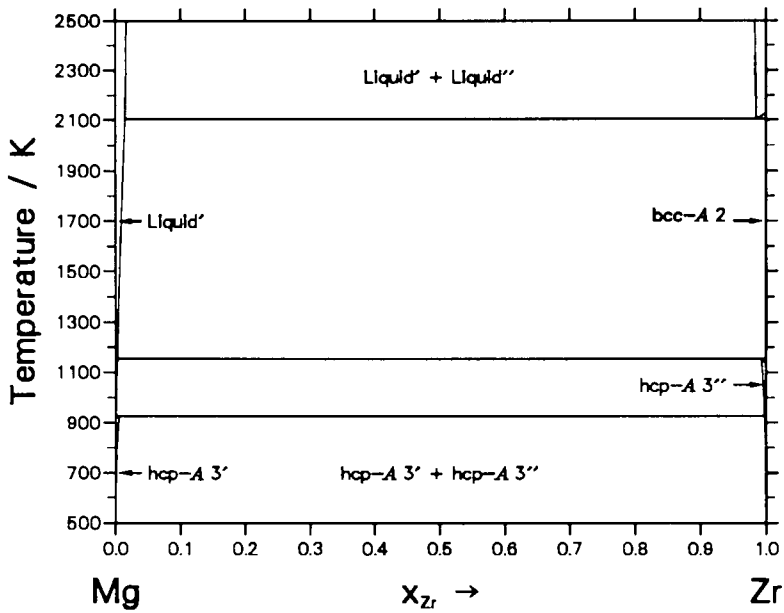


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Zr}	T / K
Liquid' + bcc-A2 \rightleftharpoons hcp-A3	Peritectic	.003 1.000 .993	1154.6
Liquid'' \rightleftharpoons Liquid' + bcc-A2	Monotectic	.985 .015 .999	2104.8
Liquid' + hcp-A3'' \rightleftharpoons hcp-A3'	Peritectic	.001 .997 .006	926.6

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Mg-Zr	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>
	(Zr)	Mg	<i>hP2</i> <i>P6₃/mmc</i>
	(Zr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>

System Mn–Si

Solution Phases:

Liquid, bcc–A2, cbcc–A12, cub–A13, fcc–A1

Compounds:

(stable)

Mn₆Si, Mn₉Si₂, Mn₃Si, Mn₅Si₃, MnSi, Mn₁₁Si₁₉

(metastable)

Al₈Mn₅–D8₁₀

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc–A2	:	Substitutional, Redlich-Kister
cbcc–A12	:	Substitutional, Redlich-Kister
cub–A13	:	Substitutional, Redlich-Kister
fcc–A1	:	Substitutional, Redlich-Kister
Mn ₆ Si	:	Stoichiometric, (Mn) ₁₇ (Si) ₃
Mn ₉ Si ₂	:	Stoichiometric, (Mn) ₃₃ (Si) ₇
Mn ₃ Si	:	Stoichiometric, (Mn) ₃ (Si)
Mn ₅ Si ₃	:	Stoichiometric, (Mn) ₅ (Si) ₃
MnSi	:	Stoichiometric, (Mn)(Si)
Mn ₁₁ Si ₁₉	:	Stoichiometric, (Mn) ₁₁ (Si) ₁₉
Al ₈ Mn ₅ –D8 ₁₀	:	Sublattice model, (Si) ₁₂ (Mn) ₄ (Mn) ₁₀

Assessor and Date:

J.E. Tibballs, 1991

Publication:

SI-report, 890221-5, 1991

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Mn₃Si

$$G^{\circ}(T) - 3.0 H_{\text{Mn}}^{\circ, \text{bcc-A12, para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 950.00 : -124189.87 + 782.4373 T - 131.682 T \cdot \ln T \\ - 0.00777 T^2 + 1657200 T^{-1}$$

$$950.00 < T < 2000.00 : -119740.6 + 777.7538 T - 131.682 T \cdot \ln T \\ - 0.00777 T^2 + 1657200 T^{-1}$$

Phase MnSi

$$G^\circ(T) - H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$- 78135.144 + 308.2488 T - 52.42121 T \cdot \ln T - 0.006903355 T^2$$

$$+ 876442.9 T^{-1}$$

Phase Mn₁₁Si₁₉

$$G^\circ(T) - 11.0 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - 19.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$- 636300.0 + 1624.93 T - 378.694 T \cdot \ln T - 0.16391 T^2$$

$$- 15432618 T^{-1}$$

Phase Mn₆Si

$$G^\circ(T) - 17.0 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 1519.00 : - 250180.6 + 84.8444 T - 12.07755 T \cdot \ln T$$

$$- 0.02850984 T^2 + 7514 T^{-1}$$

$$+ 17.0 \text{ GHSE}_{\text{Mn}} + 3.0 \text{ GHSE}_{\text{Si}}$$

$$1519.00 < T < 3000.00 : - 282008.6 - 32.58304 T + 12.06754 T \cdot \ln T$$

$$- 0.05879165 T^2 + 3.928228\text{E}+31 T^{-9}$$

$$+ 17.0 \text{ GHSE}_{\text{Mn}} + 3.0 \text{ GHSE}_{\text{Si}}$$

Phase Mn₉Si₂

$$G^\circ(T) - 33.0 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - 7.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 1519.00 : - 578208.4 + 381.294 T - 56.86988 T \cdot \ln T$$

$$- 0.0500355 T^2 + 1458600 T^{-1}$$

$$+ 33.0 \text{ GHSE}_{\text{Mn}} + 7.0 \text{ GHSE}_{\text{Si}}$$

$$298.15 < T < 1519.00 : - 639992.0 + 153.3464 T - 10.0 T \cdot \ln T$$

$$- 0.1 T^2 + 7.625384\text{E}+31 T^{-9}$$

$$+ 33.0 \text{ GHSE}_{\text{Mn}} + 7.0 \text{ GHSE}_{\text{Si}}$$

Phase Mn₅Si₃

$$G^\circ(T) - 5.0 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$- 261930.32 + 1170.778 T - 211.150 T \cdot \ln T - 0.015293 T^2$$

$$- 149263.11 T^{-1}$$

Phase Al₈Mn₅-D8₁₀

$$G^\circ(T) - 14.0 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - 12.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$+ 14.0 \text{ GHSE}_{\text{Mn}} + 12.0 \text{ GHSE}_{\text{Si}}$$

Phase bcc-A2

$$L_{\text{Mn,Si};\square}^{0,\text{bcc-A2}} = - 89620.7 + 2.94097 T$$

$$L_{\text{Mn,Si};\square}^{1,\text{bcc-A2}} = - 7500.0$$

Phase bcc-A12

$$L_{\text{Mn,Si};\square}^{0,\text{bcc-A12}} = -142743.62 + 22.3961 T$$

$$L_{\text{Mn,Si};\square}^{1,\text{bcc-A12}} = 16440.608 - 3.5300332 T$$

Phase cub-A13

$$L_{\text{Mn,Si};\square}^{0,\text{cub-A13}} = -142343.62 + 21.892610 T$$

$$L_{\text{Mn,Si};\square}^{1,\text{cub-A13}} = 16440.608 - 3.5300332 T$$

Phase fcc-A1

$$L_{\text{Mn,Si};\square}^{0,\text{fcc-A1}} = -95600 + 2.94097 T$$

$$L_{\text{Mn,Si};\square}^{1,\text{fcc-A1}} = -7500$$

Phase liquid

$$L_{\text{Mn,Si}}^{0,\text{liquid}} = -139817 + 29.86137 T$$

$$L_{\text{Mn,Si}}^{1,\text{liquid}} = -34917.2 + 3.20488 T$$

$$L_{\text{Mn,Si}}^{2,\text{liquid}} = 46782.4 - 1.8.1897 T$$

$$L_{\text{Mn,Si}}^{3,\text{liquid}} = 16168.2$$

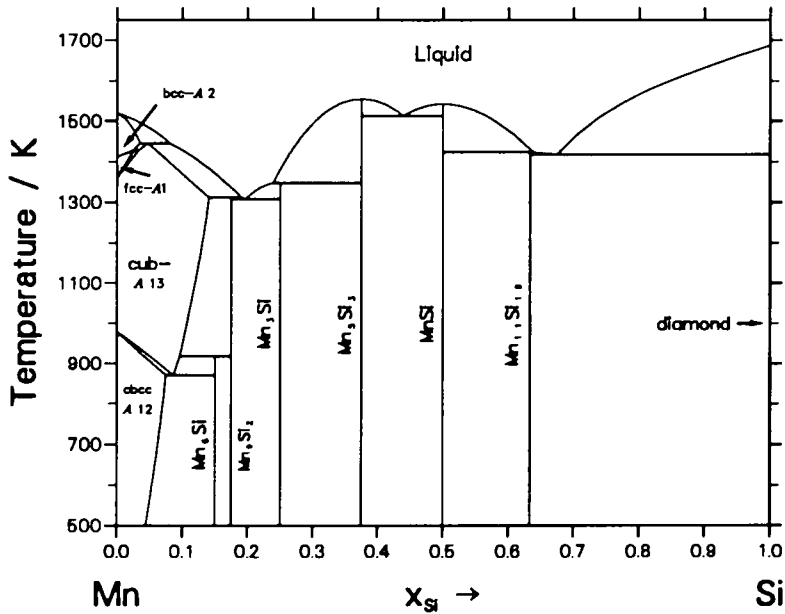


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Si}	T / K
Liquid + bcc-A2 \rightleftharpoons cub-A13	Peritectic	.080 .035 .046	1445.3
bcc-A2 + cub-A13 \rightleftharpoons fcc-A1	Peritectic	.024 .024 .033	1426.6
Liquid + cub-A13 \rightleftharpoons Mn ₉ Si ₂	Peritectic	.191 .140 .175	1312.7
Liquid \rightleftharpoons Mn ₉ Si ₂ + Mn ₃ Si	Eutectic	.197 .175 .250	1309.3
Liquid + Mn ₅ Si ₃ \rightleftharpoons Mn ₃ Si	Peritectic	.239 .375 .250	1348.0
Mn ₅ Si ₃ \rightleftharpoons Liquid	Congruent	.375 .375	1556.0
Liquid \rightleftharpoons Mn ₅ Si ₃ + MnSi	Eutectic	.439 .375 .500	1513.4
MnSi \rightleftharpoons Liquid	Congruent	.500 .500	1544.0
Liquid + MnSi \rightleftharpoons Mn ₁₁ Si ₁₉	Peritectic	.639 .500 .633	1423.4
Liquid \rightleftharpoons diamond + Mn ₁₁ Si ₁₉	Eutectic	.674 .633 1.000	1417.1
cub-A13 + Mn ₉ Si ₂ \rightleftharpoons Mn ₆ Si	Peritectoid	.096 .170 .150	918.0
cbcc-A12 \rightleftharpoons cub-A13 + Mn ₆ Si	Eutectoid	.086 .075 .150	870.6

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Mn-Si	α -Mn	α -Mn	<i>c58</i> <i>I\bar{A}3m</i>		cbcc-A12
	β -Mn	β -Mn	<i>cP20</i> <i>P₄₁323m</i>		cub-A13
	γ -Mn	Cu	<i>cF4</i> <i>Fm3m</i>		
	δ -Mn	W	<i>cI2</i> <i>Im3m</i>		
	(Si)	diamond	<i>cF8</i> <i>Fd3m</i>	M 8	
	MnSi	FeSi	<i>cP8</i> <i>P2₁3</i>	Mn 4 Si 4	
	Mn ₃ Si- α			M ₁ 4	transformation not considered
	Mn ₃ Si- β	BiF ₃	<i>cF16</i> <i>Fm3m</i>	M ₁ 4 M ₂ 4 M ₃ 8	
Mn ₅ Si ₂	Mn ₅ Si ₂	<i>tP56</i> <i>P₄₁2₁2</i>			

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
	$Mn_{11}Si_{19}$	$Mn_{11}Si_{19}$	<i>tP120</i> <i>P4̄n2</i>		$MnSi_{1.75-x}$ in [90Mas]
	$Mn_{44}Si_9$	Mo	<i>hR53</i> <i>R3̄</i>	M_1 1 M_2 2 M_3 6 M_5 6 M_6 6 Mn_1 2 Mn_2 6 Mn_3 6 Mn_4 6 Mn_5 6	approximated as Mn_6Si
	Mn_5Si_3	Mn_5Si_3	<i>hP16</i> <i>P6_3/mcm</i>	Mn_1 4 Mn_2 6 Si 6	

System Mn-Ti

Solution Phases:

Liquid, bcc-A2, fcc-A1, hcp-A3, cbcc-A12, cub-A13

Compounds:

Mn₄Ti, Mn₃Ti, MnTi- α , MnTi- β , Laves-C14

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
cbcc-A12	:	Substitutional, Redlich-Kister
cub-A13	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Laves-C14	:	Sublattice model: (Mn,Ti) ₂ (Mn,Ti)
Mn ₄ Ti	:	Stoichiometric, (Mn) _{0.815} (Ti) _{0.185}
MnTi- α	:	Stoichiometric, (Mn)(Ti)
MnTi- β	:	Stoichiometric, (Mn) _{0.515} (Ti) _{0.485}

Assessor and Date:

N. Saunders, 1993

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Mn,Ti};\square}^{0,\text{bcc-A2}} = -23200 + 20 T$$

$$L_{\text{Mn,Ti};\square}^{1,\text{bcc-A2}} = -1000$$

Phase cbcc-A12

$$L_{\text{Mn,Ti};\square}^{0,\text{cbcc-A12}} = -29500 + 20 T$$

$$L_{\text{Mn,Ti};\square}^{1,\text{cbcc-A12}} = -3635 - 5 T$$

Phase cub-A13

$$L_{\text{Mn,Ti};\square}^{0,\text{cub-A13}} = -34000 + 20 T$$

Phase fcc-A1

$$L_{\text{Mn,Ti};\square}^{0,\text{fcc-A1}} = -26200 + 20 T$$

Phase hcp-A3

$$L_{\text{Mn,Ti};\square}^{0,\text{hcp-A3}} = 22100$$

Phase liquid

$$L_{\text{Mn,Ti}}^{0,\text{liquid}} = -34000 + 21.5 T$$

$$L_{\text{Mn,Ti}}^{1,\text{liquid}} = 1400$$

Phase Mn₄Ti

$$G^\circ(T) - 0.815 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - 0.185 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = -2445.0 - 2.9 T + 0.815 \text{ GHSER}_{\text{Mn}} + 0.185 \text{ GHSER}_{\text{Ti}}$$

Phase Mn₃Ti

$$G^\circ(T) - 3.0 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = -18552.0 - 9.12 T + 3.0 \text{ GHSER}_{\text{Mn}} + \text{GHISER}_{\text{Ti}}$$

Phase MnTi- α

$$G^\circ(T) - H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = -11478.0 + \text{GHSER}_{\text{Mn}} + \text{GHSER}_{\text{Ti}}$$

Phase MnTi- β

$$G^\circ(T) - 0.515 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - 0.485 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = -5540.0 - 2.29 T + 0.515 \text{ GHSER}_{\text{Mn}} + 0.485 \text{ GHSER}_{\text{Ti}}$$

Phase Laves-C14

$$G^\circ(T) - 3.0 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) = G(\text{Mn:Mn}) = 3000.0 + 3.0 \text{ GHISER}_{\text{Mn}}$$

$$G^\circ(T) - 2.0 H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mn:Ti}) = -26400.0 + 2.0 \text{ GHSER}_{\text{Mn}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Mn}}^{\circ,\text{bcc-A12,para}}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Mn}) = 3000.0 + \text{GHISER}_{\text{Mn}} + 2.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Ti}}$$

$$L_{\text{Mn:Mn,Ti}}^{0,\text{Laves-C14}} = L_{\text{Ti:Mn,Ti}}^{0,\text{Laves-C14}} = 15000$$

$$L_{\text{Mn,Ti:Mn}}^{0,\text{Laves-C14}} = L_{\text{Mn,Ti:Ti}}^{0,\text{Laves-C14}} = 27000$$

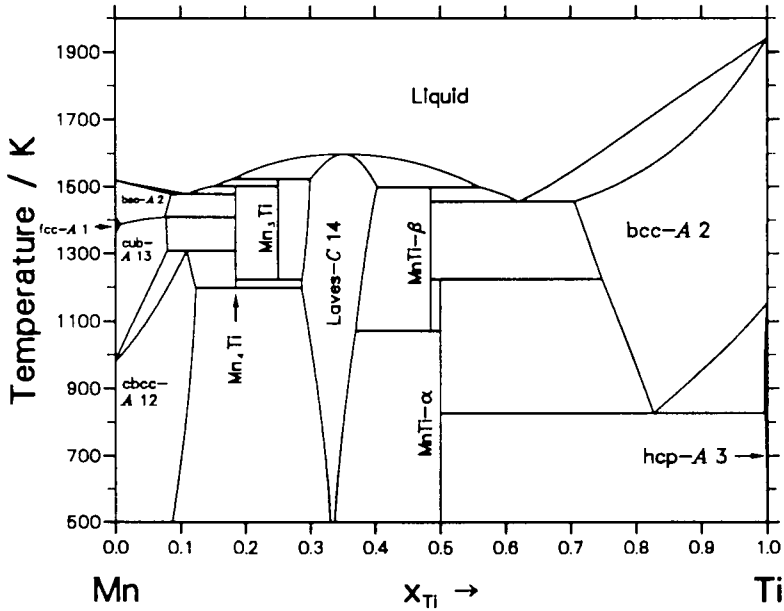


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Ti}	T / K
Liquid \rightleftharpoons bcc-A2 + Mn ₄ Ti	Eutectic	.111 .086 .185	1478.0
Liquid + Mn ₃ Ti \rightleftharpoons Mn ₄ Ti	Peritectic	.153 .250 .185	1502.8
Liquid + Laves-C14 \rightleftharpoons Mn ₃ Ti	Peritectic	.180 .300 .250	1523.5
Mn ₃ Ti \rightleftharpoons Mn ₄ Ti + Laves-C14	Eutectoid	.250 .185 .287	1222.3
Mn ₄ Ti \rightleftharpoons cbcc-A12 + Laves-C14	Eutectoid	.185 .124 .286	1198.4
cbcc-A12 + Mn ₄ Ti \rightleftharpoons cub-A13	Peritectoid	.080 .185 .110	1309.3
bcc-A2 + Mn ₄ Ti \rightleftharpoons cub-A13	Peritectoid	.076 .185 .078	1408.6
bcc-A2 \rightleftharpoons fcc-A1 + cub-A13	Eutectoid	.008 .005 .009	1387.6
Laves-C14 \rightleftharpoons Liquid	Congruent	.344 .344	1598.0
Liquid + Laves-C14 \rightleftharpoons MnTi-β	Peritectic	.560 .485 .403	1500.2
MnTi-β \rightleftharpoons Laves-C14 + MnTi-α	Eutectoid	.485 .369 .500	1071.3
MnTi-β + bcc-A2 \rightleftharpoons MnTi-α	Peritectoid	.485 .748 .500	1224.0
bcc-A2 \rightleftharpoons MnTi-α + hcp-A3	Eutectoid	.827 .500 .996	827.6
Liquid \rightleftharpoons MnTi-β + bcc-A2	Eutectic	.620 .485 .706	1455.5

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattice	Comments
Mn-Ti	α -Mn	α -Mn	<i>c584</i> <i>I43m</i>		cbcc-A12
	β -Mn	β -Mn	<i>cP20</i> <i>P4₁323m</i>		cub-A13
	γ -Mn	Cu	<i>cF4</i> <i>Fm3m</i>	M 4	fcc-A1
	δ -Mn	W	<i>cI2</i> <i>Im3m</i>	M 2	bcc-A2
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im3m</i>	M 2	
	MnTi- α		<i>t * 58</i>		
	MnTi- β				
	Mn ₃ Ti				
	Mn ₂ Ti	MgZn ₂	<i>hP12</i> <i>P6₃/mmc</i>	Mn ₁ 2 Mn ₂ 6 Ti 4	Laves-C14
Mn ₄ Ti	$\sim \delta(\text{Mo,Ni})$	<i>hR53</i> <i>R3</i>			

System Mn–Zr

Solution Phases:

Liquid, bcc-A2, cbcc-A12, cub-A13, fcc-A1, hcp-A3

Compound:

Mn₂Zr

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
cbcc-A12	:	Substitutional, Redlich-Kister
cub-A13	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Mn ₂ Zr	:	Stoichiometric, (Mn) ₂ (Zr)

Assessor and Date:

K. Hack, GTT, Germany (1997).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Mn₂Zr

$$\begin{aligned}
 G^\circ(T) - 3.0 H_{\text{Mn}}^{\circ, \text{cbcc-A12, para}}(298.15 \text{ K}) = G(\text{Mn:Mn}) = \\
 298.15 < T < 1519.00 & : -021345.84 + 390.177 T - 70.3746 T \cdot \ln T \\
 & \quad - 0.02204304 T^2 + 209481.3 T^{-1} \\
 1519.00 < T < 2000.00 & : -83200.23 + 936.7944 T - 144 T \cdot \ln T \\
 & \quad + 4.970541\text{E}+30 T^{-9} \\
 G^\circ(T) - 2.0 H_{\text{Mn}}^{\circ, \text{cbcc-A12, para}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mn:Zr}) = \\
 298.15 < T < 1900.00 & : -79282.375 + 386.94271 T - 71.0782 T \cdot \ln T \\
 & \quad - 0.01907327 T^2 + 174625.2 T^{-1} \\
 1900.00 < T < 2000.00 & : -119446.65 + 750.75589 T - 120.1618 T \cdot \ln T \\
 & \quad - 0.00437791 T^2 + 34971 T^{-1} \\
 & \quad + 3.313694\text{E}+30 T^{-9}
 \end{aligned}$$

$$G^{\circ}(T) - H_{\text{Mn}}^{\circ, \text{bcc-A12, para}}(298.15 \text{ K}) - 2.0 H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Zr:Mn}) =$$

$$298.15 < T < 1519.00 : -8770.8146 + 381.3571 T - 71.7818 T \cdot \ln T$$

$$- 0.0161035 T^2 + 139769.1 T^{-1}$$

$$1519.00 < T < 2000.00 : -29388.945 + 563.56289 T - 96.3236 T \cdot \ln T$$

$$- 0.00875582 T^2 + 69942 T^{-1}$$

$$+ 1.656847\text{E}+30 T^{-9}$$

$$G^{\circ}(T) - 3.0 H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Zr:Zr}) =$$

$$298.15 < T < 2128.00 : -8482.785 + 376.94715 T - 72.4854 T \cdot \ln T$$

$$- 0.01313373 T^2 + 104913 T^{-1}$$

$$2128.00 < T < 6000.00 : -63257.763 + 788.17255 T - 126.432 T \cdot \ln T$$

$$- 4.028685\text{E}+31 T^{-9}$$

$$I_{\text{Mn,Zr:Mn}}^{0, \text{Mn}_2\text{Zr}} = 18442.56 + 14.090471 T$$

$$I_{\text{Zr:Mn,Zr}}^{0, \text{Mn}_2\text{Zr}} = 18442.56 + 14.090471 T$$

$$I_{\text{Mn:Mn,Zr}}^{0, \text{Mn}_2\text{Zr}} = 1066.4675 + 10.504933 T$$

$$I_{\text{Mn,Zr:Zr}}^{0, \text{Mn}_2\text{Zr}} = 1066.4675 + 10.504933 T$$

Phase bcc-A2

$$L_{\text{Mn,Zr:}\square}^{0, \text{bcc-A2}} = -2135.3475 - 0.13258 T$$

$$L_{\text{Mn,Zr:}\square}^{1, \text{bcc-A2}} = -4084$$

Phase cbcc-A12

$$L_{\text{Mn,Zr:}\square}^{0, \text{cbcc-A12}} = 20000$$

Phase cub-A13

$$L_{\text{Mn,Zr:}\square}^{0, \text{cub-A13}} = 24000$$

Phase fcc-A1

$$L_{\text{Mn,Zr:}\square}^{0, \text{fcc-A1}} = 20000$$

Phase hcp-A3

$$L_{\text{Mn,Zr:}\square}^{0, \text{hcp-A3}} = 25000$$

Phase liquid

$$I_{\text{Mn,Zr}}^{0, \text{liquid}} = -35187.553 + 2.6983563 T$$

$$I_{\text{Mn,Zr}}^{1, \text{liquid}} = -1305.986$$

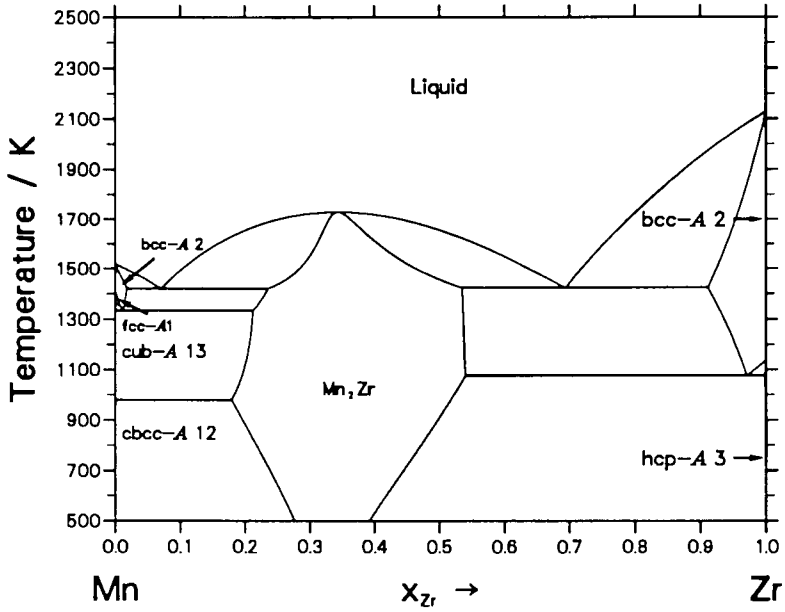


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Zr}	T / K
Liquid \rightleftharpoons bcc-A2 + Mn ₂ Zr	Eutectic	.071 .018 .236	1421.9
bcc-A2 \rightleftharpoons + cub-A13 + Mn ₂ Zr	Eutectoid	.012 .000 .213	1334.5
fcc-A1 \rightleftharpoons bcc-A2 + cub-A13	Metatectic	.0003 .0002 .0062	1359.1
cub-A13 \rightleftharpoons cbcc-A12 + Mn ₂ Zr	Degenerate	.000 .000 .179	980.1
Liquid \rightleftharpoons Mn ₂ Zr + bcc-A2	Eutectic	.694 .535 .911	1424.1
bcc-A2 \rightleftharpoons Mn ₂ Zr + hcp-A3	Eutectoid	.971 .540 .998	1075.4
Mn ₂ Zr \rightleftharpoons Liquid	Congruent	.345 .345	1730.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Mn-Zr	α -Mn	α -Mn	<i>c58</i> <i>I$\bar{4}$3m</i>		cbcc-A12
	β -Mn	β -Mn	<i>cP20</i> <i>P₄323m</i>		cub-A13
	γ -Mn	Cu	<i>cF4</i> <i>Fm3m</i>		
	δ -Mn	W	<i>cI2</i> <i>Im$\bar{3}$m</i>		
	(Zr)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Zr)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M 4	
	Mn ₂ Zr	MgZn ₂	<i>hP12</i> <i>P6₃/mmc</i>	Mn 2 Mn 6 Zr 4	Laves-C14

System Mo-Ti

Solution Phases:

(stable) Liquid, bcc-A2, hcp-A3
 (metastable) bcc-B2, fcc-A1

Compounds:

(metastable) AlM-D0₁₉, AlM-D0₂₂, AlTi-L1₀

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 bcc-B2 : Sublattice model, (Mo,Ti)_{0.5}(Mo,Ti)_{0.5}(□)₃
 The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 \rightleftharpoons bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 AlM-D0₁₉ : Sublattice model, (Mo,Ti)(Mo,Ti)₃
 AlM-D0₂₂ : Sublattice model, (Mo,Ti)₃(Mo,Ti)
 AlTi-L1₀ : Sublattice model, (Mo,Ti)(Mo,Ti)

Assessor and Date:

N. Saunders, 1995

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase liquid

$$L_{\text{Mo,Ti}}^{0,\text{liquid}} = -9000 + 2 T$$

Phase fcc-A1

$$L_{\text{Mo,Ti};\square}^{0,\text{fcc-A1}} = 16500$$

Phase hcp-A3

$$L_{\text{Mo,Ti};\square}^{0,\text{hcp-A3}} = 22760 - 6 T$$

Phase bcc-A2

$$L_{\text{Mo,Ti};\square}^{0,\text{bcc-A2}} = 2000$$

$$L_{\text{Mo,Ti};\square}^{1,\text{bcc-A2}} = -2000$$

Phase bcc-B2

$$G^\circ(T) - H_{\text{Mo}}^{0,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mo:Mo}) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Mo}}^{0,\text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mo:Ti}) = 5000$$

$$G^\circ(T) - 0.5 H_{\text{Mo}}^{0,\text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Mo}) = 5000$$

$$G^\circ(T) - H_{\text{Ti}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 0$$

$$L_{\text{Mo,Ti:Mo};\square}^{0,\text{bcc-B2}} = L_{\text{Mo,Ti:Ti};\square}^{0,\text{bcc-B2}} = -5000$$

$$L_{\text{Mo:Mo,Ti};\square}^{0,\text{bcc-B2}} = L_{\text{Ti:Mo,Ti};\square}^{0,\text{bcc-B2}} = -5000$$

Phase bcc-B2

$$G_{\text{Mo:Ti};\square}^* = 5000$$

$$G^\circ(T) - H_{\text{Mo}}^{0,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Mo:Mo};\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Mo}}^{0,\text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mo:Ti};\square) = 2.0 G_{\text{Mo:Ti};\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Mo}}^{0,\text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Mo};\square) = 2.0 G_{\text{Mo:Ti};\square}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti};\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Mo,Ti};\square}^{0,\text{bcc-A2}} = 2000$$

$$L_{\text{Mo,Ti};\square}^{1,\text{bcc-A2}} = -2000$$

Phase AIM-D0₁₉

$$\begin{aligned}
 G^\circ(T) - 4.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Mo:Mo}) = 4.0 \text{ GHCP}_{\text{Mo}} \\
 G^\circ(T) - 3.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Mo:Ti}) = \\
 &17072 - 4.5 T + 3.0 \text{ GHCP}_{\text{Mo}} + \text{GHSER}_{\text{Ti}} \\
 G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Mo}) = \\
 &17072 - 4.5 T + \text{GHCP}_{\text{Mo}} + 3.0 \text{ GHSER}_{\text{Ti}} \\
 G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 4.0 + 4.0 \text{ GHSER}_{\text{Ti}}
 \end{aligned}$$

Phase AIM-D0₂₂

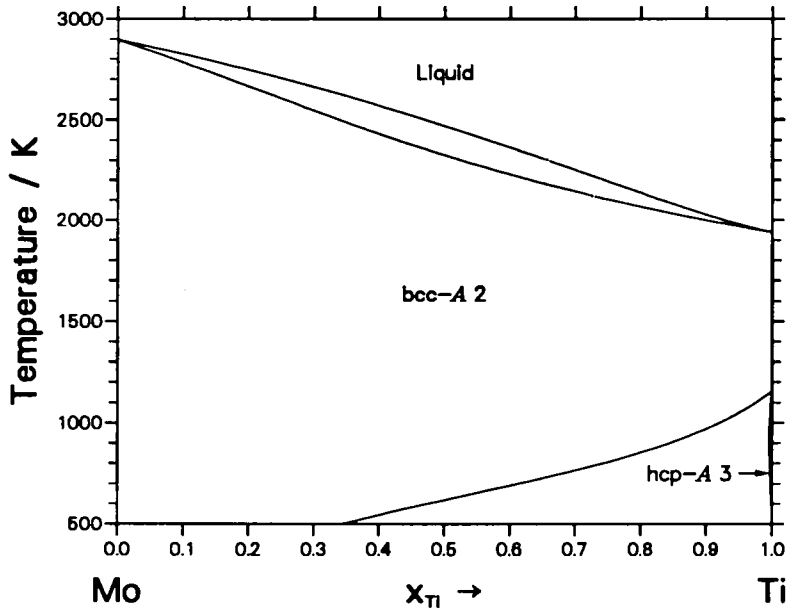
$$\begin{aligned}
 G^\circ(T) - 4.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Mo:Mo}) = 4.0 \text{ GFCC}_{\text{Mo}} \\
 G^\circ(T) - 3.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Mo:Ti}) = \\
 &3.0 \text{ GFCC}_{\text{Mo}} + \text{GFCC}_{\text{Ti}} \\
 G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Mo}) = \\
 &\text{GFCC}_{\text{Mo}} + 3.0 \text{ GFCC}_{\text{Ti}} \\
 G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 4.0 \text{ GFCC}_{\text{Ti}}
 \end{aligned}$$

Phase AlTi-L1₀

$$\begin{aligned}
 G^\circ(T) - 2.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Mo:Mo}) = 2.0 \text{ GFCC}_{\text{Mo}} \\
 G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Mo:Ti}) = \\
 &8250 + \text{GFCC}_{\text{Mo}} + \text{GFCC}_{\text{Ti}} \\
 G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Mo}) = \\
 &8250 + \text{GFCC}_{\text{Mo}} + \text{GFCC}_{\text{Ti}} \\
 G^\circ(T) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 2.0 \text{ GFCC}_{\text{Ti}} \\
 I_{\text{Mo,Ti:Mo}}^{0,\text{AlTi-L1}_0} &= L_{\text{Mo:Mo,Ti}}^{0,\text{AlTi-L1}_0} = 8250 \\
 I_{\text{Mo,Ti:Ti}}^{0,\text{AlTi-L1}_0} &= L_{\text{Ti:Mo,Ti}}^{0,\text{AlTi-L1}_0} = 8250
 \end{aligned}$$

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Mo-Ti	(Mo)	W	<i>cI2</i> <i>Im3m</i>	
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	
	(Ti)	W	<i>cI2</i> <i>Im3m</i>	



System N-Ti

Solution Phases:

Liquid, hcp-A3, bcc-A2, fcc-A1 ($\text{Ti}_x\text{N}_{1-x}$)

Compound:

Ti_2N , Ti_3N_2 , Ti_4N_3

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Sub-lattice, (Ti)(N,□)
hcp-A3	:	Sub-lattice, (Ti)(N,□)
fcc-A1	:	Sub-lattice, (Ti)(N,□)
Ti_2N	:	Stoichiometric, (Ti) ₂ (N)
Ti_3N_2	:	Stoichiometric, (Ti) _{0.29} (N) _{0.71}
Ti_4N_3	:	Stoichiometric, (Ti) _{0.315} (N) _{0.685}

Assessor and Date:

K. Zeng and R. Schmid-Fetzer, Univ. Clausthal, Germany, 1997

Comments:

The value of $\text{GHSER}_{\text{TiN}}$ is taken from S. Jonsson, Thesis, Royal Institute of Technology, Stockholm, Sweden (1993)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase fcc-A1

$$G^\circ(T) - H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \text{GHSER}_{\text{TiN}} =$$

$$- 357905.0 + 330.498 T - 52.4587 T \cdot \ln T - 9.28\text{E-}04 T^2$$

$$- 2.41\text{E+}09 T^{-3} + 871000.0 T^{-1}$$

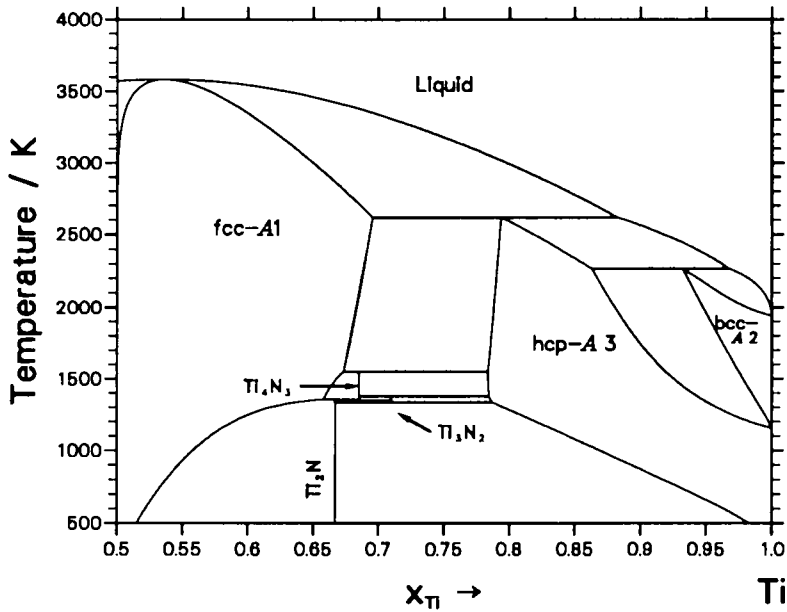
$$L_{\text{Ti};\text{CN}}^{0,\text{fcc-A1}} = - 42704.41$$

$$L_{\text{Ti};\text{CN}}^{1,\text{fcc-A1}} = - 13989.34$$

Phase Ti_4N_3

$$G^\circ(T) - 0.315 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) - 0.685 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$- 5956.8633 - 3.2749 T + 0.37 \text{GHSER}_{\text{Ti}} + 0.315 \text{GHSER}_{\text{TiN}}$$



Phase bcc-A2

$$G^{\circ}(T) - 3.0 H_{0.5N_2}^{\circ, \text{gas}}(298.15 \text{ K}) - H_{Ti}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:N}) =$$

$$2604201.62 + 118.04 T + \text{GHSE}_{TiN} + 2.0 \text{GHSE}_N$$

$$L_{Ti:N, \square}^{0, \text{bcc-A2}} = -3215338.17$$

Phase hcp-A3

$$G^{\circ}(T) - 0.5 H_{0.5N_2}^{\circ, \text{gas}}(298.15 \text{ K}) - H_{Ti}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:N}) =$$

$$-6046.53 - 2.653 T + 0.5 \text{GHSE}_{TiN} + 0.5 \text{GHSE}_{Ti}$$

$$L_{Ti:\square}^{0, \text{hcp-A3}} = -13501$$

Phase Ti₂N

$$G^{\circ}(T) - H_{0.5N_2}^{\circ, \text{gas}}(298.15 \text{ K}) - 2.0 H_{Ti}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$-67116 + 26.5395533 T + \text{GHSE}_{Ti} + \text{GHSE}_{TiN}$$

Phase Ti₃N₂

$$G^{\circ}(T) - 0.29 H_{0.5N_2}^{\circ, \text{gas}}(298.15 \text{ K}) - 0.71 H_{Ti}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$-8190.34 - 1.54816 T + 0.42 \text{GHSE}_{Ti} + 0.29 \text{GHSE}_{TiN}$$

Phase liquid

$$L_{N,Ti}^{0,liquid} = -376354.145$$

$$L_{N,Ti}^{1,liquid} = -98242.2945$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Ti}	T / K
$fcc-A1 + hcp-A3 \rightleftharpoons Ti_4N_3$	Peritectoid	.673 .784 .685	1551.1
$Ti_4N_3 + hcp-A3 \rightleftharpoons Ti_3N_2$	Peritectoid	.685 .784 .710	1376.8
$Ti_3N_2 \rightleftharpoons Ti_2N + hcp-A3$	Eutectoid	.710 .667 .787	1336.2
$Ti_4N_3 \rightleftharpoons Ti_2N + Ti_3N_2$	Eutectoid	.685 .667 .710	1348.5
$fcc-A1^* + Ti_3N_2 \rightleftharpoons Ti_2N$	Peritectoid	.658 .685 .667	1354.8
$Liquid + fcc-A1^* \rightleftharpoons hcp-A3$	Peritectic	.882 .695 .793	2618.0
$Liquid + hcp-A3 \rightleftharpoons bcc-A2$	Peritectic	.967 .863 .932	2268.6
$fcc-A1 \rightleftharpoons Liquid$	Congruent	.533 .541	3585.0

* $fcc-A1 \equiv Ti_xN_{1-x}$

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattice	Comments
N-Ti	0.5N ₂	gas			
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	TiN	ClNa	<i>cF8</i> <i>Fm$\bar{3}m$</i>	N 4 Ti 4	modelled as fcc-A1
	Ti ₂ N	anti-O ₂ Ti (rutile)	<i>tP6</i> <i>PA₂/mnm</i>	N 2 Ti 4	
	Ti ₄ N ₃	Ti ₇ S ₁₂	<i>hR8</i> <i>R$\bar{3}m$</i>	N ₁ 3 N ₂ 3 N ₃ 6 Ti ₁ 6 Ti ₂ 6	
	Ti ₃ N ₂				not indicated in [91Vil] nor in [90Mas]

System Nb–Ti

Solution Phases:

(stable) Liquid, bcc-*A2*, hcp-*A3*
 (metastable) bcc-*B2*, fcc-*A1*

Compounds:

(metastable) AlM-*D0₁₉*, AlM-*D0₂₂*, AlTi-*L1₀*, Cr₃Si-*A15*

Modelling:

Liquid : Substitutional, Redlich–Kister
 bcc-*A2* : Substitutional, Redlich–Kister
 bcc-*B2* : Sublattice model, (Nb,Ti)_{0.5}(Nb,Ti)_{0.5}(□)₃
 The thermodynamic description of the bcc-*B2* takes into account the ordering reaction bcc-*A2* ⇌ bcc-*B2*. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
 fcc-*A1* : Substitutional, Redlich–Kister
 hcp-*A3* : Substitutional, Redlich–Kister
 AlM-*D0₁₉* : Sublattice model, (Nb,Ti)(Nb,Ti)₃
 AlM-*D0₂₂* : Sublattice model, (Ti)₃(Nb,Ti)
 AlTi-*L1₀* : Sublattice model, (Nb,Ti)(Nb,Ti)
 Cr₃Si-*A15* : Sublattice model, (Nb,Ti)₃(Nb)

Assessor and Date:

N. Saunders, 1995

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase liquid

$$L_{\text{Nb,Ti}}^{0,\text{liquid}} = 8500$$

Phase fcc-A1

$$L_{\text{Nb,Ti};\square}^{0,\text{fcc-A1}} = 13600$$

$$L_{\text{Nb,Ti};\square}^{1,\text{fcc-A1}} = 1\text{E-}04$$

$$L_{\text{Nb,Ti};\square}^{2,\text{fcc-A1}} = 2500$$

Phase hcp-A3

$$L_{\text{Nb,Ti};\square}^{0,\text{hcp-A3}} = 13600$$

$$L_{\text{Nb,Ti};\square}^{1,\text{hcp-A3}} = 1\text{E-}04$$

$$L_{\text{Nb,Ti};\square}^{2,\text{hcp-A3}} = 2500$$

Phase Cr₃Si-A15

$$G^\circ(T) - 4.0 H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Nb:Nb}) =$$

$$20000 + 10 T + 4.0 \text{ GFCC}_{\text{Nb}}$$

$$G^\circ(T) - H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Nb}) =$$

$$20000 + 10 T + 3.0 \text{ GFCC}_{\text{Nb}} + \text{GFCC}_{\text{Ti}}$$

Phase bcc-A2

$$L_{\text{Nb,Ti};\square}^{0,\text{bcc-A2}} = 14000$$

$$L_{\text{Nb,Ti};\square}^{1,\text{bcc-A2}} = 1.0\text{E-}4$$

$$L_{\text{Nb,Ti};\square}^{2,\text{bcc-A2}} = 2500$$

Phase bcc-B2

$$G_{\text{Nb,Ti};\square}^* = 5500$$

$$G^\circ(T) - H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Nb:Nb}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$G(\text{Nb:Ti};\square) = G_{\text{Nb,Ti};\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$G(\text{Ti:Nb};\square) = G_{\text{Nb,Ti};\square}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}\square) = 0.0$$

$$L_{\text{Nb,Ti:Nb};\square}^{0,\text{bcc-B2}} = L_{\text{Nb,Ti,Ti};\square}^{0,\text{bcc-B2}} = - 5500$$

$$L_{\text{Nb:Nb,Ti};\square}^{0,\text{bcc-B2}} = L_{\text{Ti:Nb,Ti};\square}^{0,\text{bcc-B2}} = - 5500$$

Phase bcc-B2

$$G_{\text{Nb:Ti:}\square}^* = 5500$$

$$G^\circ(T) - H_{\text{Nb}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Nb:Nb:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Nb}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Nb:Ti:}\square) = 2.0 G_{\text{Nb:Ti:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Nb}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Nb:}\square) = 2.0 G_{\text{Nb:Ti:}\square}^*$$

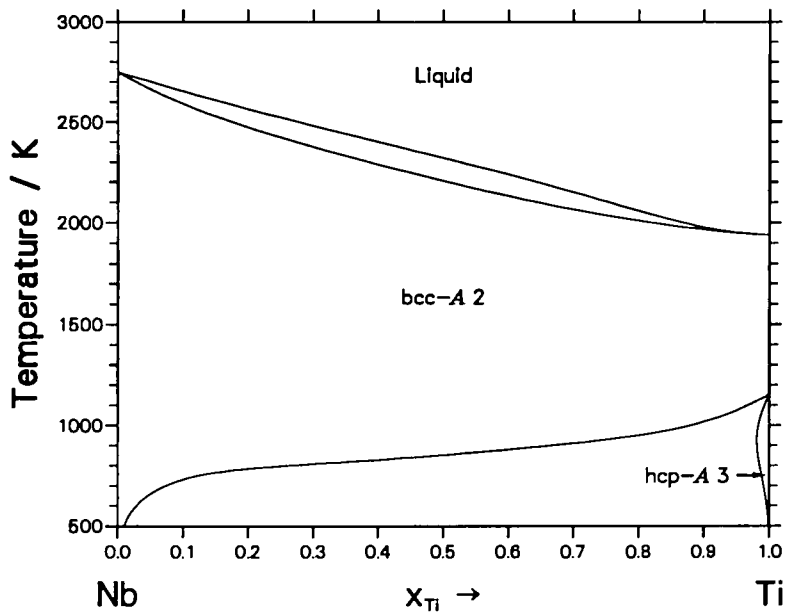
$$G^\circ(T) - H_{\text{Ti}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Nb, Ti:}\square}^{0, \text{bcc-A2}} = 14000$$

$$L_{\text{Nb, Ti:}\square}^{1, \text{bcc-A2}} = 1.0\text{E-4}$$

$$L_{\text{Nb, Ti:}\square}^{2, \text{bcc-A2}} = 2500$$



Phase AIM-D0₁₉

$$\begin{aligned}
G^\circ(T) - 4.0 H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Nb:Nb}) = 4.0 \text{ GHCP}_{\text{Nb}} \\
G^\circ(T) - 3.0 H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Nb:Ti}) = \\
&10668 + 3.0 \text{ GHCP}_{\text{Nb}} + \text{GHSER}_{\text{Ti}} \\
G^\circ(T) - H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Nb}) = \\
&10668 + \text{GHCP}_{\text{Nb}} + 3.0 \text{ GHSER}_{\text{Ti}} \\
G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 4.0 + 4.0 \text{ GHSER}_{\text{Ti}} \\
L_{\text{Nb,Ti:Nb}}^{0, \text{AIM-D0}_{19}} &= 30248 \\
L_{\text{Nb,Ti:Nb}}^{1, \text{AIM-D0}_{19}} &= 4220 \\
L_{\text{Nb,Ti:Nb}}^{2, \text{AIM-D0}_{19}} &= 3164 \\
L_{\text{Nb,Ti:Ti}}^{0, \text{AIM-D0}_{19}} &= 30248 \\
L_{\text{Nb,Ti:Ti}}^{1, \text{AIM-D0}_{19}} &= -4220 \\
L_{\text{Nb,Ti:Ti}}^{2, \text{AIM-D0}_{19}} &= 3164 \\
L_{\text{Nb:Nb,Ti}}^{0, \text{AIM-D0}_{19}} &= 4924 \\
L_{\text{Nb:Nb,Ti}}^{1, \text{AIM-D0}_{19}} &= 468 \\
L_{\text{Nb:Nb,Ti}}^{2, \text{AIM-D0}_{19}} &= 40 \\
L_{\text{Ti:Nb,Ti}}^{0, \text{AIM-D0}_{19}} &= 4924 \\
L_{\text{Ti:Nb,Ti}}^{1, \text{AIM-D0}_{19}} &= -468 \\
L_{\text{Ti:Nb,Ti}}^{2, \text{AIM-D0}_{19}} &= 40
\end{aligned}$$

Phase AIM-D0₂₂

$$\begin{aligned}
G^\circ(T) - H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Nb}) = \\
&\text{GFCC}_{\text{Nb}} + 3.0 \text{ GFCC}_{\text{Ti}} \\
G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 4.0 \text{ GFCC}_{\text{Ti}}
\end{aligned}$$

Phase AlTi-L1₀

$$\begin{aligned}
G^\circ(T) - 2.0 H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Nb:Nb}) = 2.0 \text{ GFCC}_{\text{Nb}} \\
G^\circ(T) - H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Nb:Ti}) = \\
&13600 + \text{GFCC}_{\text{Nb}} + \text{GFCC}_{\text{Ti}}
\end{aligned}$$

$$G^\circ(T) - H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Nb}) = 6800 + \text{GFCC}_{\text{Nb}} + \text{GFCC}_{\text{Ti}}$$

$$G^\circ(T) - 2.0 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 2.0 \text{ GFCC}_{\text{Ti}}$$

$$L_{\text{Nb,Ti:Nb}}^{0, \text{AlTi}-L1_0} = 7738$$

$$L_{\text{Nb,Ti:Nb}}^{1, \text{AlTi}-L1_0} = 1250$$

$$L_{\text{Nb,Ti:Nb}}^{2, \text{AlTi}-L1_0} = 312$$

$$L_{\text{Nb,Ti:Ti}}^{0, \text{AlTi}-L1_0} = 7738$$

$$L_{\text{Nb,Ti:Ti}}^{1, \text{AlTi}-L1_0} = -1250$$

$$L_{\text{Nb,Ti:Ti}}^{2, \text{AlTi}-L1_0} = 312$$

$$L_{\text{Nb:Nb,Ti}}^{0, \text{AlTi}-L1_0} = 7738$$

$$L_{\text{Nb:Nb,Ti}}^{1, \text{AlTi}-L1_0} = 1250$$

$$L_{\text{Nb:Nb,Ti}}^{2, \text{AlTi}-L1_0} = 312$$

$$L_{\text{Ti:Nb,Ti}}^{0, \text{AlTi}-L1_0} = 7738$$

$$L_{\text{Ti:Nb,Ti}}^{1, \text{AlTi}-L1_0} = -1250$$

$$L_{\text{Ti:Nb,Ti}}^{2, \text{AlTi}-L1_0} = 312$$

$$L_{\text{Nb,Ti:Nb,Ti}}^{0, \text{AlTi}-L1_0} = -7500$$

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Nb-Ti	(Nb)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	
	(Ti)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	

System Ni-V

Solution Phases:

Liquid, bcc-A2, fcc-A1, σ

Compounds:

Ni₂V, Ni₃V, Ni₂V₇

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
Ni ₂ V	:	Stoichiometric, (Ni) ₂ (V)
Ni ₃ V	:	Stoichiometric, (Ni) ₃ (V)
Ni ₂ V ₇	:	Stoichiometric, (Ni) ₂ (V) ₇
σ	:	Sublattice model, (Ni) ₈ (V) ₄ (Ni,V) ₁₈

Publication:

J. Korb, and K. Hack, GTT, Germany (1997).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Ni,V};\square}^{0,\text{bcc-A2}} = -30513.8 + 12.6138 T$$

Phase fcc-A1

$$L_{\text{Ni,V};\square}^{0,\text{fcc-A1}} = -36365.6 + 3.75677 T$$

$$L_{\text{Ni,V};\square}^{1,\text{fcc-A1}} = 11860.7 - 9.0302 T$$

$$L_{\text{Ni,V};\square}^{2,\text{fcc-A1}} = -10647.5 + 7.00954 T$$

Phase liquid

$$L_{\text{Ni,V}}^{0,\text{liquid}} = -51927 + 14.99 T$$

Phase Ni₂V

$$G^\circ(T) - 2.0 H_{\text{Ni}}^{\circ, \text{fcc-A1, para}}(298.15 \text{ K}) - H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$- 38032.065 + 337.2614 T - 64.6973 T \cdot \ln T - 0.01512 T^2$$

$$- 13.75326 T^{-1}$$

Phase Ni₃V

$$G^\circ(T) - 3.0 H_{\text{Ni}}^{\circ, \text{fcc-A1, para}}(298.15 \text{ K}) - H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$- 45524.96 + 529.01852 T - 99.74166 T \cdot \ln T - 0.00824 T^2$$

$$- 13753.332 T^{-1}$$

Phase Ni₂V₇

$$G^\circ(T) - 2.0 H_{\text{Ni}}^{\circ, \text{fcc-A1, para}}(298.15 \text{ K}) - 7.0 H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$- 190634.14 + 1333.90548 T - 233.55668 T \cdot \ln T - 0.00482 T^2$$

$$- 5.196308E-06 T^3 + 844557.21 T^{-1}$$

Phase σ

$$G^\circ(T) - 26.0 H_{\text{Ni}}^{\circ, \text{fcc-A1, para}}(298.15 \text{ K}) - 4.0 H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ni:V:Ni}) =$$

$$298.15 < T < 790.00 : - 161645.05 + 3532.8443 T - 671.032 T \cdot \ln T$$

$$- 0.1382502 T^2 + 4.87E-07 T^3 + 277840 T^{-1}$$

$$790.00 < T < 1728.00 : - 161794.7 + 3572.6245 T - 678.096 T \cdot \ln T$$

$$- 0.1256082 T^2 - 2.72E-06 T^3$$

$$G^\circ(T) - 8.0 H_{\text{Ni}}^{\circ, \text{fcc-A1, para}}(298.15 \text{ K}) - 22.0 H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ni:V:V}) =$$

$$298.15 < T < 790.00 : - 663330.65 + 4012.7719 T - 707.716 T \cdot \ln T$$

$$- 0.1068816 T^2 + 2.6785E-06 T^3 + 1528120 T^{-1}$$

$$790.00 < T < 1728.00 : - 664153.72 + 4231.5628 T - 746.568 T \cdot \ln T$$

$$- 0.0373506 T^2 - 1.496E-05 T^3$$

Table I - Invariant Reactions.

Reaction	Type	Compositions x_{2r}	T / K
Liquid + bcc-A2 \rightleftharpoons σ	Peritectic	.626 .769 .662	1552.3
σ + bcc-A2 \rightleftharpoons Ni ₂ V ₇	Peritectoid	.727 .922 .778	1171.9
Liquid \rightleftharpoons fcc-A1 + σ	Eutectic	.501 .443 .578	1485.7
fcc-A1 \rightleftharpoons Ni ₂ V + σ	Eutectoid	.368 .333 .554	1150.9
fcc-A1 \rightleftharpoons Ni ₃ V + Ni ₂ V	Eutectoid	.313 .250 .333	1175.5
Ni ₃ V \rightleftharpoons fcc-A1	Congruent	.250 .250	1324.0
Ni ₂ V \rightleftharpoons fcc-A1	Congruent	.333 .333	1190.0

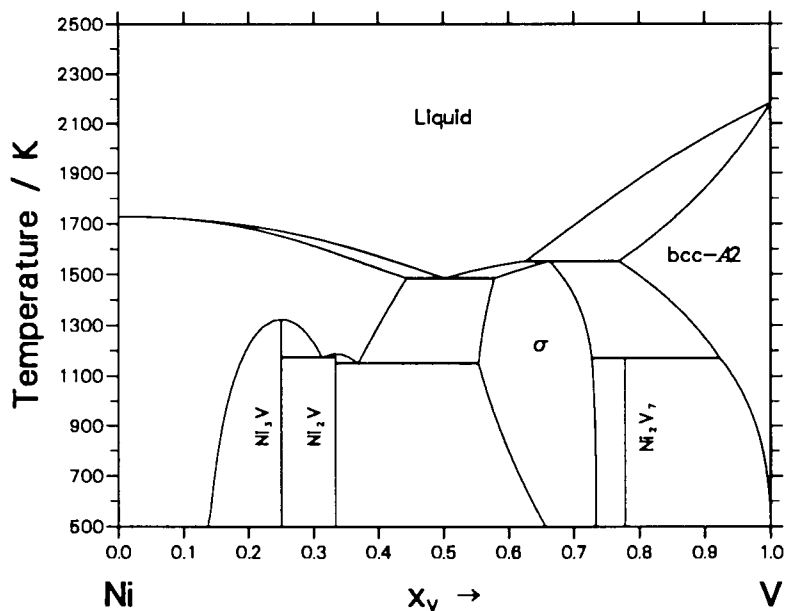


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Ni-V	(Ni)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	High and low forms given in [90Mas] assumed to be Ni ₂ V ₇ by the assessors
	(V)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>		
	Ni ₁₈ V	NbNi ₁₈	<i>tI18</i>		
	Ni ₃ V	Al ₃ Ti	<i>tI8</i> <i>I4/mmm</i>	Ni ₁ 2 Ni ₂ 4 V 2	
	Ni ₂ V σ	MoPt ₂ σ CrFe	<i>oI6</i> <i>tP30</i> <i>P4₂/mnm</i>		
	NiV ₃	Cr ₃ Si	<i>cP8</i> <i>Pm$\bar{3}n$</i>	Cr 6 Si 2	

System Si–Sn

Solution Phases:

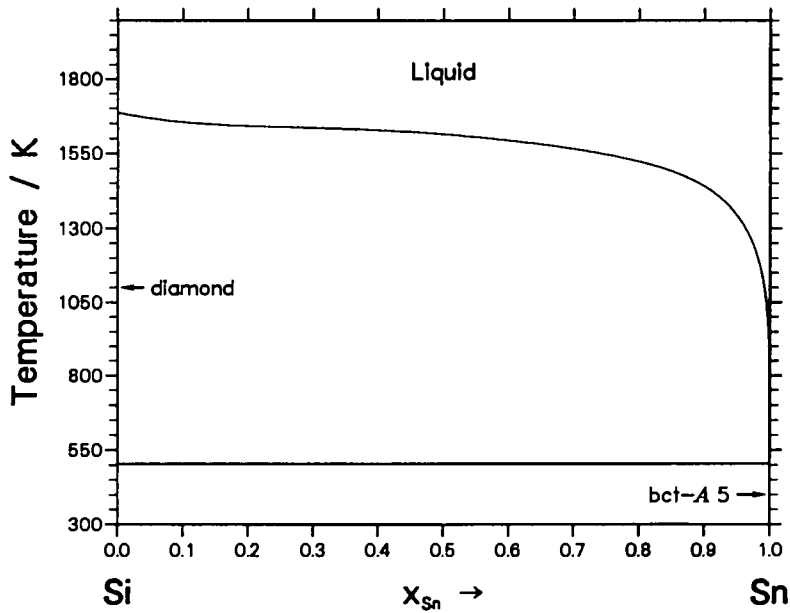
Liquid, diamond

Modelling:

Liquid : Substitutional, Redlich–Kister
diamond : Substitutional, Redlich–Kister

Assessor and Date:

H.L. Lukas 1993



Thermodynamic properties of the solution phases (J.mol⁻¹)**Phase diamond**

$$I_{\text{Si,Sn}}^{0,\text{diamond}} = 25265.65 + 23.84 T$$

Phase liquid

$$I_{\text{Si,Sn}}^{0,\text{liquid}} = 25364.6$$

$$I_{\text{Si,Sn}}^{1,\text{liquid}} = 3148.8$$

$$I_{\text{Si,Sn}}^{2,\text{liquid}} = 4460.9$$

Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Sn}	T / K
Liquid \rightleftharpoons bct-A5 + diamond	Degenerate	.000 .000 1.000	505.1

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Si-Sn	(Si)	diamond	<i>cF8</i> <i>Fd3m</i>
	(Sn)	β -Sn	<i>tI4</i> <i>I4₁/amd</i>

System Si–Ti

Solution Phases:

Liquid, bcc-A2, hcp-A3

Compounds:

Si₂Ti, Si₄Ti₅, SiTi, SiTi₃, Si₃Ti₅

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc-A2	:	Substitutional, Redlich–Kister
hcp-A3	:	Substitutional, Redlich–Kister
Si ₂ Ti	:	Stoichiometric (Si) ₂ (Ti)
Si ₄ Ti ₅	:	Stoichiometric (Si) ₄ (Ti) ₅
SiTi	:	Stoichiometric, (Si)(Ti)
SiTi ₃	:	Stoichiometric, (Si)(Ti) ₃
Si ₃ Ti ₅	:	Sublattice model, (Si,Ti) ₂ (Si,Ti) ₃ (Ti) ₃
	:	

Assessor and Date:

H. Seifert

Publication:

Thesis, Univ. Stuttgart, Germany (1994)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Si₂Ti

$$G^{\circ}(T) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 175038.5 + 4.54 T + 2.0 \text{ GHSE}_{\text{Si}} + \text{GHSE}_{\text{Ti}}$$

Phase Si₄Ti₅

$$G^{\circ}(T) - 4.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 711000.0 + 22.37355 T + 4.0 \text{ GHSE}_{\text{Si}} + 5.0 \text{ GHSE}_{\text{Ti}}$$

Phase SiTi

$$G^{\circ}(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 155061.7 + 7.6345 T + \text{GHSE}_{\text{Si}} + \text{GHSE}_{\text{Ti}}$$

Phase Si₃Ti₅

$$G^\circ(T) - 5.0 H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = G(\text{Si:Si:Ti}) =$$

$$- 206191.45 + 16.4953 T + 5.0 \text{ GHSER}_{\text{Si}} + 3.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) - 5.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Si:Ti}) =$$

$$- 583564.31 + 2.68514 T + 3.0 \text{ GHSER}_{\text{Si}} + 5.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 2.0 H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) - 6.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = G(\text{Si:Ti:Ti}) =$$

$$417372.85 + 33.81017 T + 2.0 \text{ GHSER}_{\text{Si}} + 6.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 8.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti:Ti}) =$$

$$40000.0 + 20.0 T + 8.0 \text{ GHSER}_{\text{Ti}}$$

$$L_{\text{Si,Ti:Si:Ti}}^{0,\text{Si}_3\text{Ti}_5} = -500000 + 40.0 T$$

$$L_{\text{Si,Ti:Ti:Ti}}^{0,\text{Si}_3\text{Ti}_5} = -500000 + 40.0 T$$

$$L_{\text{Si:Si,Ti:Ti}}^{0,\text{Si}_3\text{Ti}_5} = 43024.29 - 3.44194 T$$

$$L_{\text{Ti:Si,Ti:Ti}}^{0,\text{Si}_3\text{Ti}_5} = 43024.29 - 3.44194 T$$

Phase SiTi₃

$$G^\circ(T) - H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$- 200000.0 + 3.19924 T + \text{GHSER}_{\text{Si}} + 3.0 \text{ GHSER}_{\text{Ti}}$$

Phase bcc-A2

$$L_{\text{Si,Ti:}\square}^{0,\text{bcc-A2}} = - 275629.1 + 42.5094 T$$

$$L_{\text{Si,Ti:}\square}^{1,\text{bcc-A2}} = 25025.35 - 2.00203 T$$

$$L_{\text{Si,Ti:}\square}^{2,\text{bcc-A2}} = 83940.65 - 6.71526 T$$

Phase diamond

$$L_{\text{Si,Ti}}^{0,\text{diamond}} = 80 T$$

Phase hcp-A3

$$L_{\text{Si,Ti:}\square}^{0,\text{hcp-A3}} = - 302731.04 + 69.08469 T$$

$$L_{\text{Si,Ti:}\square}^{1,\text{hcp-A3}} = 25025.35 - 2.00203 T$$

$$L_{\text{Si,Ti:}\square}^{2,\text{hcp-A3}} = 83940.65 - 6.71526 T$$

Phase liquid

$$L_{\text{Si,Ti}}^{0,\text{liquid}} = -255852.17 + 21.87411 T$$

$$L_{\text{Si,Ti}}^{1,\text{liquid}} = 25025.35 - 2.00203 T$$

$$L_{\text{Si,Ti}}^{2,\text{liquid}} = 83940.65 - 6.71526 T$$

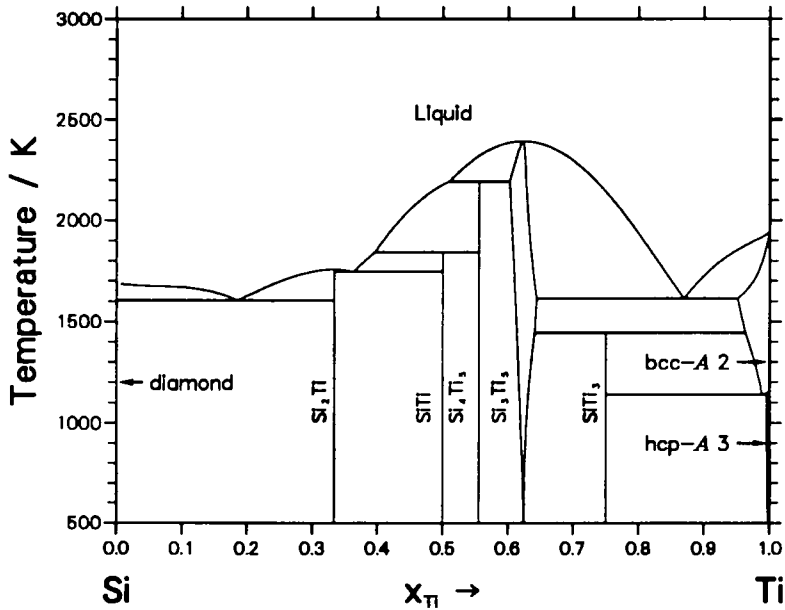


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Ti}			T / K
Liquid \rightleftharpoons diamond + Si_2Ti	Eutectic	.185	.000	.333	1604.3
Liquid \rightleftharpoons Si_2Ti + SiTi	Eutectic	.363	.333	.500	1747.4
$\text{Si}_2\text{Ti} \rightleftharpoons$ Liquid	Congruent	.333	.333	1757.0
Liquid + $\text{Si}_4\text{Ti}_5 \rightleftharpoons$ SiTi	Peritectic	.396	.556	.500	1842.8
Liquid + $\text{Si}_3\text{Ti}_5 \rightleftharpoons$ Si_4Ti_5	Peritectic	.509	.602	.555	2192.6
$\text{Si}_3\text{Ti}_5 \rightleftharpoons$ Liquid	Congruent	.625	.625	2394.0
Liquid \rightleftharpoons Si_3Ti_5 + bcc-A2	Eutectic	.869	.644	.951	1613.0
Si_3Ti_5 + bcc-A2 \rightleftharpoons SiTi_3	Peritectoid	.641	.963	.750	1443.2
bcc-A2 \rightleftharpoons SiTi_3 + hcp-A3	Eutectoid	.988	.750	.995	1139.4

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Si-Ti	(Si)	diamond	<i>cF8</i> <i>Fd$\bar{3}m$</i>		
	(Ti)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>		
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>		
	TiSi ₂	TiSi ₂	<i>oF24</i> <i>Fddd</i>		
	TiSi	TiSi	<i>oP8</i> <i>Pmm2</i>	Si ₁ 2 Si ₂ 2 Ti ₁ 1 Ti ₂ 1 Ti ₃ 1 Ti ₄ 1	
	TiSi	FeB	<i>oP8</i> <i>Pnma</i>		also given in [90Mas]
	Ti ₃ Si	PTi ₃	<i>tP32</i> <i>P4₂/n</i>		
	Ti ₅ Si ₃	Mn ₅ Si ₃	<i>hP16</i> <i>P6$_3$/mcm</i>	Si 6 Ti ₁ 4 Ti ₂ 6	
Ti ₅ Si ₄	Si ₄ Zr ₅	<i>tP36</i> <i>P4₁2₁2</i>			

System Si–V

Solution Phases:

Liquid, bcc-A2

Compounds:

Si₂V, Si₃V₅, Si₅V₆, SiV₃

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc-A2	:	Substitutional, Redlich–Kister
SiV ₃	:	Sublattice model, (Si,V)(Si,V) ₃
Si ₂ V	:	Stoichiometric (Si) ₂ (V)
Si ₃ V ₅	:	Stoichiometric (Si) ₃ (V) ₅
Si ₅ V ₆	:	Stoichiometric (Si) ₅ (V) ₆

Assessor and Date:

M.H. Rand, and N. Saunders 1994

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Si₂V

$$G^\circ(T) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{V}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = \\ - 143160.0 + 401.98 T - 67.8 T \cdot \ln T - 0.0075 T^2 \\ + 330000.0 T^{-1}$$

Phase Si₃V₅

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 H_{\text{V}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = \\ - 504000.0 + 1259.03 T - 211.04 T \cdot \ln T - 0.00748 T^2 \\ + 1680000.0 T^{-1}$$

Phase Si₅V₆

$$G^\circ(T) - 5.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 6.0 H_{\text{V}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = \\ - 641675.0 + 1665.98 T - 280.28 T \cdot \ln T - 0.013915 T^2 \\ + 2310000.0 T^{-1}$$

Phase SiV₃

$$G^\circ(T) - 4.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si}) = 208000.0 - 80.0 T + 4.0 \text{ GHSER}_{\text{Si}}$$

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 H_{\text{V}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Si:V}) = -216397.0 + 516.532 T - 90.44 T \cdot \ln T - 0.008346 T^2 + 358000 T^{-1}$$

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{V}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{V:Si}) = 166000.0 - 60.0 T + 3.0 \text{ GHSER}_{\text{Si}} + \text{GIISER}_{\text{V}}$$

$$G^\circ(T) - 4.0 H_{\text{V}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{V:V}) = 18000.0 + 10.0 T + 4.0 \text{ GIISER}_{\text{V}}$$

$$L_{\text{Si,V:Si}}^{0,\text{SiV}_3} = 9794.5 - 21.8 T$$

$$L_{\text{Si,V:V}}^{0,\text{SiV}_3} = 9794.5 - 21.8 T$$

$$L_{\text{Si:Si,V}}^{0,\text{SiV}_3} = -150000$$

$$L_{\text{V:Si,V}}^{0,\text{SiV}_3} = 0.0$$

Phase bcc-A2

$$L_{\text{Si,V:O}}^{0,\text{bcc-A2}} = -164505 + 30.1 T$$

$$L_{\text{Si,V:O}}^{1,\text{bcc-A2}} = 37000$$

$$L_{\text{Si,V:O}}^{2,\text{bcc-A2}} = 20000$$

Phase liquid

$$L_{\text{Si,V}}^{0,\text{liquid}} = -180900 + 40 T$$

$$L_{\text{Si,V}}^{1,\text{liquid}} = 37000$$

$$L_{\text{Si,V}}^{2,\text{liquid}} = 20000$$

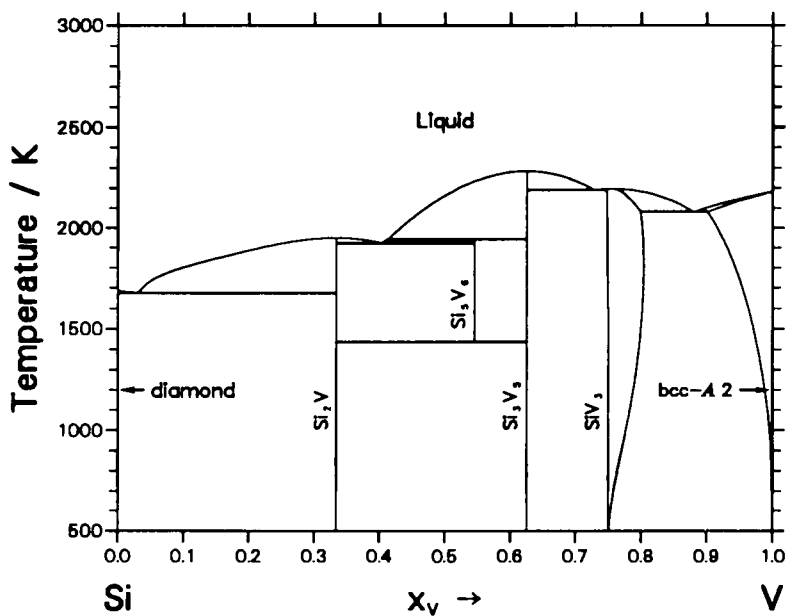


Table I – Invariant Reactions.

Reaction	Type	Compositions x_V			T / K
Liquid \rightleftharpoons diamond + Si_2V	Eutectic	.031	.000	.333	1675.1
$Si_2V \rightleftharpoons$ Liquid	Congruent	.333	.333	1952.0
Liquid \rightleftharpoons Si_2V + Si_5V_6	Eutectic	.403	.333	.545	1923.9
Liquid + $Si_3V_5 \rightleftharpoons$ Si_5V_6	Peritectic	.412	.625	.545	1943.1
$Si_3V_5 \rightleftharpoons$ Liquid	Congruent	.625	.625	2284.0
Liquid \rightleftharpoons Si_3V_5 + SiV_3	Eutectic	.727	.625	.748	2190.8
$SiV_3 \rightleftharpoons$ Liquid	Congruent	.750	.750	2196.0
Liquid \rightleftharpoons SiV_3 + bcc-A2	Eutectic	.879	.799	.901	2081.1
$Si_5V_6 \rightleftharpoons$ Si_2V + Si_3V_5	Eutectoid	.545	.333	.625	1434.7

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Si-V	(Si)	diamond	<i>cF8</i> <i>Fd$\bar{3}m$</i>	M 8	
	(V)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	SiV ₃	Cr ₃ Si	<i>cP8</i> <i>Pm$\bar{3}n$</i>	Si 2 V 6	
	Si ₂ V	CrSi ₂	<i>hP9</i> <i>P6₂22</i>	Si 6 V 4	
	Si ₃ V ₅	Si ₃ W ₅	<i>tI32</i> <i>I4/mcm</i>		
	Si ₅ V ₆	Nb ₅ Sn ₅	<i>oI44</i> <i>Immm</i>	Si ₁ 4 Si ₂ 8 Si ₃ 8 V ₁ 8 V ₂ 8 V ₃ 8	Ge ₅ Ti ₆ , <i>Ibam</i> in [91Vil]

System Si–Y

Solution Phases:

Liquid, bcc-A2, hcp-A3

Compounds:

Si₂Y–R, Si₂Y–H, Si₅Y₃–R, Si₅Y₃–H, SiY,
Si₃Y₅, Si₄Y₅

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc-A2	:	Substitutional, Redlich–Kister
hcp-A3	:	Substitutional, Redlich–Kister
Si ₂ Y–H	:	Stoichiometric, (Si) ₂ (Y)–H
Si ₂ Y–R	:	Stoichiometric, (Si) ₂ (Y)–R
Si ₅ Y ₃ –H	:	Stoichiometric (Si) ₅ (Y) ₃ –H
Si ₅ Y ₃ –R	:	Stoichiometric (Si) ₅ (Y) ₃ –R
SiY	:	Stoichiometric, (Si)(Y)
Si ₃ Y ₅	:	Stoichiometric, (Si) ₃ (Y) ₅
Si ₄ Y ₅	:	Stoichiometric, (Si) ₄ (Y) ₅

Assessor and Date:

H.L. Lukas 1991

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Si₂Y–H

$$G^{\circ}(T) - 2.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) - H_{\text{Y}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 21463.0 + 28.5 T + 2.0 \text{ GHSE}_{\text{Si}} + \text{GHSE}_{\text{Y}}$$

Phase Si₂Y–R

$$G^{\circ}(T) - 2.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) - H_{\text{Y}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\ - 219201.0 + 31.5 T + 2.0 \text{ GHSE}_{\text{Si}} + \text{GHSE}_{\text{Y}}$$

Phase Si₃Y₅

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 H_{\text{Y}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 588000.0 + 76.0 T + 3.0 \text{ GHSER}_{\text{Si}} + 5.0 \text{ GHSER}_{\text{Y}}$$

Phase Si₄Y₅

$$G^\circ(T) - 4.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 H_{\text{Y}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 697950.0 + 86.72688 T + 4.0 \text{ GHSER}_{\text{Si}} + 5.0 \text{ GHSER}_{\text{Y}}$$

Phase SiY

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Y}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 160700.0 + 19.8 T + \text{GHSER}_{\text{Si}} + \text{GHSER}_{\text{Y}}$$

Phase Si₅Y₃-H

$$G^\circ(T) - 5.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 H_{\text{Y}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 601572.0 + 76.0 T + 5.0 \text{ GHSER}_{\text{Si}} + 3.0 \text{ GHSER}_{\text{Y}}$$

Phase Si₅Y₃-R

$$G^\circ(T) - 5.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 H_{\text{Y}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 607356.0 + 84.0 T + 5.0 \text{ GHSER}_{\text{Si}} + 3.0 \text{ GHSER}_{\text{Y}}$$

Phase bcc-A2

$$L_{\text{Si,Y};\square}^{0,\text{bcc-A2}} = 80 T$$

Phase hcp-A3

$$L_{\text{Si,Y};\square}^{0,\text{hcp-A3}} = 80 T$$

Phase liquid

$$L_{\text{Si,Y}}^{0,\text{liquid}} = - 212656.12 + 25.83471 T$$

$$L_{\text{Si,Y}}^{1,\text{liquid}} = 13977.08 - 31.08941 T$$

$$L_{\text{Si,Y}}^{2,\text{liquid}} = 62049.23 - 50.31476 T$$

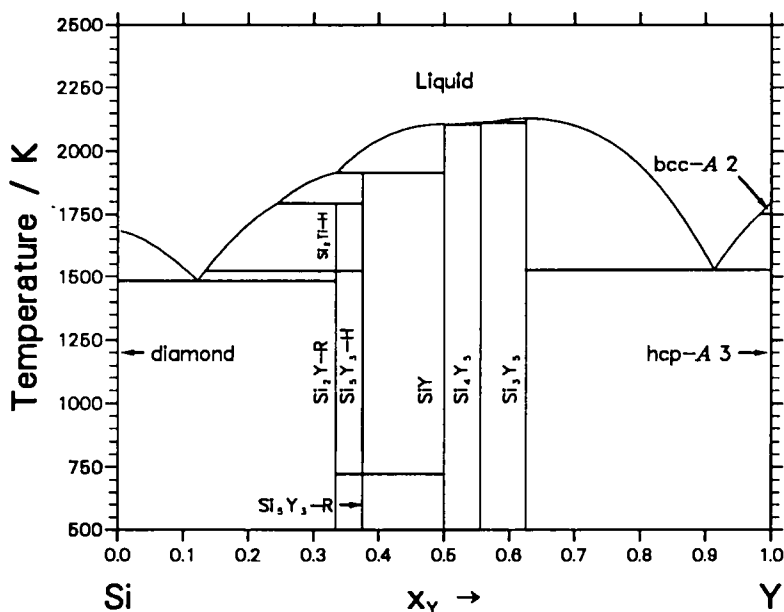


Table I – Invariant Reactions.

Reaction	Type	Compositions x_Y			T / K
Liquid \rightleftharpoons diamond + Si ₂ Y-R	Eutectic	.122	.000	.333	1485.3
Si ₂ Y-R \rightleftharpoons Si ₂ Y-H	Polymorphic	.333	.333	1523.0
Liquid + Si ₃ Y ₃ -H \rightleftharpoons Si ₂ Y-H	Peritectic	.244	.375	.333	1793.2
Liquid + SiY \rightleftharpoons Si ₃ Y ₃ -H	Peritectic	.335	.500	.375	1915.3
SiY \rightleftharpoons Liquid	Congruent	.500	.500	2108.0
Liquid \rightleftharpoons SiY + Si ₄ Y ₅	Eutectic	.518	.500	.556	2107.0
Si ₄ Y ₅ \rightleftharpoons Liquid	Congruent	.556	.556	2114.5
Liquid \rightleftharpoons Si ₄ Y ₅ + Si ₃ Y ₅	Eutectic	.567	.556	.625	2113.9
Si ₃ Y ₅ \rightleftharpoons Liquid	Congruent	.625	.625	2132.0
Liquid \rightleftharpoons Si ₃ Y ₅ + hcp-A 3	Eutectic	.913	.625	1.000	1527.9
hcp-A 3 \rightleftharpoons bcc-A 2	Allotropic	1.000	1.000	1752.0
Si ₃ Y ₃ -R \rightleftharpoons Si ₃ Y ₃ -H	Polymorphic	.375	.375	723.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Si-Y	(Si)	C(diamond)	<i>cF8</i> <i>Fd$\bar{3}m$</i>	M 8	
	(Y)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2	
	(Y)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	Si ₂ Y- α	AlB ₂	<i>hP3</i> <i>P6/mmm</i>		designated as Si ₂ Y-R
	Si ₂ Y- β	Si ₂ Th	<i>oI12</i> <i>Imma</i>		designated as Si ₂ Y-H Gd ₂ Si ₃ -type in [91Vil]
	Si ₃ Y ₅	Mn ₅ Si ₃	<i>hP16</i> <i>P6$_3$/mcm</i>	Si 6 Y ₁ 4 Y ₂ 6	
	Si ₄ Y ₅	Si ₄ Y ₅	<i>tP36</i> <i>P4$_1$2$_1$2</i>	Si ₁ 8 Si ₂ 8 Zr ₁ 4 Zr ₂ 8 Zr ₃ 8	
	Si ₅ Y ₃ - α	AlB ₂	<i>hP3</i> <i>P6/mmm</i>	Si 2 Y 1	designated as Si ₅ Y ₃ -R
	Si ₅ Y ₃ - β	ThSi ₂			designated as Si ₅ Y ₃ -H
	SiY	CrB	<i>oC8</i> <i>Cmcm</i>	Si 4 Y 4	

System Si–Zn

Solution Phases:

Liquid, diamond, hcp–Zn

Modelling:

Liquid : Substitutional, Redlich–Kister
diamond : Substitutional, Redlich–Kister
hcp–Zn : Substitutional, Redlich–Kister

Assessor and Date:

M. Jacobs 1993

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase diamond

$$L_{\text{Si,Zn}}^{0,\text{diamond}} = 100 T$$

Phase hcp–Zn

$$L_{\text{Si,Zn}}^{0,\text{hcp-Zn}} = 80 T$$

Phase liquid

$$L_{\text{Si,Zn}}^{0,\text{liquid}} = 7829.25$$

$$L_{\text{Si,Zn}}^{1,\text{liquid}} = -3338.18$$

$$L_{\text{Si,Zn}}^{2,\text{liquid}} = -891.33$$

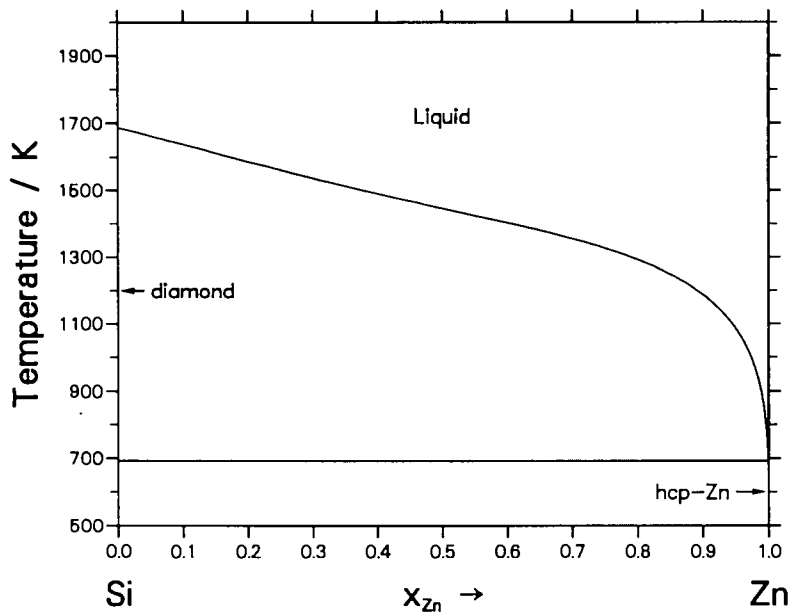


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Zn}	T / K
Liquid \rightleftharpoons diamond + hcp-Zn	Degenerate	1.000 .000 1.000	692.1

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Si-Zn	(Si)	diamond	$cF8$ $Fd\bar{3}m$
	(Zn)	Mg	$hP2$ $P6_3/mmc$

System Si–Zr

Solution Phases:

Liquid

Compounds:

Si₂Zr, Si₂Zr₃, Si₃Zr₅, Si₄Zr₅, SiZr, SiZr₂, SiZr₃

Modelling:

Liquid	:	Substitutional, Redlich–Kister
Si ₂ Zr	:	Stoichiometric (Si) ₂ (Zr)
Si ₂ Zr ₃	:	Stoichiometric (Si) ₂ (Zr) ₃
Si ₃ Zr ₅	:	Stoichiometric (Si) ₃ (Zr) ₅
Si ₄ Zr ₅	:	Stoichiometric (Si) ₄ (Zr) ₅
SiZr	:	Stoichiometric (Si)(Zr)
SiZr ₂	:	Stoichiometric, (Si)(Zr) ₂
SiZr ₃	:	Stoichiometric (Si)(Zr) ₃

Assessor and Date:

C. Gueneau, C. Servant, I. Ansara, and N. Dupin

Publication:

Calphad, 18, 3, 319-327 (1994)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase liquid

$$L_{\text{Si,Zr}}^{0,\text{liquid}} = -190000.0 + 16.8955 T$$

$$L_{\text{Si,Zr}}^{1,\text{liquid}} = 14.52575 T$$

Phase Si₂Zr

$$G^\circ(T) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ -189332.0 + 354.937 T - 63.16867 T \cdot \ln T - 7.67745\text{E-}03 T^2 \\ - 1.972048\text{E-}11 T^3 + 139751.1 T^{-1}$$

Phase SiZr

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 182203.4 + 258.514 T - 45.18631 T \cdot \ln T - 4.393865\text{E-}03 T^2 \\ + 5.49699\text{E-}11 T^3 + 148517.5T^{-1}$$

Phase Si₄Zr₅

$$G^\circ(T) - 4.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 880743.11 + 1433.658 T - 240.256 T \cdot \ln T - 0.0109481 T^2 \\ + 6.591183\text{E-}07 T^3 + 2006425 T^{-1}$$

Phase Si₂Zr₃

$$G^\circ(T) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 493990.62 + 844.448 T - 140.103 T \cdot \ln T - 0.003701 T^2 \\ + 1.028333\text{E-}07 T^3 + 1167755 T^{-1}$$

Phase Si₃Zr₅

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 685146.78 + 1044.78 T - 187 T \cdot \ln T - 0.0161754 T^2 \\ + 5.22283\text{E-}08 T^3 + 381210 T^{-1}$$

Phase SiZr₂

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 2.0 H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 255317.83 + 411.767 T - 72.43244 T \cdot \ln T - 5.46177\text{E-}03 T^2 \\ - 4.0442633\text{E-}09 T^3 + 306730.45 T^{-1}$$

Phase SiZr₃

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ - 270398.16 + 457.33 T - 82.328 T \cdot \ln T - 0.0263963 T^2 \\ + 1.54326\text{E-}06 T^3 - 34700 T^{-1}$$

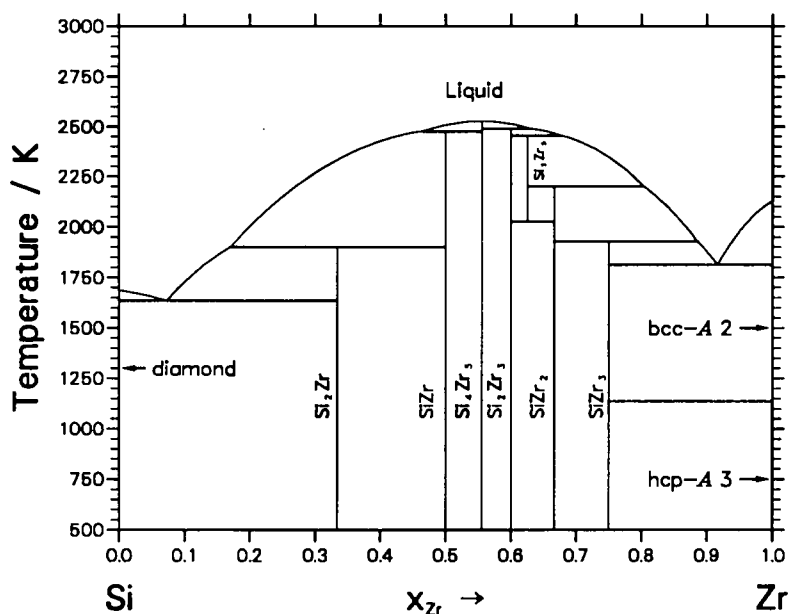


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zr}			T / K
Liquid \rightleftharpoons diamond + Si ₂ Zr	Eutectic	.073	.000	.333	1634.6
Liquid + SiZr \rightleftharpoons Si ₂ Zr	Peritectic	.170	.500	.333	1900.3
Liquid + Si ₄ Zr ₅ \rightleftharpoons SiZr	Peritectic	.463	.555	.500	2477.0
Liquid + Si ₄ Zr ₅ \rightleftharpoons Si ₂ Zr ₃	Peritectic	.629	.555	.600	2491.5
Liquid + Si ₂ Zr ₃ \rightleftharpoons Si ₃ Zr ₅	Peritectic	.677	.600	.675	2455.4
Liquid + Si ₃ Zr ₅ \rightleftharpoons SiZr ₂	Peritectic	.803	.625	.666	2200.0
Liquid + SiZr ₂ \rightleftharpoons SiZr ₃	Peritectic	.886	.666	.750	1927.4
Liquid \rightleftharpoons SiZr ₃ + bcc-A2	Eutectic	.916	.750	1.000	1814.2
hcp-A3 \rightleftharpoons bcc-A2	Allotropic	1.000	1.000	1139.4
Si ₃ Zr ₅ \rightleftharpoons Si ₂ Zr ₃ + SiZr ₂	Eutectoid	.625	.600	.666	2025.2
Liquid \rightleftharpoons Si ₄ Zr ₅	Congruent	.556	.556	2527.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments	
Si-Zr	(Si)	diamond	<i>cF8</i> <i>Fd$\bar{3}m$</i>	M 8		
	(Zr)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2		
	(Zr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 4		
	SiZr- α	BFe	<i>oP8</i>	Si 4		transformation not considered
	SiZr- β	BCr	<i>oC8</i> <i>Cmcm</i>	Zr 4		
	SiZr ₂	Al ₂ Cu	<i>tI12</i> <i>I4/mcm</i>	Si 8 Zr 4		
	SiZr ₃	PTi ₃	<i>tP32</i> <i>P4$_2$/n</i>			
	Si ₂ Zr	Si ₂ Zr	<i>oC12</i> <i>Cmcm</i>	Si ₁ 4 Si ₂ 4 Zr 4		
	Si ₂ Zr ₃	Si ₂ U ₃	<i>tP10</i> <i>P4/mbm</i>			
	Si ₃ Zr ₅	Mn ₅ Si ₃	<i>hP16</i> <i>P6$_3$/mcm</i>	Si 6 Zr ₁ 4 Zr ₂ 6		
	Si ₄ Zr ₅ - α	Si ₄ Zr ₅	<i>tP36</i> <i>P4$_1$2$_1$2</i>	Si ₁ 8 Si ₂ 8 Zr ₁ 4 Zr ₂ 8 Zr ₃ 8		transformation not considered
	Si ₄ Zr ₅ - β	Si ₄ Zr ₅				

System Sn–Ti

Solution Phases:

Liquid, bcc–A2, hcp–A3, bct–A5

Compounds:

Sn₅Ti₆, Sn₃Ti₅, SnTi₂, SnTi₃

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc–A2	:	Substitutional, Redlich–Kister
bct–A5	:	Substitutional, Redlich–Kister
hcp–A3	:	Substitutional, Redlich–Kister
SnTi ₃	:	Sublattice model: (Sn,Ti)(Sn,Ti) ₃
Sn ₅ Ti ₆	:	Stoichiometric, (Sn) ₅ (Ti) ₆
Sn ₃ Ti ₅	:	Stoichiometric, (Sn) ₃ (Ti) ₅
SnTi ₂	:	Stoichiometric, (Sn)(Ti) ₂

Assessor and Date:

F. Hayes, 1992

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc–A2

$$L_{\text{Sn,Ti};\square}^{0,\text{bcc-A2}} = -115000.00 + 6.77583 T$$

$$L_{\text{Sn,Ti};\square}^{1,\text{bcc-A2}} = 45000.00 + 1.58018 T$$

Phase bct–A5

$$L_{\text{Sn,Ti}}^{0,\text{bct-A5}} = 50000.0$$

Phase hcp–A3

$$L_{\text{Sn,Ti};\square}^{0,\text{hcp-A3}} = -111502.08 + 1.8068 T$$

$$L_{\text{Sn,Ti};\square}^{1,\text{hcp-A3}} = 43871.41 + 2.08175 T$$

Phase liquid

$$L_{\text{Sn,Ti}}^{0,\text{liquid}} = -90206.13 - 5.55089 T$$

$$L_{\text{Sn,Ti}}^{1,\text{liquid}} = 44395.59 - 6.09746 T$$

Phase SnTi₃

$$G^\circ(T) - 4.0 H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) = G(\text{Sn:Sn}) = 4.0 \text{ GHSE}_{\text{Sn}}$$

$$G^\circ(T) - H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Sn:Ti}) = -193466.8 + 35.74052 T + \text{GLIQ}_{\text{Sn}} + 3.0 \text{ GLIQ}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Sn}) = 300000 - 200 T + 3.0 \text{ GLIQ}_{\text{Sn}} + \text{GLIQ}_{\text{Ti}}$$

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 4.0 \text{ GHSE}_{\text{Ti}}$$

$$L_{\text{Sn:Sn,Ti}}^{0,\text{SnTi}_3} = 400000 - 40.0 T$$

$$L_{\text{Ti:Sn,Ti}}^{0,\text{SnTi}_3} = 600000 + 40.0 T$$

$$L_{\text{Sn,Ti:Sn}}^{0,\text{SnTi}_3} = 400000$$

$$L_{\text{Sn,Ti:Ti}}^{0,\text{SnTi}_3} = 200000 - 108.000 T$$

Phase SnTi₂

$$G^\circ(T) - H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = -152700.00 + 26.80539 T + \text{GLIQ}_{\text{Sn}} + 2.0 \text{ GLIQ}_{\text{Ti}}$$

Phase Sn₃Ti₅

$$G^\circ(T) - 3.0 H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - 5.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = -398000.00 + 64.8 T + 3.0 \text{ GLIQ}_{\text{Sn}} + 5.0 \text{ GLIQ}_{\text{Ti}}$$

Phase Sn₅Ti₆

$$G^\circ(T) - 5.0 H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - 6.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = -525800.00 + 77.0 T + 5.0 \text{ GLIQ}_{\text{Sn}} + 6.0 \text{ GLIQ}_{\text{Ti}}$$

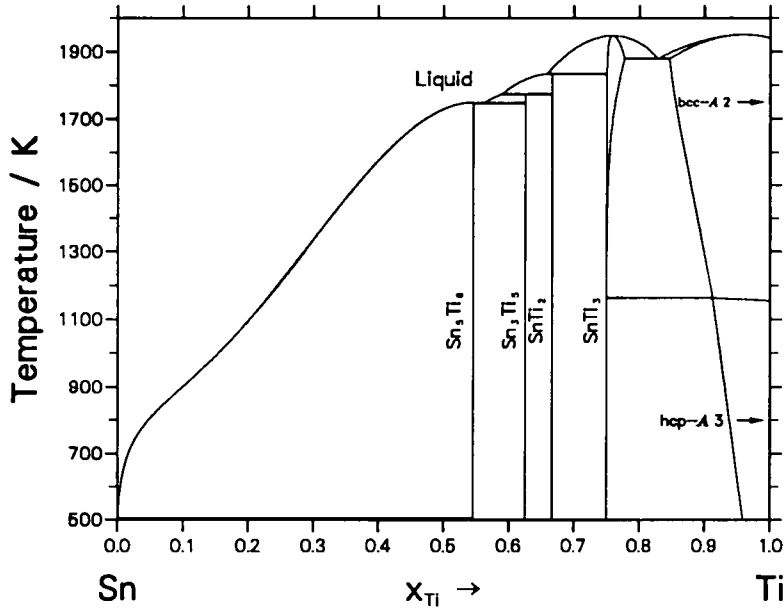


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Ti}	T / K
$bcc-A2 + SnTi_3 \rightleftharpoons hcp-A3$	Peritectic	.913 .750 .912	1163.3
$Liquid \rightleftharpoons SnTi_3 + bcc-A2$	Eutectic	.828 .777 .846	1879.8
$SnTi_3 \rightleftharpoons Liquid$	Congruent	.750 .750	1947.0
$Liquid + SnTi_3 \rightleftharpoons SnTi_2$	Peritectic	.659 .750 .667	1835.9
$Liquid + SnTi_2 \rightleftharpoons Sn_3Ti_5$	Peritectic	.589 .667 .625	1774.7
$Liquid \rightleftharpoons Sn_5Ti_6 + Sn_3Ti_5$	Eutectic	.561 .545 .625	1746.9
$Sn_5Ti_6 \rightleftharpoons Liquid$	Congruent	.545 .545	1750.0
$Liquid \rightleftharpoons bct-A5 + Sn_5Ti_6$	Degenerate	.001 .000 .545	504.8

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Sn-Ti	(Sn)	β -Sn	<i>tI4</i> <i>I4₁/amd</i>	M 2	transformation not considered
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	Sn ₅ Ti ₆ - α	Nb ₆ Sn ₅	<i>oI44</i> <i>Immm3</i>		
	Sn ₅ Ti ₆ - β	<i>hP22</i> <i>P6₃/mmc</i>	Sn 3 Ti 6	
	Sn ₃ Ti ₅	Mn ₅ Si ₃	<i>hP16</i> <i>P6₃/mcm</i>	Sn 6 Ti 4	
	SnTi ₂	InNi ₂	<i>hP6</i> <i>P6₃/mmc</i>		
	SnTi ₃	Ni ₃ Sn	<i>hP8</i> <i>P6₃/mmc</i>	Sn 2 Ti 6 Si ₁ 4 Si ₂ 8	

System Sn–Zn

Solution Phases:

(stable) Liquid, bct–A5, hcp–Zn
 (metastable) bcc–A2

Modelling:

Liquid : Substitutional, Redlich–Kister
 bcc–A2 : Substitutional, Redlich–Kister
 bct–A5 : Substitutional, Redlich–Kister
 hcp–Zn : Substitutional, Redlich–Kister

Assessor and Date:

S. Fries, and H.L. Lukas

Publication:

"Cost507 New Light Alloys", Leuven Proceedings,
 Ed. G. Effenberg (1991)

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bct–A5

$$L_{\text{Sn,Zn};\square}^{0,\text{bct-A5}} = 6514.76 + 25.70957 T$$

Phase bcc–A2

$$L_{\text{Sn,Zn};\square}^{0,\text{bcc-A2}} = 6514.76 + 25.70957 T$$

Phase hcp–Zn

$$L_{\text{Sn,Zn};\square}^{0,\text{hcp-Zn}} = 33433.94 - 11.14466 T$$

Phase liquid

$$L_{\text{Sn,Zn}}^{0,\text{liquid}} = 19314.64 - 75.89939 T + 8.751396 T \cdot \ln T$$

$$L_{\text{Sn,Zn}}^{1,\text{liquid}} = -5696.28 + 4.20198 T$$

$$L_{\text{Sn,Zn}}^{2,\text{liquid}} = 1037.22 + 0.98362 T$$

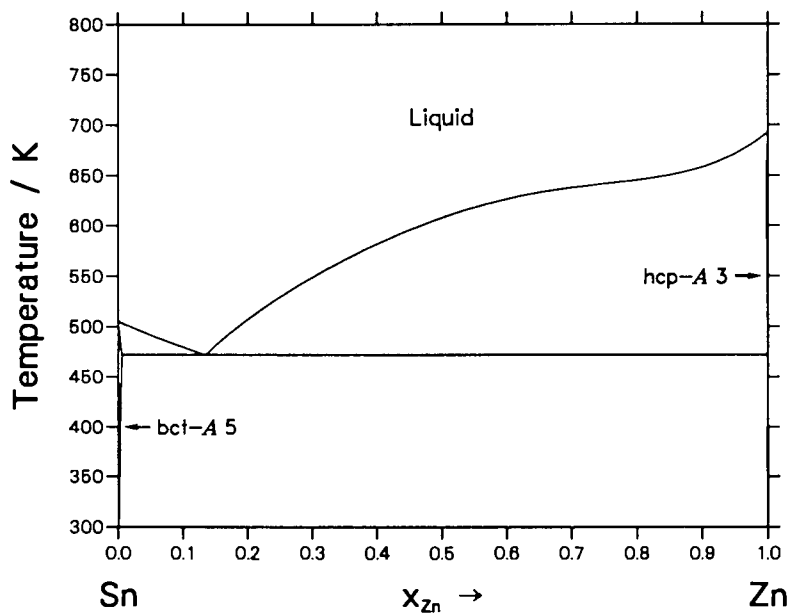


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Zn}	T / K
Liquid \rightleftharpoons bct-A5 + hcp-Zn	Eutectic	0.135 .006 1.000	471.7

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Sn-Zn	(Sn)	β -Sn	tI_4 $I4_1/amd$
	(Zn)	Mg	$hP2$ $P6_3/mmc$

System Sn – Zr

Solution Phases

Liquid, bcc-A2, bct-A5, hcp-A3

Compounds:

SnZr₄, Sn₃Zr₅, Sn₂Zr

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
SnZr ₄	:	Stoichiometric, (Sn)(Zr) ₄
Sn ₃ Zr ₅	:	Stoichiometric, (Sn) ₃ (Zr) ₅
Sn ₂ Zr	:	Stoichiometric, (Sn) ₂ (Zr)

Assessor and date:

J. Korb, and K. Hack, GTT, Germany (1996).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase liquid

$$L_{\text{Sn,Zr}}^{0,\text{liquid}} = -45520 - 95.46 T$$

$$L_{\text{Sn,Zr}}^{1,\text{Liquid}} = -80000 + 82.115 T$$

$$L_{\text{Sn,Zr}}^{2,\text{Liquid}} = -120000 + 80.0273 T$$

Phase bcc-A2

$$L_{\text{Sn,Zr}:\square}^{0,\text{bcc-A2}} = -101200 - 71.13 T$$

$$L_{\text{Sn,Zr}:\square}^{1,\text{bcc-A2}} = 55000$$

$$L_{\text{Sn,Zr}:\square}^{2,\text{bcc-A2}} = 26102.3$$

Phase hcp-A3

$$L_{\text{Sn,Zr};\square}^{0,\text{hcp-A3}} = -160000 - 31 T$$

$$L_{\text{Sn,Zr};\square}^{1,\text{hcp-A3}} = 151800$$

$$L_{\text{Sn,Zr};\square}^{2,\text{hcp-A3}} = 129900$$

Phase SnZr₄

$$G^\circ(T) - H_{\text{Sn}}^{\circ,\text{bcc-A5}}(298.15 \text{ K}) - 4.0 H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ -270456.8 + 602.125 T - 123.0 T \cdot \ln T - 0.00883 T^2$$

Phase Sn₃Zr₅

$$G^\circ(T) - 3.0 H_{\text{Sn}}^{\circ,\text{bcc-A5}}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ -769380 + 1131.86 T - 217.118 T \cdot \ln T - 0.02404 T^2 \\ + 1648000 T^{-1}$$

Phase Sn₂Zr

$$G^\circ(T) - 2.0 H_{\text{Sn}}^{\circ,\text{bcc-A5}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = \\ -267104.8 + 492.1 T - 86.404 T \cdot \ln T - 0.002226 T^2 \\ + 618000 T^{-1}$$

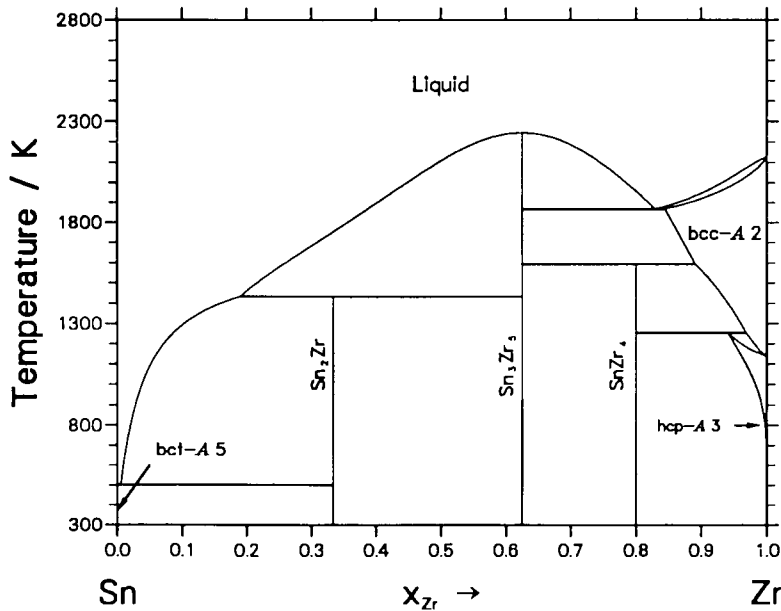


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{Zr}			T / K
Liquid \rightleftharpoons bcc-A2 + Sn ₃ Zr ₅	Eutectic	.892	.844	.625	1868.5
bcc-A2 + Sn ₃ Zr ₅ \rightleftharpoons SnZr ₄	Peritectoid	.891	.625	.800	1595.5
bcc-A2 + SnZr ₄ \rightleftharpoons hcp-A3	Peritectoid	.968	.800	.941	1254.0
Liquid + Sn ₃ Zr ₅ \rightleftharpoons Sn ₂ Zr	Peritectoid	.189	.625	.333	1433.3
Liquid \rightleftharpoons Sn ₂ Zr + bct-A5	Eutectic	.0056	.333	.000	502.0
Liquid \rightleftharpoons Sn ₃ Zr ₅	Congruent	.625	.625	2245.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Sn-Zr	(Sn)	β -Sn	<i>tI4</i> <i>I4₁/amd</i>	M 2
	(Zr)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2
	(Zr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2
	SnZr ₄	Cr ₃ Si	<i>cP8</i> <i>Pm$\bar{3}n$</i>	
	Sn ₃ Zr ₅	Mn ₅ Si ₃	<i>hP16</i> <i>P6₃/mcm</i>	
	Sn ₂ Zr	SiTi ₂	<i>oF24</i> <i>Fddd</i>	

System Ta-Ti

Solution Phases:

(stable) Liquid, bcc-A2, hcp-A3
 (metastable) bcc-B2, fcc-A1

Compounds:

(metastable) AlM-D0₁₉, AlM-D0₂₂, AlTi-L1₀

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : see below
 bcc-B2 : Sublattice model, (Ta,Ti)_{0.5}(Ta,Ti)_{0.5}(□)₃
 : The thermodynamic description of the bcc-B2 takes
 : into account the ordering reaction bcc-A2 ⇌ bcc-B2.
 : Two descriptions are given: one using equations
 : 23 and 27, the other using equations 23 and 28.
 : For the latter, the parameters are given in a frame.
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 AlM-D0₁₉ : Sublattice model, (Ta,Ti)(Ta,Ti)₃
 AlM-D0₂₂ : Sublattice model, (Ti)₃(Ta,Ti)
 AlTi-L1₀ : Sublattice model, (Ta,Ti)(Ta,Ti)
 :

Assessor and Date:

N. Saunders, 1997.

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase fcc-A1

$$L_{\text{Ta,Ti};\square}^{0,\text{fcc-A1}} = 8500$$

Phase hcp-A3

$$L_{\text{Ta,Ti};\square}^{0,\text{hcp-A3}} = 8500$$

Phase liquid

$$L_{\text{Ta,Ti}}^{0,\text{liquid}} = 1000$$

$$L_{\text{Ta,Ti}}^{1,\text{liquid}} = -7000$$

Phase AIM-D0₁₉

$$G^\circ(T) - 4.0 H_{\text{Ta}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ta:Ta}) = 4.0 \text{ GHCP}_{\text{Ta}}$$

$$G^\circ(T) - 3.0 H_{\text{Ta}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ta:Ti}) =$$

$$6376 + 3.0 \text{ GHCP}_{\text{Ta}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ta}) =$$

$$6376 + \text{GHCP}_{\text{Ta}} + 3.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 4.0 + 4.0 \text{ GHSER}_{\text{Ti}}$$

$$L_{\text{Ta,Ti:Ta}}^{0,\text{AIM-D0}_{19}} = L_{\text{Ta,Ti:Ti}}^{0,\text{AIM-D0}_{19}} = 19128$$

$$L_{\text{Ta:Ta,Ti}}^{0,\text{AIM-D0}_{19}} = L_{\text{Ti:Ta,Ti}}^{0,\text{AIM-D0}_{19}} = 2128$$

Phase AIM-D0₂₂

$$G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ta}) =$$

$$\text{GFCC}_{\text{Ta}} + 3.0 \text{ GFCC}_{\text{Ti}}$$

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 4.0 \text{ GFCC}_{\text{Ti}}$$

Phase AlTi-L1₀

$$G^\circ(T) - 2.0 H_{\text{Ta}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ta:Ta}) = 2.0 \text{ GFCC}_{\text{Ta}}$$

$$G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ta:Ti}) =$$

$$4250 + \text{GFCC}_{\text{Ta}} + \text{GFCC}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ta}) =$$

$$4250 + \text{GFCC}_{\text{Ta}} + \text{GFCC}_{\text{Ti}}$$

$$G^\circ(T) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 2.0 \text{ GFCC}_{\text{Ti}}$$

$$L_{\text{Ta,Ti:Ta}}^{0,\text{AlTi-L1}_0} = L_{\text{Ta:Ta,Ti}}^{0,\text{AlTi-L1}_0} = 4250$$

$$L_{\text{Ta,Ti:Ti}}^{0,\text{AlTi-L1}_0} = L_{\text{Ti:Ta,Ti}}^{0,\text{AlTi-L1}_0} = 4250$$

Phase bcc-A2

$$L_{\text{Ta,Ti:}\square}^{0,\text{bcc-A2}} = 12000$$

$$L_{\text{Ta,Ti:}\square}^{1,\text{bcc-A2}} = -2500$$

Phase bcc-B2

$$G_{\text{Ti:Ta:}\square}^* = -2500$$

$$G^\circ(T) - H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ta:Ta:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ta:Ti:}\square) = G_{\text{Ta:Ti:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ta:Ti:}\square) = G_{\text{Ti:Ta:}\square}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

$$L_{\text{Ta,Ti:Ta:}\square}^{0, \text{bcc-B2}} = L_{\text{Ta,Ti:Ti:}\square}^{0, \text{bcc-B2}} = -G_{\text{Ti:Ta:}\square}^*$$

$$L_{\text{Ta:Ta,Ti:}\square}^{0, \text{bcc-B2}} = L_{\text{Ti:Ta,Ti:}\square}^{0, \text{bcc-B2}} = -G_{\text{Ti:Ta:}\square}^*$$

Phase bcc-B2

$$G_{\text{Ti:Ta:}\square}^* = 2500$$

$$G^\circ(T) - H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Ta:Ta:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ta:Ti:}\square) = 2.0 G_{\text{Ti:Ta:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ta:}\square) = 2.0 G_{\text{Ti:Ta:}\square}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Ta,Ti:}\square}^{0, \text{bcc-A2}} = 12000$$

$$L_{\text{Ta,Ti:}\square}^{1, \text{bcc-A2}} = -2500$$

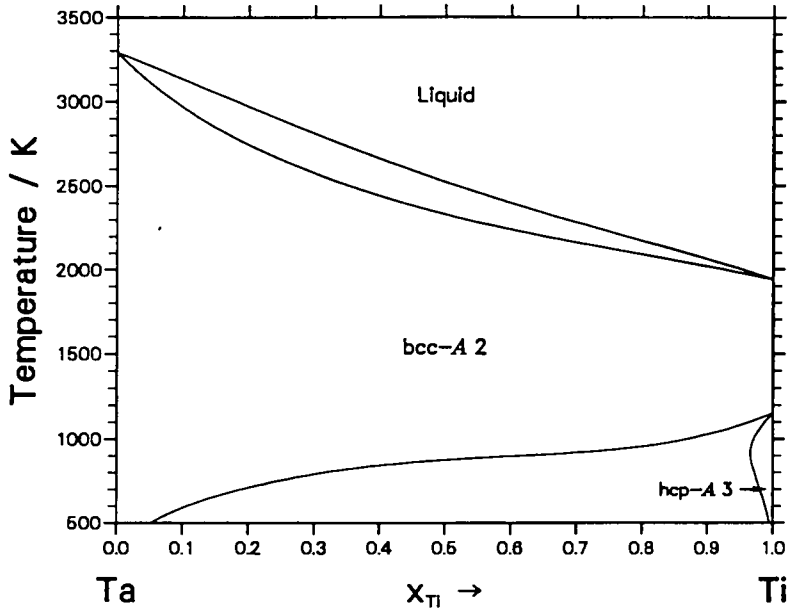


Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Ta-Ti	(V)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>

System Ti-V

Solution Phases:

Liquid, bcc-A2, hcp-A3

Modelling:

Liquid : Substitutional, Redlich-Kister
bcc-A2 : Substitutional, Redlich-Kister
hcp-A3 : Substitutional, Redlich-Kister
:

Assessor and Date:

N. Saunders (1990)

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Ti,V};\square}^{0,\text{bcc-A2}} = 10500 - 1.5 T$$

$$L_{\text{Ti,V};\square}^{1,\text{bcc-A2}} = 2000$$

$$L_{\text{Ti,V};\square}^{2,\text{bcc-A2}} = 1000$$

Phase hcp-A3

$$L_{\text{Ti,V};\square}^{0,\text{hcp-A3}} = 20000$$

Phase liquid

$$L_{\text{Ti,V}}^{0,\text{liquid}} = 1400$$

$$L_{\text{Ti,V}}^{1,\text{liquid}} = 4100$$

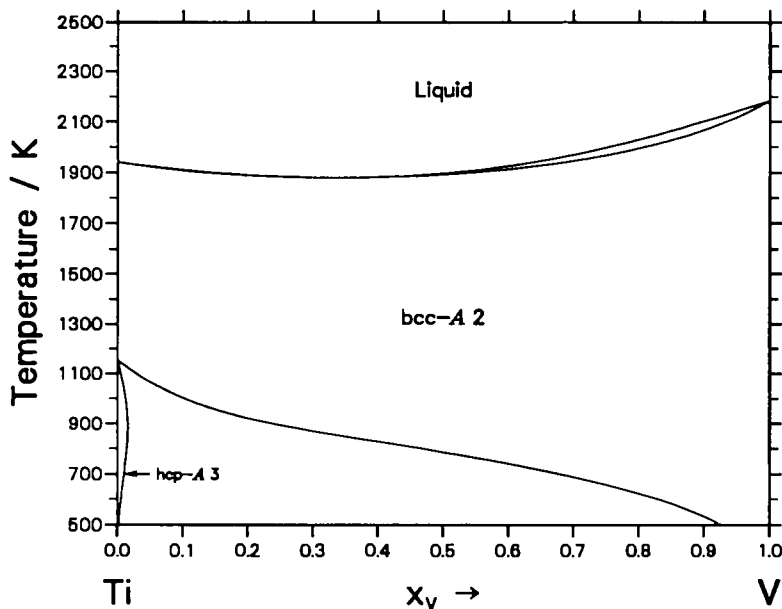


Table I – Invariant Reactions.

Reaction	Type	Compositions x_V	T / K
$\text{bcc-A2} \rightleftharpoons \text{Liquid}$	Congruent	0.333 0.333	1881.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Ti-V	(Ti)	Mg	$hP2$ $P6_3/mmc$
	(Ti)	W	$cI2$ $Im\bar{3}m$
	(V)	W	$cI2$ $Im\bar{3}m$

System Ti-W

Solution Phases:

(stable) : Liquid, bcc-A2, hcp-A3
 (metastable) : bcc-B2, fcc-A1

Compounds:

(metastable) : AlM-D0₁₉, AlTi-L1₀

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : see above
 bcc-B2 : Sublattice model, (Ti,W)_{0.5}(Ti,W)_{0.5}(□)₃
 The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 ⇌ bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 AlM-D0₁₉ : Sublattice model, (Ti,W)(Ti,W)₃
 AlTi-L1₀ : Sublattice model, (Ti,W)(Ti,W)
 :

Assessor and Date:

N. Saunders, 1997.

Thermodynamic properties of the solution phases (J.mol⁻¹)

Phase fcc-A1

$$L_{\text{Ti,W};\square}^{0,\text{fcc-A1}} = 33825$$

Phase hcp-A3

$$L_{\text{Ti,W};\square}^{0,\text{hcp-A3}} = 35774$$

Phase liquid

$$L_{\text{Ti,W}}^{0,\text{liquid}} = 28392$$

$$L_{\text{Ti,W}}^{1,\text{liquid}} = -4282$$

Phase AlM-D0₁₉

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 4.0 + 4.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{Ti:W}) = 26832 + 3.0 \text{ GHCP}_{\text{W}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) - 3.0 H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{W:Ti}) = 26832 + \text{GHCP}_{\text{W}} + 3.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 4.0 H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{W:W}) = 4.0 \text{ GHCP}_{\text{W}}$$

$$L_{\text{Ti,W:Ti}}^{0,\text{AlM-D}0_{19}} = L_{\text{Ti,W:W}}^{0,\text{AlM-D}0_{19}} = 80492$$

$$L_{\text{Ti:Ti,W}}^{0,\text{AlM-D}0_{19}} = L_{\text{W:Ti,W}}^{0,\text{AlM-D}0_{19}} = 8944$$

Phase AlTi-L1₀

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 2.0 \text{ GFCC}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{Ti:W}) = 4250 + \text{GFCC}_{\text{Ti}} + \text{GFCC}_{\text{W}}$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{W:Ti}) = 4250 + \text{GFCC}_{\text{Ti}} + \text{GFCC}_{\text{W}}$$

$$G^\circ(T) - 2.0 H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{W:W}) = 2.0 \text{ GFCC}_{\text{W}}$$

$$L_{\text{Ti,W:Ti}}^{0,\text{AlTi-L}1_0} = L_{\text{Ti:Ti,W}}^{0,\text{AlTi-L}1_0} = 16914$$

$$L_{\text{Ti,W:W}}^{0,\text{AlTi-L}1_0} = L_{\text{W:Ti,W}}^{0,\text{AlTi-L}1_0} = 16914$$

Phase bcc-A2

$$L_{\text{Ti,W:}\square}^{0,\text{bcc-A}2} = 3957 + 13.033 T$$

$$L_{\text{Ti,W:}\square}^{1,\text{bcc-A}2} = 10640 - 4.464 T$$

Phase bcc-B2

$$G_{\text{Ti,W:}\square}^* = 0$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) - 0.5 H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{Ti:W:}\square) = G_{\text{Ti,W:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15 \text{ K}) - 0.5 H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{W:Ti:}\square) = G_{\text{Ti,W:}\square}^*$$

$$G^\circ(T) - H_{\text{W}}^{\circ,\text{bcc-A}2}(298.15 \text{ K}) = G(\text{W:W:}\square) = 0.0$$

$$L_{\text{Ti,W:W:}\square}^{0,\text{bcc-B}2} = L_{\text{Ti,W:Ti:}\square}^{0,\text{bcc-B}2} = -G_{\text{Ti,W:}\square}^*$$

$$L_{\text{W:Ti,W:}\square}^{0,\text{bcc-B}2} = L_{\text{Ti:Ti,W:}\square}^{0,\text{bcc-B}2} = -G_{\text{Ti,W:}\square}^*$$

Phase bcc-B2

$$G_{\text{Ti:W:}\square}^* = 0$$

$$G^\circ(T) - H_{\text{W}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{W:W:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{W}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{W:Ti:}\square) = 2.0 \quad G_{\text{Ti:W:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{W}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:W:}\square) = 2.0 \quad G_{\text{Ti:W:}\square}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

Phase bcc-A2

$$L_{\text{Ti,W:}\square}^{0, \text{bcc-A2}} = 3957 + 13.033 T$$

$$L_{\text{Ti,W:}\square}^{1, \text{bcc-A2}} = 10640 - 4.464 T$$

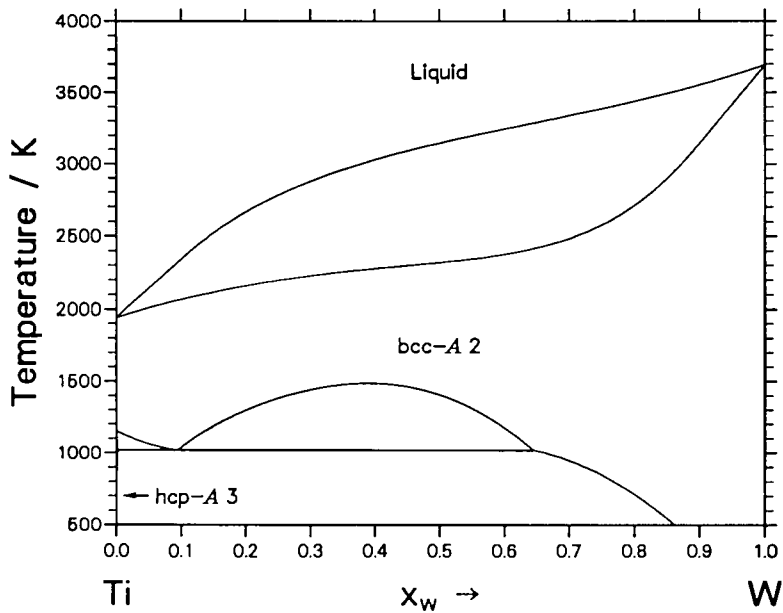


Table I – Invariant Reactions.

Reaction	Type	Compositions x_{W_i}	T / K
hcp-A3 bcc-A2' \rightleftharpoons bcc-A2''	Monotectoid	.002 .645 .095	1019.5

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Ti-W	(V)	W	$cI2$ $Im\bar{3}m$
	(Ti)	Mg	$hP2$ $P6_3/mmc$
	(Ti)	W	$cI2$ $Im\bar{3}m$

System V-Zr

Solution Phases:

Liquid, bcc-A2, hcp-A3

Compound:

V₂Zr

Modelling:

bcc-A2 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister
 Liquid : Substitutional, Redlich-Kister
 V₂Zr : Sublattice model, (V)₂(Zr)

Assessor and Date:

J. Korb, and K. Hack, GTT, Germany (1995).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase V₂Zr

$$G^{\circ}(T) - 2.0 H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = -63100 + 26.83 T + 2.0 \text{ GLIQ}_{\text{V}} + \text{GLIQ}_{\text{Zr}}$$

Phase liquid

$$L_{\text{V,Zr}}^{0, \text{liquid}} = -23986 + 19.338 T$$

$$L_{\text{V,Zr}}^{1, \text{liquid}} = -2058.35 + 3.289 T$$

Phase bcc-A2

$$L_{\text{V,Zr};\square}^{0, \text{bcc-A2}} = 21876 + 7.76081 T$$

$$L_{\text{V,Zr};\square}^{1, \text{bcc-A2}} = 8995.72 - 0.8968 T$$

Phase hcp-A3

$$L_{\text{V,Zr};\square}^{0, \text{hcp-A3}} = 29007 - 7.2944 T$$

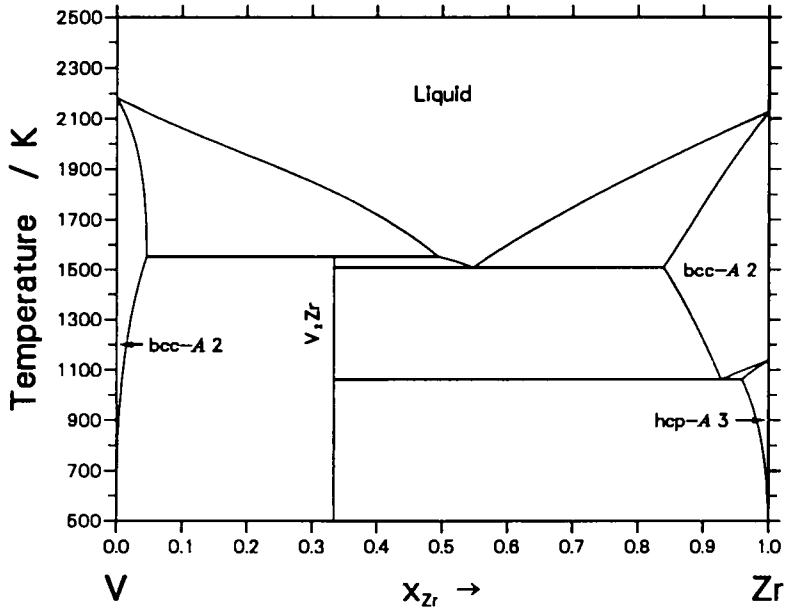


Table I - Invariant Reactions.

Reaction	Type	Compositions x_{Zr}	T / K
$\text{bcc-A2} + \text{Liquid} \rightleftharpoons \text{V}_2\text{Zr}$	Peritectic	.046 .494 .333	1552.7
$\text{Liquid} \rightleftharpoons \text{V}_2\text{Zr} + \text{bcc-A2}$	Eutectic	.548 .333 .839	1510.2
$\text{bcc-A2} \rightleftharpoons \text{V}_2\text{Zr} + \text{hcp-A3}$	Eutectoid	.927 .333 .959	1062.9

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
V-Zr	(V)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	Laves-C15
	(Zr)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Zr)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 4	
	V ₂ Zr	Cu ₂ Mg	<i>cF24</i> <i>Fd$\bar{3}m$</i>	M ₁ 8 M ₂ 16	

TERNARY SYSTEMS

System Al-C-Si

Ternary Solution Phases:

Liquid, fcc-Al

Ternary Compounds:

Al₄SiC₄, Al₈SiC₇

Quasi-binary phase:

(Al,Si)₄C₃

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-Al	:	Substitutional, Redlich-Kister
Al ₄ C ₃	:	Quasi-binary, (Al,Si) ₄ (C) ₃
Al ₄ SiC ₄	:	(Al) ₄ (Si) ₁ (C) ₄
Al ₈ SiC ₇	:	(Al) ₈ (Si) ₁ (C) ₇

Comments:

Liquid and fcc-Al phases assumed to be ideal
Al and Si behave ideally in the Al₄C₃ phase
No ternary compounds

Assessor and Date:

J. Gröbner, H. L. Lukas, and F. Aldinger.

Publication:

Calphad 20, 2 (1996) 247-254.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₄SiC₄

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 4.0 H_{\text{C}}^{\circ, \text{graphite}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = \\ - 380700.0 + 1233 T - 193.902723 T \cdot \ln T - 0.017517573 T^2 \\ + 3240000 T^{-1} + 9\text{E-}07 T^3$$

Phase Al₈SiC₇

$$G^\circ(T) - 8.0 H_{\text{Al}}^{\circ, \text{fcc-Al}}(298.15 \text{ K}) - 7.0 H_{\text{C}}^{\circ, \text{graphite}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = \\ - 686400.0 + 2212.8 T - 344.434112 T \cdot \ln T - 0.04544832 T^2 \\ + 5680000 T^{-1} + 3.2\text{E-}06 T^3$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-C-Si	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4
	(C)	graphite		
	(Si)	diamond	$cF8$ $Fd\bar{3}m$	
	Al_4SiC_4	Al_5C_3N	$hP18$ $P6_3mc$	
	Al_8SiC_7		$hP16$	
	$(Al,Si)_4C_3$	Al_4C_3	$hP7$ $R\bar{3}m$	

System Al-Cu-Li

Ternary Solution Phases:

Liquid, fcc-A1, bcc-A2

Ternary Compounds:

AlCuLi-R, AlCuLi-T1, AlCuLi-T2, AlCuLi-TB

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
AlCuLi-R	:	Stoichiometric, (Al) _{0.55} (Cu) _{0.117} (Li) _{0.333}
AlCuLi-T1	:	Stoichiometric, (Al) _{0.5} (Cu) _{0.25} (Li) _{0.25}
AlCuLi-T2	:	Stoichiometric, (Al) _{0.57} (Cu) _{0.11} (Li) _{0.32}
AlCuLi-TB	:	Stoichiometric, (Al) _{0.60} (Cu) _{0.32} (Li) _{0.08}

Assessor and Date:

N. Saunders, 1994.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlCuLi-R

$$\begin{aligned}
 G^\circ(T) - 0.55 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 0.117 H_{\text{Cu}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) \\
 - 0.333 H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Cu:Li}) = \\
 - 20983.0 + 6.0 T + 0.55 \text{ GHSE}_{\text{Al}} + 0.117 \text{ GHSE}_{\text{Cu}} \\
 + 0.333 \text{ GHSE}_{\text{Li}}
 \end{aligned}$$

Phase AlCuLi-T1

$$\begin{aligned}
 G^\circ(T) - 0.5 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 0.25 H_{\text{Cu}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) \\
 - 0.25 H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = G(\text{Al:Cu:Li}) = \\
 - 24560.0 + 6.0 T + 0.25 \text{ GHSE}_{\text{Al}} + 0.25 \text{ GHSE}_{\text{Cu}} \\
 + 0.25 \text{ GHSE}_{\text{Li}}
 \end{aligned}$$

Phase AlCuLi-T2

$$\begin{aligned}
 G^\circ(T) - 0.57 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.11 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) \\
 - 0.32 H_{\text{Li}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Cu:Li}) = \\
 - 20000.0 + 5.497 T + 0.57 \text{ GHSE}_{\text{Al}} + 0.11 \text{ GHSE}_{\text{Cu}} \\
 + 0.32 \text{ GHSE}_{\text{Li}}
 \end{aligned}$$

Phase AlCuLi-TB

$$\begin{aligned}
 G^\circ(T) - 0.60 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.32 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) \\
 - 0.08 H_{\text{Li}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Cu:Li}) = \\
 - 19918.0 + 4.0 T + 0.60 \text{ GHSE}_{\text{Al}} + 0.32 \text{ GHSE}_{\text{Cu}} \\
 + 0.08 \text{ GHSE}_{\text{Li}}
 \end{aligned}$$

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Cu-Li	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	(Cu)	Cu	<i>cF4</i>	M 4	
	(Li)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M 2	
	Al _{7.5} Cu ₄ Li	CaF ₂	<i>cF12</i> <i>Fm$\bar{3}$m</i>		AlCuLi-TB
	Al ₂ CuLi	Al ₂ CuLi	<i>hP12</i> <i>P6/mmm</i>		AlCuLi-T1
	Al ₆ CuLi ₃				AlCuLi-T2 quasicrystal
	Al ₅ CuLi ₃	Mg ₂₃ (Zn, Al) ₄₉	<i>cI162</i> <i>Im$\bar{3}$</i>		AlCuLi-TR

System Al-Cu-Mg

Ternary Solution Phases:

Liquid, fcc-A1, hcp-A3

Ternary Compounds:

Laves-C14, Laves-C15, Laves-C36, Q-Phase, S-Phase, τ , V-Phase

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Laves-C14	:	Sublattice model, (Al,Cu,Mg)(Al,CuMg) ₂
Laves-C15	:	Sublattice model, (Al,Cu,Mg)(Al,Cu,Mg) ₂
Laves-C36	:	Sublattice model, (Al,Cu,Mg)(Al,Cu,Mg) ₂
τ	:	Sublattice model, (Mg) ₂₆ (Al, Mg) ₆ (Al,Cu,Mg) ₄₈ (Al)
Q-Phase	:	Stoichiometric, (Al) ₇ (Cu) ₃ (Mg) ₆
S-Phase	:	Stoichiometric, (Al) ₂ (Cu)(Mg)
V-Phase	:	Stoichiometric, (Al) ₅ (Cu) ₆ (Mg) ₂

Assessor and Date:

T. Bühler, RWTH, Germany, (1997).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Q-Phase

$$\begin{aligned}
 G^\circ(T) - 7.0 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 3.0 H_{\text{Cu}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) \\
 - 6.0 H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al}:\text{Cu}:\text{Mg}) = \\
 - 221500 + 18.46 T + 7.0 \text{ GHSE}_{\text{Al}} + 3.0 \text{ GHSE}_{\text{Cu}} \\
 + 6.0 \text{ GHSE}_{\text{Mg}}
 \end{aligned}$$

Phase Laves-C14

$$L_{\text{Cu,Mg:Al}}^{0,\text{Laves-C14}} = 13011.35$$

$$L_{\text{Cu:Al,Mg}}^{0,\text{Laves-C14}} = 8000$$

$$L_{\text{Al,Mg:Cu}}^{0,\text{Laves-C14}} = 15000$$

$$L_{\text{Al:Cu,Mg}}^{0,\text{Laves-C14}} = 6599.45$$

$$L_{\text{Al,Cu:Mg}}^{0,\text{Laves-C14}} = -224000 + 2.44 T$$

Phase Laves-C15

$$L_{\text{Cu,Mg:Al}}^{0,\text{Laves-C15}} = 13011.35$$

$$L_{\text{Cu:Al,Mg}}^{0,\text{Laves-C15}} = 8000$$

$$L_{\text{Al,Mg:Cu}}^{0,\text{Laves-C15}} = 15000$$

$$L_{\text{Al:Cu,Mg}}^{0,\text{Laves-C15}} = 6599.45$$

$$L_{\text{Al,Cu:Mg}}^{0,\text{Laves-C15}} = -180000 - 1.615 T$$

Phase Laves-C36

$$L_{\text{Cu,Mg:Al}}^{0,\text{Laves-C36}} = 13011.35$$

$$L_{\text{Cu:Al,Mg}}^{0,\text{Laves-C36}} = 8000$$

$$L_{\text{Al,Mg:Cu}}^{0,\text{Laves-C36}} = 15000$$

$$L_{\text{Al:Cu,Mg}}^{0,\text{Laves-C36}} = 6599.45$$

$$L_{\text{Al,Cu:Mg}}^{0,\text{Laves-C36}} = -227442 + 14.61 T$$

Phase S-Phase

$$\begin{aligned} G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) \\ - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al:Cu:Mg}) = \\ - 63200 + 4.13 T + 2.0 \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Mg}} \end{aligned}$$

Phase V-Phase

$$\begin{aligned}
 G^\circ(T) - 5.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}1}(298.15 \text{ K}) - 6.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}1}(298.15 \text{ K}) \\
 - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-\text{Al}3}(298.15 \text{ K}) = G(\text{Al}:\text{Cu}:\text{Mg}) = \\
 - 274527.45 + 13.0 T + 5.0 \text{ GHSER}_{\text{Al}} + 6.0 \text{ GHSER}_{\text{Cu}} + 2.0 \\
 \text{GHSER}_{\text{Mg}}
 \end{aligned}$$

Phase τ

$$\begin{aligned}
 G^\circ(T) - 7.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}1}(298.15 \text{ K}) - 48.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}1}(298.15 \text{ K}) \\
 - 26.0 H_{\text{Mg}}^{\circ,\text{hcp}-\text{Al}3}(298.15 \text{ K}) = G(\text{Mg}:\text{Al}:\text{Cu}:\text{Al}) = \\
 - 23000 + 440 T + 7.0 \text{ GHSER}_{\text{Al}} + 48.0 \text{ GHSER}_{\text{Cu}} \\
 + 26.0 \text{ GHSER}_{\text{Mg}}
 \end{aligned}$$

$$\begin{aligned}
 G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}1}(298.15 \text{ K}) - 48.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{Al}1}(298.15 \text{ K}) \\
 - 32.0 H_{\text{Mg}}^{\circ,\text{hcp}-\text{Al}3}(298.15 \text{ K}) = G(\text{Mg}:\text{Mg}:\text{Cu}:\text{Al}) = \\
 - 220000 + 440 T + \text{GHSER}_{\text{Al}} + 48.0 \text{ GHSER}_{\text{Cu}} \\
 + 32.0 \text{ GHSER}_{\text{Mg}}
 \end{aligned}$$

$$L_{\text{Mg}:\text{Al}:\text{Al},\text{Cu}:\text{Al}}^{0,\tau} = - 4649190 + 2261.86 T$$

$$L_{\text{Mg}:\text{Mg}:\text{Al},\text{Cu}:\text{Al}}^{0,\tau} = - 4649190 + 2261.86 T$$

$$L_{\text{Mg}:\text{Mg}:\text{Cu},\text{Mg}:\text{Al}}^{0,\tau} = - 220000$$

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Cu-Mg	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Cu)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	Laves-C14	MgZn ₂	<i>hP12</i> <i>P6₃/mmc</i>	Cu 2 Cu 6 Mg 4	
	Laves-C15	Cu ₂ Mg	<i>cF24</i> <i>Fd$\bar{3}m$</i>	Mg ₁ 8 Cu ₂ 16	
	Laves-C36	MgNi ₂	<i>hP24</i> <i>P6₃/mmc</i>	Cu ₁ 6 Cu ₂ 6 Mg ₁ 3 Mg ₂ 3	
	Al ₁₁ Cu ₁₁ Mg ₄	Mg ₂ Zn ₁₁	<i>cP39</i> <i>Pm$\bar{3}$</i>		V-phase
	Al ₇ Cu ₃ Mg ₆		<i>cI96</i> <i>Pm$\bar{3}$</i>		Q-phase
	Al ₂ CuMg	BRe ₃	<i>oC16</i> <i>Cmcm</i>	Cu 4 Mg 4 Al 8	S-phase
	(Al _x Cu _{1-x}) ₄₉ Mg ₃₂	Mg ₃₂ (Al,Zn) ₄₉	<i>cI163</i>	Al ₁ 1 Cu ₁ 1 Mg 6 Al ₂ 6 Al ₃ 8 Cu ₂ 12	

System Al-Cu-Si

Ternary Solution Phases:

Liquid, fcc-A1, bcc-A2, hcp-A3

Modelling:

Liquid : Substitutional, Redlich-Kister
 bcc-A2 : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister

Assessor and Date:

T. Bühler, RWTH, Aachen, Germany, (1997).

Comments:

No coefficients for the ternary solution phases.
 No ternary compounds.

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-Cu-Mg	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4
	(Cu)	Cu	$cF4$ $Fm\bar{3}m$	M 4
	(Si)	diamond	$cF8$ $Fd\bar{3}m$	M 8

System Al–Fe–Mn

Ternary Solution Phases:

Liquid, fcc–Al, Al₈Mn₅–D8₁₀

Quasi-binary phases:

Al₁₃Fe₄, Al₂Fe, Al₅Fe₂, Al₆Mn, Al₄Mn, Al₁₂Mn

Modelling:

Liquid	:	Substitutional, Redlich–Kister
Al ₅ Fe ₄	:	Substitutional, Redlich–Kister
fcc–Al	:	Substitutional, Redlich–Kister
Al ₈ Mn ₅ –D8 ₁₀	:	Sublattice model, (Al) ₁₂ (Mn) ₄ (Al,Fe,Mn) ₁₀
Al ₂ Fe	:	Quasi–binary, (Al) ₂ (Fe,Mn)
Al ₅ Fe ₂	:	Quasi–binary, (Al) ₅ (Fe,Mn) ₂
Al ₁₃ Fe ₄	:	Quasi–binary, (Al) _{.6275} (Fe,Mn) _{.235} (Al,□) _{.1375}
Al ₄ Mn	:	Quasi–binary, (Al) ₄ (Fe,Mn)
Al ₆ Mn	:	Quasi–binary, (Al) ₆ (Fe,Mn)
Al ₁₂ Mn	:	Quasi–binary, (Al) ₁₂ Mn

Comments:

The data below are valid in the composition range $x_{\text{Mn}} < 0.25$ (wt%Mn < 40.0) and

$x_{\text{Fe}} < 0.25$ (wt%Fe < 40.0)

No ternary interaction coefficients for the liquid phase. Interactions between Fe and Mn in Al₁₂Mn, Al₂Fe and Al₅Fe₂ assumed to be ideal.

Assessor and Date:

Å. Jansson, and T.G. Chart (August 1997)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase fcc–Al

$L_{\text{Al,Fe,Mn:}\square}^{0,\text{fcc-Al}}$	=	0.000
	=	
$L_{\text{Al,Fe,Mn:}\square}^{1,\text{fcc-Al}}$	=	- 63652
	=	
$L_{\text{Al,Fe,Mn:}\square}^{2,\text{fcc-Al}}$	=	- 26753

Phase $\text{Al}_{13}\text{Fe}_4$

$$L_{\text{Al:Fe,Mn:Al}}^{0,\text{Al}_{13}\text{Fe}_4} = -11987 + 6 T$$

=

$$L_{\text{Al:Fe,Mn:}\square}^{0,\text{Al}_{13}\text{Fe}_4} = -11987 + 6 T$$

Phase Al_4Mn

$$L_{\text{Al:Fe,Mn}}^{0,\text{Al}_4\text{Mn}} = -10000$$

Phase Al_6Mn

$$L_{\text{Al:Fe,Mn}}^{0,\text{Al}_6\text{Mn}} = -32753 + 21 T$$

Phase $\text{Al}_8\text{Mn}_5\text{-D8}_{10}$

$$G^\circ(T) - 12.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 10.0 H_{\text{Fe}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) - 4.0 H_{\text{Mn}}^{\circ,\text{cbcc-A12,para}}(298.15 \text{ K}) = -632544.85 + 12.0 \text{ GHSER}_{\text{Al}} + 10.0 \text{ GHSER}_{\text{Fe}} + 4.0 \text{ GHSER}_{\text{Mn}}$$

$$L_{\text{Al:Mn:Al,Fe}}^{0,\text{Al}_8\text{Mn}_5\text{-D8}_{10}} = -457832.778$$

$$L_{\text{Al:Mn:Fe,Mn}}^{0,\text{Al}_8\text{Mn}_5\text{-D8}_{10}} = -11169.158$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Fe-Mn	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Fe)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Fe)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	α -Mn	α -Mn	<i>c58</i> <i>I43m</i>		bcc-A1
	β -Mn	β -Mn	<i>cP20</i> <i>P4$_1$32</i>		cub-A13
	AlFe	CsCl	<i>cP2</i> <i>Pm$\bar{3}m$</i>	M ₁ 1 M ₂ 1	
	AlFe ₃	BiF ₃	<i>cF16</i> <i>Fm$\bar{3}m$</i>	Al 4 Fe ₁ 4 Fe ₂ 8	not considered
	Al ₂ Fe	Al ₂ Fe	<i>aP18</i> <i>P1</i>		
	Al ₃ Fe		<i>mC102</i> <i>C2/m</i>		designated by Al ₁₃ Fe ₄
	Al ₅ Fe ₂		<i>oC*</i> <i>Cmcm</i>		
	Al ₄ Mn	Al ₄ Mn	<i>oP60</i> <i>Pnnn</i>		
	Al ₆ Mn	Al ₆ Mn	<i>oC28</i>		
	Al ₁₂ Mn	Al ₁₂ W	<i>cI26</i> <i>Im$\bar{3}$</i>		not quoted in [90Mas] metast.
Al ₈ Mn ₅	Al ₈ Cr ₅	<i>hR26</i> <i>R3m</i>		Al ₈ Mn ₅ -D0 ₈	

System Al-Fe-Si

Ternary Solution Phases:

Liquid, fcc-A1, bcc-A2, bcc-B2

Quasi-binary phases:

AlFeSi- α , AlFeSi- β , AlFeSi- γ , AlFeSi- δ , Al₁₃Fe₄

Modelling:

Liquid	:	Substitutional, Redlich-Kister
Al ₅ Fe ₄	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
bcc-B2	:	Sublattice model, (Al,Fe,Si) _{0.5} (Al,Fe,Si) _{0.5} (\square) ₃
Al ₁₃ Fe ₄	:	Quasi-binary, (Al) _{.6275} (Fe) _{.235} (Al,Si, \square) _{.1375}
AlFeSi- α	:	Quasi-binary, (Al) _{.6612} (Fe) _{.19} (Si) _{.0496} (Al,Si) _{.0992}
AlFeSi- β	:	Stoichiometric, (Al) ₁₄ (Fe) ₃ (Si) ₃
AlFeSi- δ	:	Stoichiometric, (Al) _{.55} (Fe) _{.15} (Si) _{.3}
AlFeSi- γ	:	Stoichiometric, (Al) ₃ (Fe)(Si)
AlFeSi- τ_1	:	Stoichiometric, (Al) ₂ (Fe) ₂ (Si)
AlFeSi- τ_3	:	Stoichiometric, (Al) ₂ (Fe)(Si)

Comments:

No ternary interaction coefficients for the substitutional solutions.

Assessor and Date:

P. Kolby, 1997.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Al₁₃Fe₄

$$\begin{aligned}
 G^\circ(T) &= 0.6275 H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 0.235 H_{\text{Fe}}^{\circ, \text{bcc-A2, para}}(298.15 \text{ K}) \\
 &\quad - 0.1375 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\
 &\quad - 22013.336 + 0.6275 \text{ GHSE}_{\text{Al}} + 0.235 \text{ GHSE}_{\text{Fe}} + 0.1375 \text{ GHSE}_{\text{Si}}
 \end{aligned}$$

Phase AlFeSi- α

$$G^\circ(T) - 0.7604 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.19 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ - 0.0496 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si:Al}) = \\ - 24920.609 + 5.4894 T + 0.7604 \text{ GHSER}_{\text{Al}} + 0.19 \text{ GHSER}_{\text{Fe}} + 0.0496 \\ \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - 0.6612 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.19 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ - 0.1488 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si:Si}) = \\ - 25340.922 + 5.4894 T + 0.6612 \text{ GHSER}_{\text{Al}} + 0.19 \text{ GHSER}_{\text{Fe}} \\ + 0.1488 \text{ GHSER}_{\text{Si}}$$

Phase AlFeSi- β

$$G^\circ(T) - 14.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ - 391310.9 + 55.84756 T + 14.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Fe}} \\ + 3.0 \text{ GHSER}_{\text{Si}}$$

Phase AlFeSi- δ

$$G^\circ(T) - 0.55 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.15 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ - 0.3 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ - 14431.105 - 2.90062 T + 0.55 \text{ GHSER}_{\text{Al}} + 0.15 \text{ GHSER}_{\text{Fe}} \\ + 0.3 \text{ GHSER}_{\text{Si}}$$

Phase AlFeSi- γ

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ - 116929.6 + 8.399833 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Si}}$$

Phase AlFeSi- τ_1

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ - 153000 + 2.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Si}}$$

Phase AlFeSi- τ_3

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ - 99325.65 + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Si}}$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Fe-Si	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Fe)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Fe)	W	$cI2$ $Im\bar{3}m$	M 2	
	(Si)	diamond	$cF8$ $Fd\bar{3}m$		
	Al ₃ Fe		$mC102$ $C2/m$		designated by Al ₁₃ Fe ₄
Al-Fe-Si	AlFeSi- α	Fe ₂ Al ₇ Si	$hP246$		$hP246$ and Fe ₂ Al _{7.4} Si in [92Pet]
	AlFeSi- β	Fe ₂ Al ₉ Si ₂	m^{**}		
	AlFeSi- γ		c^{**}		
	AlFeSi- δ	PdGa ₅	$tI24$		FeAl ₄ Si ₂ in [91Vil] FeAl ₄ Si ₃ in [92Pet]
	AlFeSi- τ_1				Fe ₃ Al ₃ Si ₂
	AlFeSi- τ_3				Fe ₅ Al ₉ Si ₅

System Al–Li–Mg

Ternary Solution Phases:

Liquid, fcc–A1, bcc–A2, hcp–A3

Ternary Compounds:

AlLi, AlLiMg– τ , AlMg– β , Al₁₂Mg₁₇

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc–A2	:	Substitutional, Redlich-Kister
fcc–A1	:	Substitutional, Redlich-Kister
hcp–A3	:	Substitutional, Redlich-Kister
AlLi	:	Sublattice model, (Al,Li,Mg)(Li,Mg, \square)
AlLiMg– τ	:	Stoichiometric, (Al) _{0.53} (Li) _{0.33} (Mg) _{0.14}
AlMg– β	:	Sublattice model, (Al) _{0.615} (Li,Mg) _{0.385}
Al ₁₂ Mg ₁₇	:	Sublattice model, (Li,Mg) ₂₄ (Al,Li,Mg) ₁₀ (Al,Mg) ₂₄

Assessor and Date:

N. Saunders, (1994).

Comments:

The data below are compatible with Version I of the Al–Mg system.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Liquid

$$L_{\text{Al,Li,Mg}}^{0,\text{liquid}} = -20000$$

$$L_{\text{Al,Li,Mg}}^{1,\text{liquid}} = -15000$$

$$L_{\text{Al,Li,Mg}}^{2,\text{liquid}} = -20000$$

Phase bcc-A2

$$L_{\text{Al,Li,Mg};\square}^{0,\text{bcc-A2}} = -71200.0 + 50.0 T$$

Phase fcc-A1

$$L_{\text{Al,Li,Mg};\square}^{0,\text{fcc-A1}} = -63650.0 + 50.0 T$$

Phase hcp-A3

$$L_{\text{Al,Li,Mg};\square}^{0,\text{hcp-A3}} = 1.0\text{E-4}$$

$$L_{\text{Al,Li,Mg};\square}^{1',\text{hcp-A3}} = 1.0\text{E-4}$$

$$L_{\text{Al,Li,Mg};\square}^{2,\text{hcp-A3}} = -80000 + 50.0 T$$

Phase AlLi

$$L_{\text{Al,Mg};\text{Li}}^{0,\text{AlLi}} = 3300.0 - 2.0 T$$

$$L_{\text{Al,Mg};\text{Li,Mg}}^{0,\text{AlLi}} = -43460.0 + 60.0 T$$

$$L_{\text{Al};\text{Li,Mg}}^{0,\text{AlLi}} = -25000.0 + 10.0 T$$

Phase AlMg-β

$$L_{\text{Al};\text{Li,Mg}}^{0,\text{AlMg-}\beta} = -4250$$

Phase AlLiMg-τ

$$\begin{aligned} G^\circ(T) - 0.53 H_{\text{Al}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - 0.33 H_{\text{Li}}^{0,\text{bcc-A2}}(298.15 \text{ K}) \\ - 0.14 H_{\text{Mg}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al};\text{Li};\text{Mg}) = \\ -15500 + 23.93 T - 3.0 T \cdot \ln T + 0.53 \text{ GHSER}_{\text{Al}} \\ + 0.33 \text{ GHSER}_{\text{Li}} + 0.14 \text{ GHSER}_{\text{Mg}} \end{aligned}$$

Phase Al₁₂Mg₁₇

$$\begin{aligned} G^\circ(T) - 24.0 H_{\text{Al}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - 10.0 H_{\text{Li}}^{0,\text{bcc-A2}}(298.15 \text{ K}) \\ - 24.0 H_{\text{Mg}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg};\text{Li};\text{Al}) = \\ -610000 + 125 T + 24.0 \text{ GHSER}_{\text{Al}} + 10.0 \text{ GHSER}_{\text{Li}} \\ + 24.0 \text{ GHSER}_{\text{Mg}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 24.0 H_{\text{Al}}^{0,\text{fcc-A1}}(298.15 \text{ K}) - 24.0 H_{\text{Li}}^{0,\text{bcc-A2}}(298.15 \text{ K}) \\ - 10.0 H_{\text{Mg}}^{0,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Li};\text{Mg};\text{Al}) = \\ -625000 + 269 T + 24.0 \text{ GHSER}_{\text{Al}} + 24.0 \text{ GHSER}_{\text{Li}} \\ + 10.0 \text{ GHSER}_{\text{Mg}} \end{aligned}$$

$$\begin{aligned}
 &G^\circ(T) - 24.0 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 10.0 H_{\text{Li}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) \\
 &- 24.0 H_{\text{Mg}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Li:Al:Mg}) = \\
 &\quad 1.0\text{E-}4 + 24.0 \text{ GHSER}_{\text{Al}} + 10.0 \text{ GHSER}_{\text{Li}} + 24.0 \text{ GHSER}_{\text{Mg}} \\
 &L_{\text{Li,Mg:Al:Al}}^{0, \text{Al}_{12}\text{Mg}_{17}} = -220000 \\
 &L_{\text{Mg:Al,Li:Al}}^{0, \text{Al}_{12}\text{Mg}_{17}} = -50000
 \end{aligned}$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Li-Mg	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	(Li)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M 2	
	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	AlLi	NaTl	<i>cF16</i> <i>Fd$\bar{3}$m</i>	M ₁ 8 M ₂ 8	
	AlMg- γ	α -Mn cbcc-A12	<i>cI58</i> <i>I$\bar{4}$3m</i>	Al 24 Mg ₁ 2 Mg ₂ 8 Mg ₃ 24	designated as Al ₁₂ Mg ₁₇
	Al ₃ Mg ₂	Cd ₂ Na	<i>cF112</i> <i>Fd$\bar{3}$m</i>		<i>cF1832</i> in [91Vi] designated as AlMg- β
	Al ₂ LiMg		<i>c * 456</i>		AlLiMg- τ

System Al-Mg-Mn

Ternary Solution Phases:

Liquid, fcc-Al

Ternary Compound:

AlMgMn-T

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-Al	:	Substitutional, Redlich-Kister
AlMgMn-T	:	Stoichiometric, (Al) ₁₈ (Mg) ₃ (Mn) ₂

Assessor and Date:

I. Ansara (1994).

Comments:

The data are valid only in the Al-rich corner.
Very little information on the phase relationships
is known

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlMgMn-T

$$\begin{aligned}
 G^{\circ}(T) - 18.0 H_{\text{Al}}^{\circ, \text{fcc-Al1}}(298.15 \text{ K}) - 3.0 H_{\text{Mg}}^{\circ, \text{hcp-Al3}}(298.15 \text{ K}) \\
 - 2.0 H_{\text{Mn}}^{\circ, \text{cbcc-Al2, para}}(298.15 \text{ K}) = G(\text{Al:Mg:Mn}) = \\
 - 206402.0 + 11.85 T + 18.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Mg}} \\
 + 2.0 \text{ GHSER}_{\text{Mn}}
 \end{aligned}$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mg-Mn	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Mg)	Mg	$hP2$ $P6_3/mmc$	M 2	
	α -Mn	α -Mn	$c58$ $I\bar{4}3m$		cbcc-A1
	β -Mn	β -Mn	$cP20$ $P4_132$		cub-A13
	γ -Mn	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	δ -Mn	W	$cI2$ $Im\bar{3}m$	M 2	
	$Al_{18}Mg_3Mn_2$	$Al_{18}Cr_2Mg_3$	$cF184$ $Fd\bar{3}m$		designated as AlMgMn-T

System Al-Mg-Si

Ternary Solution Phases:

Liquid, fcc-A1, hcp-A3, diamond

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
diamond	:	Substitutional, Redlich-Kister

Assessor and Date:

H. L. Lukas (1996)

Comments:

No ternary compounds or quasi-binary phases

Publication:

H. Feufel, T. Gödecke, H. L. Lukas, and F. Sommer,
J. Alloys Comp. **247**, 31-42 (1997).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Liquid

$$L_{\text{Al,Mg,Si}}^{0,\text{liquid}} = 4125.86 - 0.51573 T$$

$$L_{\text{Al,Mg,Si}}^{1,\text{liquid}} = -47961.64 + 5.9952 T$$

$$L_{\text{Al,Mg,Si}}^{2,\text{liquid}} = 25813.8 - 3.22672 T$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mg-Si	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Si)	diamond	<i>cF8</i> <i>Fd$\bar{3}$m</i>		

System Al-Mg-Zn

Ternary Solution Phases:

Liquid, fcc-Al, hcp-A3, hcp-Zn, τ , φ

Compounds:

AlMg- β , AlMg- γ , Laves-C14

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-Al	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
AlMg- β	:	Sublattice model, $(\text{Mg})_{89}(\text{Al,Zn})_{140}$
AlMg- γ	:	Sublattice model, $(\text{Al,Mg,Zn})_{12}(\text{Al,Mg,Zn})_{12}(\text{Mg})_5$
Laves-C14	:	Sublattice model, $(\text{Al,Mg,Zn})(\text{Al,Mg,Zn})_2$
τ	:	Sublattice model, $(\text{Mg})_{26}(\text{Al,Mg})_6(\text{Al,Mg,Zn})_{48}(\text{Al})$
φ	:	Sublattice model, $(\text{Mg})_6(\text{Al,Zn})_5$

Assessor and Date:

P. Liang, H. L. Lukas (1967)

Publication:

P. Liang, T. Tarfa, J. A. Robinson, S. Wagner, P. Ochin, M. G. Harmelin, H. J. Seifert, H. L. Lukas, G. Effenberg, F. Aldinger

Thermochimica Acta, **314**, 1-2, 87-110 (1998).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Liquid

$$L_{\text{Al,Mg,Zn}}^{0,\text{liquid}} = -11475 + 11 T$$

$$L_{\text{Al,Mg,Zn}}^{1,\text{liquid}} = -11475 + 11 T$$

$$L_{\text{Al,Mg,Zn}}^{2,\text{liquid}} = -11475 + 11 T$$

Phase hcp-A3

$$L_{\text{Al,Mg,Zn}}^{0,\text{hcp-A3}} = 1.0\text{E-4}$$

$$L_{\text{Al,Mg,Zn}}^{1,\text{hcp-A3}} = 1.0\text{E-4}$$

$$L_{\text{Al,Mg,Zn}}^{2,\text{hcp-A3}} = 1.0\text{E-4}$$

Phase hcp-Zn

$$L_{\text{Al,Mg,Zn}}^{0,\text{hcp-Zn}} = 1.0\text{E-4}$$

$$L_{\text{Al,Mg,Zn}}^{1,\text{hcp-Zn}} = 1.0\text{E-4}$$

$$L_{\text{Al,Mg,Zn}}^{2,\text{hcp-Zn}} = 1.0\text{E-4}$$

Phase Laves-C14

$$L_{\text{Mg,Zn:Al}}^{0,\text{Laves-C14}} = 35000$$

$$L_{\text{Zn:Al,Mg}}^{0,\text{Laves-C14}} = 15000$$

$$L_{\text{Al,Zn:Mg}}^{0,\text{Laves-C14}} = -7500 - 18 T$$

$$L_{\text{Al:Mg,Zn}}^{0,\text{Laves-C14}} = 8000$$

$$L_{\text{Al,Mg:Zn}}^{0,\text{Laves-C14}} = 8000$$

Phase AlMg-β

$$L_{\text{Al,Mg,Zn}}^{0,\text{AlMg-}\beta} = -1717500 + 343.5 T$$

Phase AlMg- γ

$$L_{\text{Mg:Mg:Al:Zn}}^{0,\text{AlMg-}\gamma} = -116000 + 58 T$$

$$L_{\text{Mg:Zn:Al:Mg}}^{0,\text{AlMg-}\gamma} = 113100 - 14.5 T$$

Phase φ

$$L_{\text{Mg:Mg:Al,Zn}}^{0,\varphi} = -23100 + 11 T$$

Phase τ

$$\begin{aligned} G^\circ(T) - 7.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 26.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) \\ - 48.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Al:Zn:Al}) = \\ - 832680 + 162 T + 7.0 \text{GHSE}_{\text{Al}} + 26.0 \text{GHSE}_{\text{Mg}} \\ + 48.0 \text{GHSE}_{\text{Zn}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 32.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) \\ - 48.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Mg:Zn:Al}) = \\ - 811620 + 162 T + \text{GHSE}_{\text{Al}} + 32.0 \text{GHSE}_{\text{Mg}} + 48.0 \text{GHSE}_{\text{Zn}} \end{aligned}$$

$$L_{\text{Mg:Al:Al,Zn:Al}}^{0,\tau} = -16200 + 243 T$$

$$L_{\text{Mg:Mg:Al,Zn:Al}}^{0,\tau} = -105300 + 243 T$$

$$L_{\text{Mg:Al:Mg,Zn:Al}}^{0,\tau} = 243000 + 81 T$$

$$L_{\text{Mg:Mg:Mg,Zn:Al}}^{0,\tau} = 243000 + 81 T$$

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Cu-Mg	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2	
	Laves-C14	MgZn ₂	<i>hP12</i> <i>P6$_3$/mmc</i>	Cu 2 Cu 6 Mg 4	
	Al ₃ Mg ₂	Cd ₂ Na	<i>cF112</i> <i>Fd$\bar{3}$m</i>		<i>cF1832</i> in [91Vil] designated as AlMg- β
	AlMg- γ	α -Mn	<i>cI58</i> <i>I43m</i>	Al 24 Mg ₁ 2	designated as Al ₁₂ Mg ₁₇
	Φ		<i>o*</i>		
	τ	Mg ₃₂ (Al,Zn) ₄₉	<i>cI162</i> <i>I$\bar{m}$$\bar{3}$</i>		

System Al-Mn-Si

Ternary Solution Phases:

Liquid, fcc-Al, Al₈Mn₅-D8₁₀

Quasi-binary phases:

AlMnSi- α , AlMnSi- β

Compounds:

AlMnSi- δ

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-Al	:	Substitutional, Redlich-Kister
Al ₈ Mn ₅ -D8 ₁₀	:	Sublattice model, (Al,Si) ₁₂ (Mn) ₄ (Al,Mn) ₁₀
AlMnSi- α	:	Quasi-binary, (Al) ₁₆ (Mn) ₄ (Si)(Al,Si) ₂
AlMnSi- β	:	Quasi-binary, (Al) ₁₅ (Si)(Al,Si) ₄ (Mn) ₆
AlMnSi- δ	:	Stoichiometric, (Al) ₂ (Mn)(Si) ₃

Comments:

The data below are valid in the composition range $x_{Si} < 0.2$ and $x_{Mn} < 0.05$
The fcc-Al phase is assumed to be ideal

Assessor and Date:

P. Kolby, M.H. Rand, and T.G. Chart, 1997.

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Liquid

$$L_{Al,Mn,Si}^{0,Liquid} = -37000$$

Phase Al₈Mn₅-D8₁₀

$$G^{\circ}(T) - 10.0 H_{Al}^{\circ, fcc-Al}(298.15 \text{ K}) - 4.0 H_{Mn}^{\circ, cbcc-Al2, para}(298.15 \text{ K}) - 12.0 H_{Si}^{\circ, diamond}(298.15 \text{ K}) = 10.0 \text{ GHSE}_{Al} + 4.0 \text{ GHSE}_{Mn} + 12.0 \text{ GHSE}_{Si}$$

Phase AlMnSi- α

$$G^\circ(T) - 18.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 4.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{Al12,para}}(298.15 \text{ K}) \\ - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 755772 + 3544.43 T - 573.95 T \cdot \ln T \\ - 0.114419 T^2 + 9.70013\text{E-}06 T^3 + 3716760 T^{-1}$$

$$G^\circ(T) - 16.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 4.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{Al12,para}}(298.15 \text{ K}) \\ - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 698911 + 2958.7 T - 493.78 T \cdot \ln T \\ - 0.17905 T^2 + 1.87237\text{E-}05 T^3 + 1822810 T^{-1}$$

$$L_{\text{Al:Mn:Si:Al,Si}}^{\circ,\text{AlMnSi-}\alpha} = 0.0001$$

Phase AlMnSi- β

$$G^\circ(T) - 19.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 6.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{Al12,para}}(298.15 \text{ K}) \\ - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 880648 + 3451.04 T - 572.75 T \cdot \ln T \\ - 0.201935 T^2 + 2.0\text{E-}05 T^3 + 2184750 T^{-1}$$

$$G^\circ(T) - 15.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 6.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{Al12,para}}(298.15 \text{ K}) \\ - 5.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 779980 + 3451.04 T - 593.657 T \cdot \ln T \\ - 0.16164 T^2 + 1.35092\text{E-}05 T^3 + 2946120 T^{-1}$$

$$L_{\text{Al:Si:Al,Si:Mn}}^{\circ,\text{AlMnSi-}\beta} = 0.0001$$

Phase AlMnSi- δ

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-\text{Al1}}(298.15 \text{ K}) - 3.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{Al12,para}}(298.15 \text{ K}) \\ - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 70000 - 2 T + 2.0 \text{GHSE}_{\text{Al}} + 3.0 \text{GHSE}_{\text{Mn}} \\ + \text{GHSE}_{\text{Si}}$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mn-Si	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Mg)	Mg	$hP2$ $P6_3/mmc$	M 2	
	α -Mn	α -Mn	$c58$ $I\bar{4}3m$		cbcc-A1
	β -Mn	β -Mn	$cP20$ $P4_132$		cub-A13
	γ -Mn	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	δ -Mn	W	$cI2$ $Im\bar{3}m$	M 2	
	(Si)	diamond	$cF8$ $Fd\bar{3}m$		
	AlMnSi- α	Al ₉ Mn ₂ Si	$cP138$ $Pm\bar{3}$		
	AlMnSi- β	Al ₁₀ Mn ₃	$hP26$ $P6_3/mmc$		
	AlMnSi- δ		$hP100$		quoted in [93Pet]
Al ₈ Mn ₅ -D8 ₁₀	Al ₈ Cr ₅	$hR26$ $R\bar{3}m$			

System Al–Mo–Ti

Solution Phases:

Liquid, bcc-A2, fcc-A1, bcc-B2, hcp-A3

Ternary Compounds:

AlM-D0₁₉, AlM-D0₂₂, AlTi-L1₀

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
bcc-B2	:	Sublattice model, (Al,Mo,Ti) _{0.5} (Al,Mo,Ti) _{0.5} (□) ₃ The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 ⇌ bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM-D0 ₁₉	:	Sublattice model, (Al,Mo,Ti) ₃ (Al,Mo,Ti)(□) _{0.5}
AlM-D0 ₂₂	:	Sublattice model, (Al,Mo,Ti) ₃ (Al,Mo,Ti)
AlTi-L1 ₀	:	Sublattice model, (Al,Mo,Ti)(Al,Mo,Ti)

Assessor and Date:

N. Saunders, 1996

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlM-D0₁₉

$$L_{\text{Mo:Al,Ti:}\square}^{0,\text{AlM-D0}_{19}} = 10656 - 1.332 T$$

$$L_{\text{Al,Ti:Mo:}\square}^{0,\text{AlM-D0}_{19}} = 32000 - 4 T$$

Phase AlM-D0₂₂

$$L_{\text{Al:Mo,Ti}}^{0,\text{AlM-D0}_{22}} = -212000 + 120 T$$

Phase AlTi-L1₀

$$L_{\text{Mo,Ti:Al}}^{0,\text{AlTi-L1}_0} = L_{\text{Al:Mo,Ti}}^{0,\text{AlTi-L1}_0} = -13000$$

$$L_{\text{Mo,Ti:Al}}^{1,\text{AlTi-L1}_0} = L_{\text{Al:Mo,Ti}}^{1,\text{AlTi-L1}_0} = 1.0\text{E-4}$$

$$L_{\text{Mo,Ti:Al}}^{2,\text{AlTi-L1}_0} = L_{\text{Al:Mo,Ti}}^{2,\text{AlTi-L1}_0} = -13000$$

$$L_{\text{Mo:Al,Ti}}^{0,\text{AlTi-L1}_0} = L_{\text{Al,Ti:Mo}}^{0,\text{AlTi-L1}_0} = -15134 - 2.36 T$$

Phase bcc-A2

$$L_{\text{Al,Mo,Ti:}\square}^{1,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Mo,Ti:}\square}^{2,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Mo,Ti:}\square}^{3,\text{bcc-A2}} = 0$$

Phase bcc-B2

$$L_{\text{Mo,Ti:Al:}\square}^{0,\text{bcc-B2}} = L_{\text{Al:Mo,Ti:}\square}^{0,\text{bcc-B2}} = -5000$$

$$L_{\text{Mo:Al,Ti:}\square}^{0,\text{bcc-B2}} = L_{\text{Al,Ti:Mo:}\square}^{0,\text{bcc-B2}} = 8750 - 1.25 T$$

$$L_{\text{Ti:Al,Mo:}\square}^{0,\text{bcc-B2}} = L_{\text{Al,Mo:Ti:}\square}^{0,\text{bcc-B2}} = 14100 - 2 T$$

Phase bcc-A2

$$L_{\text{Al,Mo,Ti:}\square}^{0,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Mo,Ti:}\square}^{1,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Mo,Ti:}\square}^{2,\text{bcc-A2}} = 0$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mo-Ti	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	(Mo)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M 2	
	bcc-B2	CsCl	<i>cP2</i> <i>Pm$\bar{3}$m</i>	M ₁ 1 M ₂ 1	
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M 2	
	AlTi	AuCu	<i>tP4</i> <i>P4/mmm</i>	Al 2 Ti ₁ 1 Ti ₂ 1	AlTi-L1 ₀
	AlTi ₃	Ni ₃ Sn	<i>hP8</i> <i>P6₃/mmc</i>		AlM-D0 ₁₉
	Al ₃ Ti	Al ₃ Ti	<i>tI8</i> <i>I4/mmm</i>	Al ₁ 2 Al ₂ 4 Ti 2	AlM-D0 ₂₂

System Al-N-Ti

Ternary Solution Phases:

Liquid, bcc-A2, hcp-A3

Ternary Compounds:

AlTi₂, AlTi₃, Al₂N₂Ti₃

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
AlTi ₂	:	Stoichiometric, (Al)(Ti) ₂ (N) _{0.82}
AlTi ₃	:	Stoichiometric, (Al)(Ti) ₃ (N) _{0.56}
Al ₂ N ₂ Ti ₃	:	Stoichiometric, (Al) ₂ (Ti) ₃ (N) ₂

Assessor and Date:

K. Zeng, and R. Schmid-Fetzer, Univ. Clausthal, Germany, (1996).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-A2

$$L_{\text{Al,Ti:N}}^{0,\text{bcc-A2}} = -200000$$

$$L_{\text{Al,Ti:N},\square}^{0,\text{bcc-A2}} = -200000$$

Phase hcp-A3

$$L_{\text{Al,Ti:N}}^{0,\text{hcp-A3}} = -100000$$

$$L_{\text{Al,Ti:N},\square}^{0,\text{hcp-A3}} = -80000$$

$$L_{\text{Al,Ti:N},\square}^{1,\text{hcp-A3}} = -37300 + 100 T$$

Phase AlNTi₂

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc}-\text{Al}}(298.15 \text{ K}) - 0.82 H_{0.5\text{N}_2}^{\circ, \text{gas}}(298.15 \text{ K}) \\ - 2.0 H_{\text{Ti}}^{\circ, \text{hcp}-\text{A3}}(298.15 \text{ K}) = \\ - 389592 + 104 T + \text{GHSER}_{\text{Al}} + 2.0 \text{GHSER}_{\text{Ti}} + 0.82 \text{GHSER}_{0.5\text{N}_2}$$

Phase AlNTi₃

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc}-\text{Al}}(298.15 \text{ K}) - 0.56 H_{0.5\text{N}_2}^{\circ, \text{gas}}(298.15 \text{ K}) \\ - 3.0 H_{\text{Ti}}^{\circ, \text{hcp}-\text{A3}}(298.15 \text{ K}) = \\ - 349502.5 + 92.5 T + \text{GHSER}_{\text{Al}} + 3.0 \text{GHSER}_{\text{Ti}} + 0.56 \text{GHSER}_{0.5\text{N}_2}$$

Phase Al₂N₂Ti₃

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ, \text{fcc}-\text{Al}}(298.15 \text{ K}) - 2.0 H_{0.5\text{N}_2}^{\circ, \text{gas}}(298.15 \text{ K}) \\ - 3.0 H_{\text{Ti}}^{\circ, \text{hcp}-\text{A3}}(298.15 \text{ K}) = \\ 3405331.05 - 5217.37371 T + 1.75061514 T^2 + 2.0 \text{GHSER}_{\text{Al}} \\ + 3.0 \text{GHSER}_{\text{Ti}} + 2.0 \text{GHSER}_{0.5\text{N}_2}$$

Table I:a - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-N-Ti	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2
	AlNTi ₂	AlCCr ₂	<i>hP8</i> <i>P6₃/mmc</i>	
	AlNTi ₃	CaO ₃ Ti	<i>cP5</i> <i>Pm$\bar{3}m$</i>	M ₁ 1 M ₂ 1 Ti 3

Table I:b - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
	$\text{Al}_2\text{N}_2\text{Ti}_3$	$\text{Al}_2\text{N}_2\text{Ti}_3$	<i>hP22</i> <i>P31c</i>	Al ₁ 2 Ti ₁ 2 Al ₂ 2 N ₁ 2 N ₂ 2 N ₃ 2 N ₄ 2 Ti ₂ 2 Ti ₃ 2 Ti ₄ 2 Ti ₅ 2

System Al-Nb-Ti

Solution Phases:

Liquid, bcc-A2, fcc-A1, bcc-B2, hcp-A3

Ternary Compounds:

AlM-D0₁₉, AlM-D0₂₂, AlTi-L1₀, σ , AlNb₃-A15

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
bcc-B2	:	Sublattice model, (Al,Nb,Ti) _{0.5} (Al,Nb,Ti) _{0.5} (□) ₃
bcc-B2	:	Sublattice model, (Al,Mo,Ti) _{0.5} (Al,Mo,Ti) _{0.5} (□) ₃ The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 \rightleftharpoons bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlNb ₃ -A15	:	Sublattice model, (Al,Nb)(Nb) ₃
AlM-D0 ₁₉	:	Sublattice model, (Al,Nb,Ti) ₃ (Al,Nb,Ti)(□) _{0.5}
AlM-D0 ₂₂	:	Sublattice model, (Al,Nb,Ti) ₃ (Al,Nb,Ti)
AlTi-L1 ₀	:	Sublattice model, (Al,Nb,Ti)(Al,Nb,Ti)
σ	:	Sublattice model, (Al) ₈ (Nb,Ti) ₄ (Al,Nb,Ti) ₁₈

Assessor and Date:

N. Saunders, 1996

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlM-D0₂₂

$$L_{\text{Al:Nb,Ti}}^{0,\text{AlM-D0}_{22}} = 20000$$

Phase AlM-D0₁₉

$$L_{\text{Nb:Al,Ti};\square}^{0,\text{AlM-D0}_{19}} = 10656 - 1.333 T$$

$$L_{\text{Ti:Al,Nb};\square}^{0,\text{AlM-D0}_{19}} = 4000$$

$$L_{\text{Al,Ti:Nb};\square}^{0,\text{AlM-D0}_{19}} = 32000 - T$$

$$L_{\text{Al,Nb:Ti};\square}^{0,\text{AlM-D0}_{19}} = 12000$$

Phase AlTi-L1₀

$$L_{\text{Al,Nb,Ti:Al}}^{0,\text{AlTi-L1}_0} = -45000$$

$$L_{\text{Al:Al,Nb,Ti}}^{0,\text{AlTi-L1}_0} = -45000$$

$$L_{\text{Nb,Ti:Al}}^{0,\text{AlTi-L1}_0} = -18076 + 12 T$$

$$L_{\text{Nb:Al,Ti}}^{0,\text{AlTi-L1}_0} = -15134 - 2.36 T$$

$$L_{\text{Ti:Al,Nb}}^{0,\text{AlTi-L1}_0} = -37600$$

$$L_{\text{Al,Ti:Nb}}^{0,\text{AlTi-L1}_0} = -15134 - 2.36 T$$

$$L_{\text{Al:Nb,Ti}}^{0,\text{AlTi-L1}_0} = -18076 + 12 T$$

$$L_{\text{Al,Nb:Ti}}^{0,\text{AlTi-L1}_0} = -37600$$

Phase bcc-A2

$$L_{\text{Al,Nb,Ti};\square}^{0,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Nb,Ti};\square}^{1,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Nb,Ti};\square}^{2,\text{bcc-A2}} = 0$$

Phase bcc-B2

$$G_{\text{Al:Nb};\square}^* = -8650 + T$$

$$G_{\text{Al:Ti};\square}^* = -8750 + 1.35 T$$

$$G_{\text{Nb:Ti};\square}^* = 5500$$

$$L_{\text{Nb,Ti:Al};\square}^{0,\text{bcc-B2}} = L_{\text{Al:Nb,Ti:Al};\square}^{0,\text{bcc-B2}} = -G_{\text{Nb:Ti};\square}^*$$

$$L_{\text{Nb:Al,Ti};\square}^{0,\text{bcc-B2}} = L_{\text{Al,Ti:Nb};\square}^{0,\text{bcc-B2}} = -G_{\text{Al:Ti};\square}^*$$

$$L_{\text{Ti:Al,Nb};\square}^{0,\text{bcc-B2}} = L_{\text{Al,Nb:Ti};\square}^{0,\text{bcc-B2}} = -G_{\text{Al:Nb};\square}^*$$

Phase bcc-A2

$$L_{\text{Al,Nb,Ti};\square}^{0,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Nb,Ti};\square}^{1,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Nb,Ti};\square}^{2,\text{bcc-A2}} = 0$$

Phase hcp-A3

$$L_{\text{Al,Nb,Ti};\square}^{0,\text{hcp-A3}} = -10 T$$

Phase σ

$$\begin{aligned} G^\circ(T) - 8.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 18.0 H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) \\ - 4.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al:Ti:Nb}) = \\ - 660000 + 79.5 T + 8.0 \text{ GHSE}_{\text{Al}} + 18.0 \text{ GHSE}_{\text{Nb}} \\ + 4.0 \text{ GHSE}_{\text{Ti}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 8.0 H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 4.0 H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) \\ - 18.0 H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al:Nb:Ti}) = \\ - 690000 + 148.5 T + 8.0 \text{ GHSE}_{\text{Al}} + 4.0 \text{ GHSE}_{\text{Nb}} \\ + 18.0 \text{ GHSE}_{\text{Ti}} \end{aligned}$$

$$L_{\text{Al:Nb:Al,Ti};\square}^{0,\sigma} = -1680000 + 510 T$$

$$L_{\text{Al:Ti:Al,Nb};\square}^{0,\sigma} = -990000 + 270 T$$

$$L_{\text{Al:Ti:Al,Nb};\square}^{1,\sigma} = 420000$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Nb-Ti	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Nb)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	bcc-B2	CsCl	<i>cP2</i> <i>Pm$\bar{3}m$</i>	M ₁ 1 M ₂ 1	
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	AlTi	AuCu	<i>tP4</i> <i>P4/mmm</i>	Al 2 Ti ₁ 1 Ti ₂ 1	AlTi-L1 ₀
	AlTi ₃	Ni ₃ Sn	<i>hP8</i> <i>P6₃/mmc</i>		AlM-D0 ₁₉
	Al ₃ Ti	Al ₃ Ti	<i>tI8</i> <i>I4/mmm</i>	Al ₁ 2 Al ₂ 4 Ti 2	AlM-D0 ₂₂
	AlNb ₃	Cr ₃ Si	<i>cP8</i> <i>Pm$\bar{3}n$</i>	Al 2 Nb 6	cub-A15
	σ	σ CrFe	<i>tP30</i> <i>P4₂/mnm</i>		

System Al–Si–Zn

Ternary Solution Phases:

Liquid, fcc–Al, hcp–Zn

Modelling:

Liquid : Substitutional, Redlich-Kister
 fcc–Al : Substitutional, Redlich-Kister
 hcp–Zn : Substitutional, Redlich-Kister

Assessor and Date:

M. Jacobs (1992).

Comments:

No ternary interaction coefficients.
 No ternary compounds.

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-Si-Zn	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4
	(Si)	diamond	<i>cF8</i> <i>Fd$\bar{3}$m</i>	
	(Zn)	Mg	<i>hP2</i> <i>P6$\bar{3}$/mmc</i>	M 2

System Al-Sn-Zn

Ternary Solution Phases:

Liquid, fcc-A1, hcp-A3, hcp-Zn

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister

Assessor and Date:

H. L. Lukas (1991)

Publication:

N. Chakraborti, G. Effenberg, S. Fries, S. Kuang,
H.-L. Lukas, and G. Petzow,
Votr. Poster Symp. Materialforsch., 1991,
2nd, 3, 2692-2693 (1991).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Liquid

$$L_{Al,Sn,Zn}^{0,liquid} = -2777.03 + 0.59427 T$$

$$L_{Al,Sn,Zn}^{1,liquid} = 15225.63 - 3.25821 T$$

$$L_{Al,Sn,Zn}^{2,liquid} = -16198.13 + 3.46632 T$$

Phase hcp-A3

$$L_{Al,Sn,Zn}^{0,hcp-A3} = 1.0E-4$$

Phase hcp-Zn

$$L_{Al,Sn,Zn}^{0,hcp-Zn} = 1.0E-4$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-Sn-Zn	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4
	(Sn)	β -Sn	<i>tI4</i> <i>I4$_1$/amd</i>	
	(Zn)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2

System Al-Sn-Zr

Ternary Solution Phases:

Liquid, bcc-A2, bct-A5, fcc-A1, hcp-A3

Compound:

AlSn₂Zr₅

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bct-A5	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
AlSn ₂ Zr ₅	:	Stoichiometric, (Al)(Sn) ₂ (Zr) ₅

Assessor and Date:

J. Korb, and K. Hack, GTT, Germany (1997)

Thermodynamic properties of the compound phase (J.mol⁻¹)

Phase AlSn₂Zr₅

$$\begin{aligned}
 G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 2.0 H_{\text{Sn}}^{\circ, \text{bct-A5}}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\
 - 58824.4 + 896.225 T - 177.0982 T \cdot \ln T - 0.0411 T^2 \\
 - 8.4073\text{E-}6 T^3 + 261079 T^{-1}
 \end{aligned}$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol	Sub-lattices	Comments
Al-Sn-Zr	(Al)	Cu	$cF4$ $Fm\bar{3}m$		not quoted in [91Vil] nor in [90Mas]
	(Sn)	β -Sn	$tI4$ $I4_1/amd$		
	(Zr)	Mg	$hP2$ $P6_3/mmc$	M 2	
	(Zr)	W	$cI2$ $I\bar{m}\bar{3}m$	M 4	
	$AlSn_2Zr_5$				

System Al-Ta-Ti

Solution Phases:

Liquid, bcc-A2, fcc-A1, bcc-B2, hcp-A3

Ternary Compounds:

AlM-D0₁₉, AlM-D0₂₂, AlTi-L1₀, σ

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
bcc-B2	:	Sublattice model, (Al,Ta,Ti) _{0.5} (Al,Ta,Ti) _{0.5} (\square) ₃ The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 \rightleftharpoons bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM-D0 ₁₉	:	Sublattice model, (Al,Ta,Ti) ₃ (Al,Ta,Ti)(\square) _{0.5}
AlM-D0 ₂₂	:	Sublattice model, (Al,Ta,Ti) ₃ (Al,Ta,Ti)
AlTi-L1 ₀	:	Sublattice model, (Al,Ta,Ti)(Al,Ta,Ti)
σ	:	Sublattice model, (Al) ₈ (Ta,Ti) ₄ (Al,Ta,Ti) ₁₈

Assessor and Date:

N. Saunders, 1996

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase hcp-A3

$$L_{Al,Ta,Ti:\square}^{0,hcp-B3} = -40000$$

Phase AlTi-L1₀

$$L_{\text{Ta,Ti:Al}}^{0,\text{AlTi-L1}_0} = L_{\text{Al:Ta,Ti}}^{0,\text{AlTi-L1}_0} = -11000$$

$$L_{\text{Ta:Al,Ti}}^{0,\text{AlTi-L1}_0} = L_{\text{Al,Ti:Ta}}^{0,\text{AlTi-L1}_0} = -15134 - 2.36 T$$

Phase AlM-D0₁₉

$$L_{\text{Ta,Ti:Al:O}}^{0,\text{AlM-D0}_{19}} = -24000$$

$$L_{\text{Ta:Al,Ti:O}}^{0,\text{AlM-D0}_{19}} = 10656 - 1.332 T$$

$$L_{\text{Ti:Al,Ta:O}}^{0,\text{AlM-D0}_{19}} = 8000$$

$$L_{\text{Al,Ti:Ta:O}}^{0,\text{AlM-D0}_{19}} = 32000 - T$$

$$L_{\text{Al:Ta,Ti:O}}^{0,\text{AlM-D0}_{19}} = 2128$$

$$L_{\text{Al,Ta:Ti:O}}^{0,\text{AlM-D0}_{19}} = 20000$$

Phase AlM-D0₂₂

$$L_{\text{Al:Ta,Ti}}^{0,\text{AlM-D0}_{22}} = 20000$$

Phase bcc-A2

$$L_{\text{Al,Ta,Ti:Box}}^{0,\text{bcc-A2}} = -10000$$

Phase bcc-B2

$$G_{\text{Al:Ta}}^* = -8250 + T$$

$$G_{\text{Al:Ti}}^* = -8750 + 1.25 T$$

$$L_{\text{Ti:Al,Ta:O}}^{0,\text{bcc-B2}} = L_{\text{Al,Ta:Ti:O}}^{0,\text{bcc-B2}} = -G_{\text{Al:Ta}}^*$$

$$L_{\text{Ta:Al,Ti:O}}^{0,\text{bcc-B2}} = L_{\text{Al,Ti:Ta:O}}^{0,\text{bcc-B2}} = -G_{\text{Al:Ti}}^*$$

Phase bcc-A2

$$L_{\text{Al,Mo,Ti:O}}^{0,\text{bcc-A2}} = -10000$$

$$L_{\text{Al,Mo,Ti:O}}^{1,\text{bcc-A2}} = -10000$$

$$L_{\text{Al,Mo,Ti:O}}^{2,\text{bcc-A2}} = -10000$$

Phase σ

$$G^\circ(T) - 8.0 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 18.0 H_{Ta}^{\circ, bcc-A2}(298.15 \text{ K}) \\ - 4.0 H_{Ti}^{\circ, hcp-A3}(298.15 \text{ K}) = G(\text{Al:Ti:Ta}) = \\ - 672000 + 105 T + 8.0 \text{ GHSE}_{Al} + 18.0 \text{ GHSE}_{Ta} \\ + 4.0 \text{ GHSE}_{Ti}$$

$$G^\circ(T) - 8.0 H_{Al}^{\circ, fcc-A1}(298.15 \text{ K}) - 4.0 H_{Ta}^{\circ, bcc-A2}(298.15 \text{ K}) \\ - 18.0 H_{Ti}^{\circ, hcp-A3}(298.15 \text{ K}) = G(\text{Al:Ta:Ti}) = \\ - 720000 + 153.9 T + 8.0 \text{ GHSE}_{Al} + 4.0 \text{ GHSE}_{Ta} \\ + 18.0 \text{ GHSE}_{Ti}$$

$$L_{Al:Ta:Al:Ti:\square}^{0,\sigma} = -1680000 + 510 T$$

$$L_{Al:Ti:Al:Ta:\square}^{0,\sigma} = -1230000 + 450 T$$

$$L_{Al:Ti:Al:Ta:\square}^{1,\sigma} = 1.0E-4$$

$$L_{Al:Ti:Al:Ta:\square}^{2,\sigma} = 300000$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Ta-Ti	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(Ta)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	bcc-B2	CsCl	<i>cP2</i> <i>Pm$\bar{3}m$</i>	M ₁ 1 M ₂ 1	
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	AlTi	AuCu	<i>tP4</i> <i>P4/mmm</i>	Al 2 Ti ₁ 1 Ti ₂ 1	AlTi-L1 ₀
	AlTi ₃	Ni ₃ Sn	<i>hP8</i> <i>P6₃/mmc</i>		AlM-D0 ₁₉
	Al ₃ Ti	Al ₃ Ti	<i>tI8</i> <i>I4/mmm</i>	Al ₁ 2 Al ₂ 4 Ti 2	AlM-D0 ₂₂
	σ	σ CrFe	<i>tP30</i> <i>P4₂/mnm</i>		

System Al-Ti-W

Solution Phases:

Liquid, bcc-A2, fcc-A1, bcc-B2, hcp-A3

Ternary Compounds:

AlM-D0₁₉, AlTi-L1₀

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
bcc-B2	:	Sublattice model, (Al,Ti,W) _{0.5} (Al,Ti,W) _{0.5} (□) ₃ The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc-A2 \rightleftharpoons bcc-B2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM-D0 ₁₉	:	Sublattice model, (Al,Ti,W) ₃ (Al,Ti,W)(□) _{0.5}
AlTi-L1 ₀	:	Sublattice model, (Al,Ti,W)(Al,Ti,W)

Assessor and Date:

N. Saunders, 1996

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase AlM-D0₁₉

$$L_{\text{Ti,W:Al:}\square}^{0,\text{AlM-D0}_{19}} = 73212$$

$$L_{\text{Ti:Al,W:}\square}^{0,\text{AlM-D0}_{19}} = -2000$$

$$L_{\text{Al,Ti:W:}\square}^{0,\text{AlM-D0}_{19}} = 8000$$

$$L_{\text{Al:Ti,W:}\square}^{0,\text{AlM-D0}_{19}} = 8136$$

Phase AlTi-L1₀

$$L_{\text{Ti,W:Al}}^{0,\text{AlTi-L1}_0} = L_{\text{Al,Ti,W}}^{0,\text{AlTi-L1}_0} = 16914$$

$$L_{\text{W:Al,Ti}}^{0,\text{AlTi-L1}_0} = L_{\text{Al,Ti,W}}^{0,\text{AlTi-L1}_0} = -15134 - 2.36 T$$

$$L_{\text{Ti:Al,W}}^{0,\text{AlTi-L1}_0} = L_{\text{Al,W:Ti}}^{0,\text{AlTi-L1}_0} = -3000$$

Phase bcc-A2

$$L_{\text{Al,Ti,W:\square}}^{1,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Ti,W:\square}}^{2,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Ti,W,Ti:\square}}^{3,\text{bcc-A2}} = 0$$

Phase bcc-B2

$$G_{\text{Al:Ti:\square}}^* = -8750 + 1.25 T$$

$$L_{\text{W:Al,Ti:\square}}^{0,\text{bcc-B2}} = L_{\text{Al,Ti,W:\square}}^{0,\text{bcc-B2}} = -G_{\text{Al:Ti:\square}}^*$$

Phase bcc-A2

$$L_{\text{Al,Ti,W:\square}}^{0,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Ti,W:\square}}^{1,\text{bcc-A2}} = 0$$

$$L_{\text{Al,Ti,W:\square}}^{2,\text{bcc-A2}} = 0$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Ti-W	(Al)	Cu	<i>cF4</i> <i>Fm$\bar{3}m$</i>	M 4	
	(W)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	bcc-B2	CsCl	<i>cP2</i> <i>Pm$\bar{3}m$</i>	M ₁ 1 M ₂ 1	
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}m$</i>	M 2	
	AlTi	AuCu	<i>tP4</i> <i>P4/mmm</i>	Al 2 Ti ₁ 1 Ti ₂ 1	AlTi-L1 ₀
	AlTi ₃	Ni ₃ Sn	<i>hP8</i> <i>P6₃/mmc</i>		AlM-D0 ₁₉

System B–Hf–Ti

Ternary Solution Phases:

Liquid, bcc-A2, hcp-A3

Quasi-binary phases:

B₂M, B₄M₃, BM

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc-A2	:	Sublattice model (Hf,Ti)(B,□) ₃
hcp-A3	:	Sublattice model (Hf,Ti)(B,□) _{0.5}
B ₂ M	:	Quasi-binary, (B) ₂ (Hf,Ti)
B ₄ M ₃	:	Quasi-binary, (B) ₄ (Hf,Ti) ₃
BM	:	Quasi-binary, (B)(Hf,Ti)

Comments:

No ternary compounds

Assessor and Date:

H. Bittermann, (1997)

Publication:

H. Bittermann, and P. Rogl, J. Phase Equil., **18**,
24–47 (1997).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase Liquid

$$I_{\text{B,Hf,Ti}}^{0,\text{liquid}} = 41733.1$$

$$I_{\text{B,Hf,Ti}}^{0,\text{liquid}} = 125.375 \ T$$

$$I_{\text{B,Hf,Ti}}^{0,\text{liquid}} = 93.6697 \ T$$

Phase B₂M

$$L_{\text{B:Hf,Ti}}^{0,\text{B}_2\text{M}} = 7223.32 + 1.75379 T$$

Phase B₄M₃

$$L_{\text{B:Hf,Ti}}^{0,\text{B}_4\text{M}_3} = 115124 - 49.5166 T$$

Phase BM

$$L_{\text{B:Hf,Ti}}^{0,\text{BM}} = 19396.7 - 6.57772 T$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
B-Hf-Ti	(B)	β -rhombo-B		
	(Hf)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2
	(Hf)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M 2
	(Ti)	Mg	<i>hP2</i> <i>P6₃/mmc</i>	M 2
	(Ti)	W	<i>cI2</i> <i>Im$\bar{3}$m</i>	M 2
	BM	BFe	<i>oP8</i> <i>Pnma</i>	B 4 Ti 4
	B ₂ M	AlB ₂	<i>hP3</i> <i>P6/mmm</i>	B 2 Ti 1
	B ₄ M ₃	B ₄ Ta ₃	<i>oI14</i> <i>Immm</i>	

System Cu-Mg-Y

Ternary Solution Phases:

Liquid, fcc-A1, bcc-A2, hcp-A3

Modelling:

Liquid : Substitutional, Redlich-Kister
 fcc-A1 : Substitutional, Redlich-Kister
 hcp-A3 : Substitutional, Redlich-Kister

Assessor and Date:

T. Bühler, RWTH, Aachen, Germany, (1997).

Comments:

No coefficients for the ternary solution phases.
 No ternary compounds.

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Cu-Mg-Si	(Cu)	Cu	$cF4$ $Fm\bar{3}m$	M 4
	(Mg)	Mg	$hP2$ $P6_3/mmc$	M 2
	(Y)	W	$cI2$ $Im\bar{3}m$	M 4
	(Y)	Mg	$hP2$ $P6_3/mmc$	M 2

System Cu–Mg–Si

Ternary Solution Phases:

(stable) Liquid, fcc-A1, bcc-A2, hcp-A3
(metastable) hcp-Zn

Ternary Compounds:

CuMgSi- σ , CuMgSi- τ , Laves-C15

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
CuMgSi- σ	:	Stoichiometric, (Cu) ₁₆ (Mg) ₆ (Si) ₇
CuMgSi- τ	:	Stoichiometric, (Cu) ₃ (Mg) ₂ (Si)
Laves-C15	:	Sublattice model, (Cu,Mg,Si) ₂ (Cu,Mg,Si)

Assessor and Date:

T. Bühler, RWTH, Aachen, Germany, (1997).

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase CuMgSi- σ

$$\begin{aligned}
 G^\circ(T) - 16.0 H_{\text{Cu}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) \\
 - 7.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Cu:Mg:Si}) = \\
 - 559636 + 110.94 T + 16.0 \text{ GHSE}_{\text{Cu}} + 6.0 \text{ GHSE}_{\text{Mg}} \\
 + 7.0 \text{ GHSE}_{\text{Si}}
 \end{aligned}$$

Phase CuMgSi- τ

$$G^{\circ}(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Cu:Mg:Si}) = -141720 + 20.26 T + 3.0 \text{GHSER}_{\text{Cu}} + 2.0 \text{GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Si}}$$

Phase Liquid

$$L_{\text{Cu,Mg,Si}}^{0,\text{liquid}} = 1\text{E-}04$$

$$L_{\text{Cu,Mg,Si}}^{1,\text{liquid}} = -141736$$

$$L_{\text{Cu,Mg,Si}}^{2,\text{liquid}} = 1\text{E-}04$$

Phase hcp-Zn

$$L_{\text{Cu,Mg,Si};\square}^{0,\text{hcp-Zn}} = 50000$$

$$L_{\text{Cu,Mg,Si};\square}^{1,\text{hcp-Zn}} = 50000$$

$$L_{\text{Cu,Mg,Si};\square}^{2,\text{hcp-Zn}} = 50000$$

Phase Laves-C15

$$L_{\text{Mg,Si};\text{Cu}}^{0,\text{Laves-C15}} = 15000$$

$$L_{\text{Si};\text{Cu,Mg}}^{0,\text{Laves-C15}} = 6599.45$$

$$L_{\text{Cu,Si};\text{Mg}}^{0,\text{Laves-C15}} = -193131 + 20.69 T$$

$$L_{\text{Cu};\text{Mg,Si}}^{0,\text{Laves-C15}} = 8000$$

$$L_{\text{Cu,Mg};\text{Si}}^{0,\text{Laves-C15}} = 13011.35$$

Table I:a – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Cu-Mg-Si	(Cu)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Mg)	Mg	$hP2$ $P6_3/mmc$	M 2	
	(Si)	diamond	$cF8$ $Fd\bar{3}m$	M 8	

Table I:b – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
	Cu ₂ Mg	Cu ₂ Mg	<i>cF24</i> <i>Fd3m</i>	Cu 16 Mg 8	Laves-C15
	Cu ₁₆ Mg ₅ Si ₇	Mn ₂₃ Th ₆	<i>cF112</i> <i>Fm3m</i>	Si ₁ 4 Si ₁ 24 Mg 24 Cu ₁ 32 Cu ₂ 32	CuMgSi-σ
	Cu ₃ Mg ₂ Si	MgZn ₂	<i>hP12</i> <i>P6₃/mmc</i>	Si 2 Mg 4 Cu 6	CuMgSi-τ

System Cu-Mg-Zn

Ternary Solution Phases:

Liquid, fcc-A1, bcc-A2, bcc-B2, hcp-A3, hcp-Zn

Compounds:

Laves-C14, Laves-C15, Laves-C36, CuZn- γ , MgZn, Mg₂Zn₃, Mg₂Zn₁₁

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
bcc-B2	:	Sublattice model, (Cu,Mg,Zn) _{0.5} (Cu,Mg,Zn) _{0.5} Two descriptions of the bcc-A2: bcc-B2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 and 22 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
hcp-Zn	:	Substitutional, Redlich-Kister-Muggianu
CuZn- γ	:	Sublattice model, (Cu,Zn) ₂ (Cu,Zn) ₂ (Cu) ₃ (Mg,Zn) ₆
Laves-C14	:	Sublattice model, (Cu,Mg,Zn) ₂ (Cu,Mg,Zn)
Laves-C15	:	Sublattice model, (Cu,Mg,Zn) ₂ (Cu,Mg,Zn)
Laves-C36	:	Sublattice model, (Cu,Mg,Zn) ₂ (Cu,Mg,Zn)
MgZn	:	Sublattice model, (Mg) ₁₂ (Cu,Zn) ₁₃
Mg ₂ Zn ₃	:	Sublattice model, (Mg) ₂ (Cu,Zn) ₃
Mg ₂ Zn ₁₁	:	Sublattice model, (Mg) ₂ (Cu,Zn) ₁₁

Assessor and Date:

P. Liang, H. L. Lukas (1997)

Publication:

P. Liang, H. L. Lukas, H. J. Seifert, G. Ghosh, G. Effenberg, F. Aldinger,
in preparation for *Calphad* (1997)

Thermodynamic properties of the solution and compound phases (J.mol⁻¹)

Phase bcc-B2

$$G_{\text{Cu:Mg}}^* = 0.0$$

$$L_{\text{Cu,Mg}}^0 = -2500$$

$$G_{\text{Cu:Zn}}^* = 0.0$$

$$L_{\text{Cu,Zn}}^0 = -12898.97 + 3.26598 T$$

$$L_{\text{Cu,Zn}}^1 = 945.265 - 0.80679 T$$

$$L_{\text{Cu,Zn}}^2 = 1921.485 - 1.86969 T$$

$$G_{\text{Mg:Zn}}^* = 0.0$$

$$L_{\text{Mg,Zn}}^0 = -2500$$

$$L_{\text{Cu,Mg:Zn};\square}^{0,\text{bcc-B2}} = L_{\text{Zn:Cu,Mg};\square}^{0,\text{bcc-B2}} = -G_{\text{Cu:Mg}}^* + L_{\text{Cu,Mg}}^0 - L_{\text{Cu,Zn}}^1 + 0.5 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Mg:Zn};\square}^{1,\text{bcc-B2}} = L_{\text{Zn:Cu,Mg};\square}^{1,\text{bcc-B2}} = -0.5 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Mg};\square}^{0,\text{bcc-B2}} = L_{\text{Mg:Cu,Zn};\square}^{0,\text{bcc-B2}} = -G_{\text{Cu:Zn}}^* + L_{\text{Cu,Zn}}^0$$

$$L_{\text{Cu,Zn:Mg};\square}^{1,\text{bcc-B2}} = L_{\text{Mg:Cu,Zn};\square}^{1,\text{bcc-B2}} = L_{\text{Cu,Zn}}^1$$

$$L_{\text{Cu,Zn:Mg};\square}^{2,\text{bcc-B2}} = L_{\text{Mg:Cu,Zn};\square}^{2,\text{bcc-B2}} = L_{\text{Cu,Zn}}^2$$

$$L_{\text{Mg,Zn:Cu};\square}^{0,\text{bcc-B2}} = L_{\text{Cu:Mg,Zn};\square}^{0,\text{bcc-B2}} = -G_{\text{Mg:Zn}}^* + L_{\text{Mg,Zn}}^0 + L_{\text{Cu,Zn}}^1 + 0.5 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Mg,Zn:Cu};\square}^{1,\text{bcc-B2}} = L_{\text{Cu:Mg,Zn};\square}^{1,\text{bcc-B2}} = 0.5 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Mg,Zn:Cu,Zn};\square}^{0,\text{bcc-B2}} = L_{\text{Cu,Zn:Mg,Zn};\square}^{0,\text{bcc-B2}} = -5 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Mg,Zn:Cu,Mg};\square}^{0,\text{bcc-B2}} = L_{\text{Cu,Mg:Mg,Zn};\square}^{0,\text{bcc-B2}} = -2 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Cu,Mg};\square}^{0,\text{bcc-B2}} = L_{\text{Cu,Mg:Cu,Zn};\square}^{0,\text{bcc-B2}} = -5 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Mg,Zn:Cu};\square}^{0,\text{bcc-B2}} = L_{\text{Cu:Cu,Mg,Zn};\square}^{0,\text{bcc-B2}} = 1.5 L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Mg,Zn:Zn};\square}^{0,\text{bcc-B2}} = L_{\text{Zn:Cu,Mg,Zn};\square}^{0,\text{bcc-B2}} = 1.5 L_{\text{Cu,Zn}}^2$$

Phase bcc-A2

$$L_{\text{Cu,Mg,Zn};\square}^{0,\text{bcc-A2}} = 0$$

$$L_{\text{Cu,Mg,Zn};\square}^{1,\text{bcc-A2}} = 0$$

$$L_{\text{Cu,Mg,Zn};\square}^{2,\text{bcc-A2}} = 0$$

Phase Mg₂Zn₁₁

$$L_{\text{Mg;Cu,Zn}}^{0,\text{Mg}_2\text{Zn}_{11}} = -351000$$

Phase Laves-C14

$$L_{\text{Mg,Zn;Cu}}^{0,\text{Laves-C14}} = 35000.00$$

$$L_{\text{Cu;Mg,Zn}}^{0,\text{Laves-C14}} = 35000.00$$

$$L_{\text{Zn;Cu,Mg}}^{0,\text{Laves-C14}} = 6599.45$$

$$L_{\text{Cu,Mg;Zn}}^{0,\text{Laves-C14}} = 13011.35$$

$$L_{\text{Cu,Zn;Mg}}^{0,\text{Laves-C14}} = -75305.48$$

Phase Laves-C15

$$L_{\text{Cu,Mg;Zn}}^{0,\text{Laves-C15}} = 13011.35$$

$$L_{\text{Zn;Cu,Mg}}^{0,\text{Laves-C15}} = 6599.45$$

$$L_{\text{Mg,Zn;Cu}}^{0,\text{Laves-C15}} = 35000.00$$

$$L_{\text{Cu;Mg,Zn}}^{0,\text{Laves-C15}} = 8000.00$$

$$L_{\text{Cu,Zn;Mg}}^{0,\text{Laves-C15}} = -78824.62$$

$$L_{\text{Mg;Cu,Zn}}^{0,\text{Laves-C15}} = 25529.06$$

Phase Laves-C36

$$L_{\text{Mg,Zn:Cu}}^{0,\text{Laves-C36}} = 35000.00$$

$$L_{\text{Cu:Mg,Zn}}^{0,\text{Laves-C36}} = 8000.00$$

$$L_{\text{Zn:Cu,Mg}}^{0,\text{Laves-C36}} = 6599.45$$

$$L_{\text{Cu,Mg:Zn}}^{0,\text{Laves-C36}} = 13011.35$$

$$L_{\text{Cu,Zn:Mg}}^{0,\text{Laves-C36}} = -90226.26$$

Phase Mg_2Zn_3

$$L_{\text{Mg:Cu,Zn}}^{0,\text{Mg}_2\text{Zn}_3} = -100000$$

Phase MgZn

$$L_{\text{Mg:Cu,Zn}}^{0,\text{MgZn}} = -575000$$

Phase CuZn- γ

$$K4 = -11552.71 - 1.67824 T$$

$$K5 = 15732.3 - 10.26575 T$$

$$K6 = 37289.2 - 13.05259 T$$

$$K7 = 9000.0 - 1.50000 T$$

$$13 K4 + 2 K5 + 2 K6 + 6 K7 = 9857.77 - 77.4538 T$$

$$13 K4 + 6 K7 = -96185.23 - 30.81712 T$$

$$13 K4 + 2 K6 + 6 K7 = -21606.83 - 56.9223 T$$

$$\begin{aligned} G^\circ(T) - 5.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) \\ - 2.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Zn:Cu:Cu:Mg}) = \\ 13.0 K4 + 2.0 K5 + 2.0 K6 + 6 K7 + 5.0 \text{GHSER}_{\text{Cu}} \\ + 6.0 \text{GHSER}_{\text{Mg}} + 2.0 \text{GHSER}_{\text{Zn}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 5.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) \\ - 2.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn:Cu:Mg}) = \\ 13.0 K4 + 6.0 K7 + 5.0 \text{GHSER}_{\text{Cu}} + 6.0 \text{GHSER}_{\text{Mg}} \\ + 2.0 \text{GHSER}_{\text{Zn}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) \\ - 4.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn:Cu:Mg}) = \\ 13.0 K4 + 2.0 K6 + 6.0 K7 + 3.0 \text{GHSER}_{\text{Cu}} + 6.0 \text{GHSER}_{\text{Mg}} \\ + 4.0 \text{GHSER}_{\text{Zn}} \end{aligned}$$

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Cu-Mg-Zn	(Cu)	Cu	<i>cF4</i> <i>Fm$\bar{3}$m</i>	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2	
	(Zn)	Mg	<i>hP2</i> <i>P6$_3$/mmc</i>	M 2	
	CuMg ₂	CuMg ₂	<i>oF48</i> <i>Fddd</i>	Cu 16 Mg1 16 Mg2 16	
	Cu ₂ Mg	Cu ₂ Mg	<i>cF24</i> <i>Fd$\bar{3}$m</i>	Cu 16 Mg 8	Laves-C15
	Laves-C36	MgNi ₂	<i>hP24</i> <i>P6$_3$/mmc</i>	Cr ₁ 6 Cr ₂ 6 Zr ₁ 3 Zr ₂ 3	Laves-C36
	Laves-C14	MgZn ₂	<i>hP12</i> <i>P6$_3$/mmc</i>	Cr 2 Cr 6 Zr 4	Laves-C14
	γ	Cu ₅ Zn ₈	<i>cI52</i> <i>I$\bar{4}$3m</i>	Cu ₁ 8 Cu ₂ 12 Zn ₁ 8 Zn ₂ 24	Cu ₅ Zn
	Mg ₂ Zn ₁₁	Mg ₂ Zn ₁₁	<i>cP39</i> <i>Pm$\bar{3}$</i>		
	MgZn				
Mg ₂ Zn ₃		<i>mC110</i> <i>B2/m</i>			

APPENDICES

APPENDIX I: THERMODYNAMIC PROPERTIES OF THE ELEMENTS
($J \cdot mol^{-1}$)

NOTE: The Gibbs Energies of Formation at T are relative to the Enthalpy of the Pure Elements in their Reference Phase at 298.15 K ¹

ALUMINIUM

Aluminium fcc-A1

$$GHSE_{Al} = G_{Al}^{fcc-A1}(T) - H_{Al}^{o,fcc-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 700.00 : -7976.15 + 137.093038 T - 24.3671976 T \cdot \ln T \\ - 1.884662E-3 T^2 - 0.877664E-6 T^3 \\ + 74092 T^{-1}$$

$$700.00 < T < 933.47 : -11276.24 + 223.048446 T - 38.5844296 T \cdot \ln T \\ + 18.531982E-3 T^2 - 5.764227E-6 T^3 \\ + 74092 T^{-1}$$

$$933.47 < T < 2900.00 : -11278.378 + 188.684153 T - 31.748192 T \cdot \ln T \\ - 1230.524E25 T^{-9}$$

Aluminium bcc-A2

$$GBCC_{Al} = G_{Al}^{bcc-A2}(T) - H_{Al}^{o,fcc-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : 10083.00 - 4.813 T + GHSE_{Al}$$

Aluminium cbcc-A12

$$G_{Al}^{cbcc-A12}(T) - H_{Al}^{o,fcc-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : 10083.40 - 4.813 T + GHSE_{Al}$$

Aluminium bcc-B2

$$G_{Al:Al}^{bcc-B2}(T) - H_{Al}^{o,fcc-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : GBCC_{Al}$$

Aluminium bct-A5

$$G_{Al}^{bct-A5}(T) - H_{Al}^{o,fcc-A1} =$$

$$298.15 < T < 2900.00 : 10083.0 - 4.813 T + GHSE_{Al}$$

¹Scientific Group Thermodata Europe (S.G.T.E.) Data for Pure Elements, A.T. Dinsdale, CAL-PHAD, 15, 4, 317 - 425 (1991).

Aluminium cub-A13

$$G_{\text{Al}}^{\text{cub-A13}}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}} =$$

$$298.15 < T < 2900.00 : 10920.44 - 4.8116 T + \text{GHSER}_{\text{Al}}$$

Aluminium diamond

$$G_{\text{Al}}^{\text{diamond}}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : 30.0 T + \text{GHSER}_{\text{Al}}$$

Aluminium hcp-A3

$$\text{GHCP}_{\text{Al}} = G_{\text{Al}}^{\text{hcp-A3}}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : 5481.0 - 1.8 T + \text{GHSER}_{\text{Al}}$$

Aluminium hcp-Zn

$$G_{\text{Al}}^{\text{hcp-Zn}}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 5482 - 1.8 T + \text{GHSER}_{\text{Al}}$$

Aluminium liquid

$$\text{GLIQ}_{\text{Al}} = G_{\text{Al}}^{\text{liquid}}(T) - H_{\text{Al}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 933.47 : + 11005.029 - 11.841867 T + 7.934\text{E-}20 T^7 \\ + \text{GHSER}_{\text{Al}}$$

$$933.47 < T < 2900.00 : + 10482.382 - 11.253974 T + 1.231\text{E+}28 T^{-9} \\ + \text{GHSER}_{\text{Al}}$$

BORON**Boron β -rhombo-B**

$$\text{GHSER}_{\text{B}} = G_{\text{B}}^{\beta\text{-rhombo-B}}(T) - H_{\text{B}}^{\circ, \beta\text{-rhombo-B}}(298.15 \text{ K}) =$$

$$298.15 < T < 1100.00 : - 7735.284 + 107.111864 T - 15.6641 T \cdot \ln T \\ - 0.006864515 T^2 + 6.18878\text{E-}07 T^3 \\ + 370843 T^{-1}$$

$$1100.00 < T < 2348.00 : - 16649.474 + 184.801744 T - 26.6047 T \cdot \ln T \\ - 7.9809\text{E-}04 T^2 - 2.556\text{E-}08 T^3 \\ + 1748270 T^{-1}$$

$$2348.00 < T < 3000.00 : - 36667.582 + 231.336244 T - 31.5957527 T \cdot \ln T \\ - 0.00159488 T^2 + 1.34719\text{E-}07 T^3 \\ + 11205883 T^{-1}$$

$$3000.00 < T < 6000.00 : - 21530.653 + 222.396264 T - 31.4 T \cdot \ln T$$

$$\text{GBCC}_B = G_B^{\text{bcc-A2}}(T) - H_B^{\circ, \beta\text{-rhombo-B}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 50208.0 - 13.472 T + \text{GHSER}_B$$

Boron diamond

$$G_B^{\text{diamond}}(T) - H_B^{\circ, \beta\text{-rhombo-B}} =$$

$$298.15 < T < 6000.00 : 20 + \text{GHSER}_B$$

Boron fcc-A1

$$\text{GFCC}_B = G_B^{\text{fcc-A1}}(T) - H_B^{\circ, \beta\text{-rhombo-B}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 43514.0 - 12.217 T + \text{GHSER}_B$$

Boron hcp-A3

$$\text{GHCP}_B = G_B^{\text{hcp-A3}}(T) - H_B^{\circ, \beta\text{-rhombo-B}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 50208.0 - 9.706 T + \text{GHSER}_B$$

Boron liquid

$$\text{GLIQ}_B = G_B^{\text{liquid}}(T) - H_B^{\circ, \beta\text{-rhombo-B}}(298.15 \text{ K}) =$$

$$298.15 < T < 500.00 : 40723.275 + 86.843839 T - 15.6641 T \cdot \ln T$$

$$- 0.006864515 T^2 + 6.18878\text{E-}07 T^3$$

$$+ 370843 T^{-1}$$

$$500.00 < T < 2348.00 : 41119.703 + 82.101722 T - 14.9827763 T \cdot \ln T$$

$$- 0.007095669 T^2 + 5.07347\text{E-}07 T^3$$

$$+ 335484 T^{-1}$$

$$2348.00 < T < 6000.00 : + 28842.012 + 200.94731 T - 31.4 T \cdot \ln T$$

CARBON**Carbon graphite**

$$\text{GHSER}_C = G_C^{\text{graphite}}(T) - H_C^{\circ, \text{graphite}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : - 17368.441 + 170.73 T - 24.3 T \cdot \ln T$$

$$- 4.723\text{E-}04 T^2 + 2562600 T^{-1} - 2.643\text{E+}08 T^{-2}$$

$$+ 1.2\text{E+}10 T^{-3}$$

Carbon diamond

$$G_C^{\text{diamond}}(T) - H_C^{\circ, \text{graphite}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : - 16359.441 + 175.61 T - 24.31 T \cdot \ln T$$

$$- 4.723\text{E-}04 T^2 + 2698000 T^{-1} - 2.61\text{E+}08 T^{-2}$$

$$+ 1.11\text{E+}10 T^{-3}$$

Carbon liquid

$$GLIQ_C = G_C^{\text{liquid}}(T) - H_C^{\circ, \text{graphite}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 117369 - 24.63 T + GHSE_{C_c}$$

CERIUM**Cerium fcc-A1**

$$GHSE_{C_{ce}} = G_{C_{ce}}^{\text{fcc-A1}}(T) - H_{C_{ce}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : -7160.519 + 84.23022 T - 22.3664 T \cdot \ln T$$

$$\quad \quad \quad - 0.0067103 T^2 - 3.20773E-07 T^3 - 18117 T^{-1}$$

$$1000.00 < T < 2000.00 : -79678.506 + 659.4604 T - 101.32248 T \cdot \ln T$$

$$\quad \quad \quad + 0.026046487 T^2 - 1.9302976E-06 T^3 + 11531707 T^{-1}$$

$$2000.00 < T < 4000.00 : -14198.639 + 190.370192 T - 37.6978 T \cdot \ln T$$

Cerium bcc-A2

$$GBCC_{C_{ce}} = G_{C_{ce}}^{\text{bcc-A2}}(T) - H_{C_{ce}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : -1354.69 - 5.21501 T - 7.7305867 T \cdot \ln T$$

$$\quad \quad \quad - 0.029098402 T^2 + 4.784299E-06 T^3 - 196303 T^{-1}$$

$$1000.00 < T < 1072.00 : -12101.106 + 187.449688 T - 37.6142 T \cdot \ln T$$

$$1072.00 < T < 6000.00 : -11950.375 + 186.333811 T - 37.4627992 T \cdot \ln T$$

$$\quad \quad \quad - 5.7145E-05 T^2 + 2.348E-09 T^3 - 25897 T^{-11}$$

Cerium dhcp

$$G_{C_{ce}}^{\text{dhcp}}(T) - H_{C_{ce}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 4000.00 : -190.0 + 0.56886 T + GHSE_{C_{ce}}$$

Cerium hcp-A3

$$GHCP_{C_{ce}} = G_{C_{ce}}^{\text{hcp-A3}}(T) - H_{C_{ce}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 4000.00 : 50000 + GHSE_{C_{ce}}$$

Cerium liquid

$$GLIQ_{C_{ce}} = G_{C_{ce}}^{\text{liquid}}(T) - H_{C_{ce}}^{\circ, \text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : 4117.865 - 11.423898 T - 7.5383948 T \cdot \ln T$$

$$\quad \quad \quad - 0.02936407 T^2 + 4.827734E-06 T^3 - 198834 T^{-1}$$

$$1000.00 < T < 4000.00 : -6730.605 + 183.023193 T - 37.6978 T \cdot \ln T$$

CHROMIUM

Chromium bcc-A2(paramagnetic)

$$\begin{aligned}
 \text{GHSER}_{\text{Cr}} &= G_{\text{Cr}}^{\text{bcc-A2,para}}(T) - H_{\text{Cr}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\
 298.15 < T < 2180.00 &: -8856.94 + 157.48 T - 26.908 T \cdot \ln T \\
 &\quad + 1.89435\text{E-}3 T^2 - 1.47721\text{E-}6 T^3 + 139250 T^{-1} \\
 2180.00 < T < 6000.00 &: -34869.344 + 344.18 T - 50 T \cdot \ln T \\
 &\quad - 2885.26\text{E}29 T^{-9}
 \end{aligned}$$

Chromium cbcc-A12

$$\begin{aligned}
 G_{\text{Cr}}^{\text{cbcc-A12,para}}(T) - H_{\text{Cr}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) &= \\
 298.15 < T < 6000.00 &: 11087.0 + 2.7196 T + \text{GHSER}_{\text{Cr}}
 \end{aligned}$$

Chromium cub-A13

$$\begin{aligned}
 G_{\text{Cr}}^{\text{cub-A13}}(T) - H_{\text{Cr}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) &= \\
 298.15 < T < 6000.00 &: 15899.0 + 0.6276 T + \text{GHSER}_{\text{Cr}}
 \end{aligned}$$

Chromium fcc-A1(paramagnetic)

$$\begin{aligned}
 \text{GFCC}_{\text{Cr}} &= G_{\text{Cr}}^{\text{fcc-A1}}(T) - H_{\text{Cr}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\
 298.15 < T < 6000.00 &: 7284.0 + 0.163 T + \text{GHSER}_{\text{Cr}} +
 \end{aligned}$$

Chromium hcp-A3(paramagnetic)

$$\begin{aligned}
 \text{GHCP}_{\text{Cr}} &= G_{\text{Cr}}^{\text{hcp-A3}}(T) - H_{\text{Cr}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\
 298.15 < T < 6000.00 &: 4438.00 + \text{GHSER}_{\text{Cr}} +
 \end{aligned}$$

Chromium liquid

$$\begin{aligned}
 \text{GLIQ}_{\text{Cr}} &= G_{\text{Cr}}^{\text{liquid}}(T) - H_{\text{Cr}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\
 298.15 < T < 2180.00 &: 24339.955 - 11.420225 T + 2.37615\text{E-}21 T^7 \\
 &\quad + \text{GHSER}_{\text{Cr}} \\
 2180.00 < T < 6000.00 &: 18409.36 - 8.563683 T + 2.88526\text{E+}32 T^{-9} \\
 &\quad + \text{GHSER}_{\text{Cr}}
 \end{aligned}$$

Chromium Laves-C14

$$\begin{aligned}
 G_{\text{Cr:Cr}}^{\text{Cr,Laves-C14}} - 3.0 H_{\text{Cr}}^{\text{o,bcc-A2}}(298.15 \text{ K}) &= \\
 298.15 < T < 6000.00 &: 15000.0 + 3.0 \text{GHSER}_{\text{Cr}}
 \end{aligned}$$

Chromium Laves-C15

$$\begin{aligned}
 G_{\text{Cr:Cr}}^{\text{Cr,Laves-C15}} - 3.0 H_{\text{Cr}}^{\text{o,bcc-A2}}(298.15 \text{ K}) &= \\
 298.15 < T < 6000.00 &: 15000.0 + 3.0 \text{GHSER}_{\text{Cr}}
 \end{aligned}$$

Chromium Laves-C36

$$G_{\text{Cr:Cr}}^{\text{Cr,Laves-C36}} - 3.0 H_{\text{Cr}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 15000.0 + 3.0 \text{ GHSER}_{\text{Cr}}$$

COPPER**Copper fcc-A1**

$$\text{GHSE}_{\text{Cu}} = G_{\text{Cu}}^{\text{fcc-A1}}(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 1357.77 : -7770.458 + 130.485235 T - 24.112392 T \cdot \ln T$$

$$- 2.65684\text{E-}3 T^2 + 0.129223\text{E-}6 T^3 + 52478 T^{-1}$$

$$1357.77 < T < 3200.00 : -13542.026 + 183.803828 T - 31.38 T \cdot \ln T$$

$$+ 364.167\text{E}27 T^{-9}$$

Copper bcc-A2

$$\text{GBCC}_{\text{Cu}} = G_{\text{Cu}}^{\text{bcc-A2}}(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 3200.00 : 4017.00 - 1.255 T + \text{GHSE}_{\text{Cu}}$$

Copper hcp-A3

$$\text{GHCP}_{\text{Cu}} = G_{\text{Cu}}^{\text{hcp-A3}}(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 3200.00 : 600.0 + 0.2 T + \text{GHSE}_{\text{Cu}}$$

Copper liquid

$$\text{GLIQ}_{\text{Cu}} = G_{\text{Cu}}^{\text{liquid}}(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 1357.77 : 12964.736 - 9.511904 T - 5.849\text{E-}21 T^7$$

$$+ \text{GHSE}_{\text{Cu}}$$

$$1357.77 < T < 3200.00 : 13495.481 - 9.922344 T - 3.642\text{E+}29 T^9$$

$$+ \text{GHSE}_{\text{Cu}}$$

IRON**Iron bcc-A2(paramagnetic)**

$$\text{GHSE}_{\text{Fe}} = G_{\text{Fe}}^{\text{bcc-A2,para}}(T) - H_{\text{Fe}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1811.00 : 1225.7 + 124.134 T - 23.5143 T \cdot \ln T$$

$$- 4.39752\text{E-}3 T^2 - 0.058927\text{E-}6 T^3 + 77359 T^{-1}$$

$$1811.00 < T < 6000.00 : -25383.581 + 299.31255 T - 46 T \cdot \ln T \\ + 2296.03E28 T^{-9}$$

Iron bcc-A12

$$G_{\text{Fe}}^{\text{bcc-A12}}(T) - H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : +4745 + \text{GHSER}_{\text{Fe}}$$

Iron cub-A13

$$G_{\text{Fe}}^{\text{cub-A13}}(T) - H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 3745 + \text{GHSER}_{\text{Fe}}$$

Iron fcc-A1(paramagnetic)

$$\text{GFCC}_{\text{Fe}} = G_{\text{Fe}}^{\text{fcc-A1}}(T) - H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1811.00 : -1462.4 + 8.8282 T - 1.15 T \cdot \ln T \\ + 0.00064 T^2 + \text{GHSER}_{\text{Fe}}$$

$$1811.00 < T < 6000.00 : -713.815 + 0.94001 T \\ + 0.49251 T^{-9} + \text{GHSER}_{\text{Fe}}$$

Iron hcp-A3

$$\text{GHCP}_{\text{Fe}} = G_{\text{Fe}}^{\text{hcp-A3}}(T) - H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1811.00 : -3705.78 + 12.591 T - 1.15 T \cdot \ln T \\ + 6.4E-04 T^2 + \text{GHSER}_{\text{Fe}}$$

$$1811.00 < T < 6000.00 : -3957.199 + 5.24951 T + 4.9251E+30 T^{-9} \\ + \text{GHSER}_{\text{Fe}}$$

Iron liquid

$$\text{GLIQ}_{\text{Fe}} = G_{\text{Fe}}^{\text{liquid}}(T) - H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1811.00 : +12040.17 - 6.55843 T - 3.67516E-21 T^7 \\ + \text{GHSER}_{\text{Fe}}$$

$$1811.00 < T < 6000.00 : +14544.751 - 8.01055 T - 2.29603E+31 T^{-9} \\ + \text{GHSER}_{\text{Fe}}$$

HAFNIUM**Hafnium hcp-A3**

$$\text{GHSEr}_{\text{Hf}} = G_{\text{Hf}}^{\text{hcp-A3}}(T) - H_{\text{Hf}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 2506.00 : -6987.297 + 110.744026 T - 22.7075 T \cdot \ln T \\ - 0.004146145 T^2 - 4.77E-10 T^3 - 22590 T^{-1}$$

$$2506.00 < T < 6000.00 : -1446776.33 + 6193.60999 T - 787.536383 T \cdot \ln T \\ + 0.1735215 T^2 - 7.575759E-06 T^3 \\ + 5.01742495E+08 T^{-1}$$

Hafnium bcc-A2

$$GBCC_{\text{Hf}} = G_{\text{Hf}}^{\text{bcc-A2}}(T) - H_{\text{Hf}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 2506.00 : 5370.703 + 103.836026 T - 22.8995 T \cdot \ln T \\ - 0.004206605 T^2 + 8.71923E-07 T^3 - 22590 T^{-1} \\ - 1.446E-10 T^4$$

$$2506.00 < T < 6000.00 : + 1912456.77 - 8624.20573 T + 1087.61412 T \cdot \ln T \\ - 0.286857065 T^2 + 1.3427829E-05 T^3 \\ - 6.10085091E+08 T^{-1}$$

Hafnium fcc-A1

$$GFCC_{\text{Hf}} = G_{\text{Hf}}^{\text{fcc-A1}}(T) - H_{\text{Hf}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 10000 - 2.2 T + \text{GHSER}_{\text{Hf}}$$

Hafnium liquid

$$GLIQ_{\text{Hf}} = G_{\text{Hf}}^{\text{liquid}}(T) - H_{\text{Hf}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : 20414.959 + 99.790933 T - 22.7075 T \cdot \ln T \\ - 0.004146145 T^2 - 4.77E-10 T^3 - 22590 T^{-1}$$

$$1000.00 < T < 2506.00 : 49731.499 - 149.91739 T + 12.116812 T \cdot \ln T \\ - 0.021262021 T^2 + 1.376466E-06 T^3 - 4449699 T^{-1}$$

$$2506.00 < T < 6000.00 : -4247.217 + 265.470523 T - 44 T \cdot \ln T$$

LITHIUM**Lithium bcc-A2**

$$\text{GHSER}_{\text{Li}} = G_{\text{Li}}^{\text{bcc-A2}}(T) - H_{\text{Li}}^{\text{o,bcc-A2}}(298.15 \text{ K}) =$$

$$200.00 < T < 453.60 : -10583.817 + 217.637482 T - 38.940488 T \cdot \ln T \\ + 35.466931E-3 T^2 - 19.869816E-6 T^3 + 159994 T^{-1}$$

$$453.60 < T < 500.00 : -559579.123 + 10547.879893 T \\ - 1702.8886493 T \cdot \ln T \\ + 2258.329444E-3 T^2 - 571.066077E-6 T^3 \\ + 33885874 T^{-1}$$

$$500.00 < T < 3000.00 : -9062.994 + 179.278285 T - 31.2283718 T \cdot \ln T \\ + 2.633221E-3 T^2 - 0.438058E-6 T^3 - 102387 T^{-1}$$

Lithium fcc-A1

$$\text{GFCC}_{\text{Li}} = G_{\text{Li}}^{\text{fcc-A1}}(T) - H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$200.00 < T < 3000.00 : -108 + 1.3 T + \text{GHSE}_{\text{Li}}$$

Lithium hcp-A3

$$\text{GHCP}_{\text{Li}} = G_{\text{Li}}^{\text{hcp-A3}}(T) - H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$200.00 < T < 3000.00 : -154 + 2 T + \text{GHSE}_{\text{Li}}$$

Lithium liquid

$$\text{GLIQ}_{\text{Li}} = G_{\text{Li}}^{\text{liquid}}(T) - H_{\text{Li}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$200.00 < T < 250.00 : -7883.612 + 211.841861 T - 38.940488 T \cdot \ln T$$

$$+ 35.466931\text{E-}3 T^2 - 19.869816\text{E-}6 T^3$$

$$+ 159994 T^{-1}$$

$$250.00 < T < 453.60 : 12015.027 - 362.187078 T + 61.6104424 T \cdot \ln T$$

$$- 182.426463\text{E-}3 T^2 + 63.955671\text{E-}6 T^3$$

$$- 559968 T^{-1}$$

$$453.60 < T < 3000.00 : -6057.31 + 172.652183 T - 31.2283718 T \cdot \ln T$$

$$+ 2.633221\text{E-}3 T^2 - 0.438058\text{E-}6 T^3$$

$$- 102387 T^{-1}$$

MAGNESIUM**Magnesium hcp-A3**

$$\text{GHSE}_{\text{Mg}} = G_{\text{Mg}}^{\text{hcp-A3}}(T) - H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 923.00 : -8367.34 + 143.675547 T - 26.1849782 T \cdot \ln T$$

$$+ 0.4858\text{E-}3 T^2 - 1.393669\text{E-}6 T^3 + 78950 T^{-1}$$

$$923.00 < T < 3000.00 : -14130.185 + 204.716215 T - 34.3088 T \cdot \ln T$$

$$+ 1038.192\text{E}25 T^{-9}$$

Magnesium bcc-A2

$$\text{GBCC}_{\text{Mg}} = G_{\text{Mg}}^{\text{bcc-A2}}(T) - H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 3000.00 : 3100.00 - 2.1 T + \text{GHSE}_{\text{Mg}}$$

Magnesium cbcc-A12

$$G_{\text{Mg}}^{\text{cbcc-A12}}(T) - H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 3000.00 : 4602.4 - 3.011 T + \text{GHSE}_{\text{Mg}}$$

Magnesium cub-A13

$$G_{\text{Mg}}^{\text{cub-A13}}(T) - H_{\text{Mg}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 3000.00 : 5000.0 - 3.0 T + \text{GHSER}_{\text{Mg}}$$

Magnesium fcc-A1

$$\text{GFCC}_{\text{Mg}} = G_{\text{Mg}}^{\text{fcc-A1}}(T) - H_{\text{Mg}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 3000.00 : 2600 - 0.90 T + \text{GHSER}_{\text{Mg}}$$

Magnesium liquid

$$\text{GLIQ}_{\text{Mg}} = G_{\text{Mg}}^{\text{liquid}}(T) - H_{\text{Mg}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 923.00 : 8202.243 - 8.83693 T + \text{GHSER}_{\text{Mg}} - 8.0176\text{E-}20 T^7 \\ + \text{GHSER}_{\text{Mg}}$$

$$923.00 < T < 3000.00 : 8690.316 - 9.392158 T - 1.038192\text{E+}28 T^{-9} \\ + \text{GHSER}_{\text{Mg}}$$

MANGANESE**Manganese bcc-A12(paramagnetic)**

$$\text{GHSER}_{\text{Mn}} = G_{\text{Mn}}^{\text{bcc-A12,para}}(T) - H_{\text{Mn}}^{\text{o,bcc-A12,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1519.00 : -8115.28 + 130.059 T - 23.4582 T \cdot \ln T \\ - 7.34768\text{E-}3 T^2 + 69827 T^{-1}$$

$$1519.00 < T < 3000.00 : -28733.41 + 312.2648 T - 48 T \cdot \ln T \\ + 1656.847\text{E+}27 T^{-9}$$

Manganese bcc-A2(paramagnetic)

$$\text{GBCC}_{\text{Mn}} = G_{\text{Mn}}^{\text{bcc-A2,para}}(T) - H_{\text{Mn}}^{\text{o,bcc-A12,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1519.00 : -3235.3 + 127.85 T - 23.7 T \cdot \ln T \\ - 7.44271\text{E-}3 T^2 + 60000 T^{-1}$$

$$1519.00 < T < 3000.00 : -23188.83 + 307.7043 T - 48 T \cdot \ln T \\ + 1265.152\text{E}27 T^{-9}$$

Manganese fcc-A1(paramagnetic)

$$\text{GFCC}_{\text{Mn}} = G_{\text{Mn}}^{\text{fcc-A1,para}}(T) - H_{\text{Mn}}^{\text{o,bcc-A12,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1519.00 : -3439.3 + 131.884 T - 24.5177 T \cdot \ln T \\ - 6\text{E-}3 T^2 + 69600 T^{-1}$$

$$298.15 < T < 1519.00 : -26070.1 + 309.6664 T - 48 T \cdot \ln T \\ + 386.196\text{E}28 T^{-9}$$

Manganese Laves-C15

$$G_{\text{Mn:Mn}}^{\text{Laves-C15}} - 3.0 H_{\text{Mn}}^{\text{o,bcc-A12,para}}(298.15 \text{ K}) =$$

$$298.15 < T < 3000.00 : 3000.0 + 3.0 \text{GHSER}_{\text{Mn}}$$

Manganese cub-A13

$$G_{\text{Mn}}^{\text{cub-A13}}(T) - H_{\text{Mn}}^{\text{o,ccbcc-A12,para}}(298.15 \text{ K}) =$$

298.15	< T <	1519.00	:	+ 2314.88 + 5.936 T - 1.4203 T · lnT + 1.51409E-03 T ² + 442.0 T ⁻¹ + GHSER _{Mn}
1519.00		3000.00	:	+ 442.65 - 0.9715 T + 2.3107229E+30 T ⁻⁹ + GHSER _{Mn}

Manganese hcp-A3(paramagnetic)

$$GHCP_{\text{Mn}} = G_{\text{Mn}}^{\text{hcp-A3,para}}(T) - H_{\text{Mn}}^{\text{o,ccbcc-A12,para}}(298.15 \text{ K}) =$$

298.15	< T <	1519.00	:	- 4439.3 + 133.007 T - 24.5177 T · lnT - 6E-3 T ² + 69600 T ⁻¹
1519.00		6000.00	:	- 27070.1 + 310.7894 T - 48 T · lnT + 386.196E28 T ⁻⁹

Manganese liquid

$$GLIQ_{\text{Mn}} = G_{\text{Mn}}^{\text{liquid}}(T) - H_{\text{Mn}}^{\text{o,ccbcc-A12,para}}(298.15 \text{ K}) =$$

298.15	< T <	1519.00	:	17859.91 - 12.6208 T - 4.41929E-21 T ⁷ + GHSER _{Mn}
1519.00		3000.00	:	18739.51 - 13.2288 T - 1.656847E+30 T ⁻⁹ + GHSER _{Mn}

MOLYBDENUM**Molybdenum bcc-A2**

$$GHSER_{\text{Mo}} = G_{\text{Mo}}^{\text{bcc-A2}}(T) - H_{\text{Mo}}^{\text{o,bcc-A2}}(298.15 \text{ K}) =$$

298.15	< T <	2896.00	:	- 7746.302 + 131.9197 T - 23.56414 T · lnT - 0.003443396 T ² + 5.66283E-07 T ³ + 65812 T ⁻¹ - 1.30927E-10 T ⁴
2896.00		5000.00	:	- 30556.41 + 283.559746 T - 42.63829 T · lnT - 4.849315E+33 T ⁻⁹

Molybdenum fcc-A1

$$GFCC_{\text{Mo}} = G_{\text{Mo}}^{\text{fcc-A1}}(T) - H_{\text{Mo}}^{\text{o,bcc-A2}}(298.15 \text{ K}) =$$

298.15	< T <	2896.00	:	7453.698 + 132.5497 T - 23.56414 T · lnT - 0.003443396 T ² + 5.66283E-07 T ³ + 65812 T ⁻¹ - 1.30927E-10 T ⁴
2896.00		5000.00	:	- 15356.41 + 284.189746 T - 42.63829 T · lnT - 4.849315E+33 T ⁻⁹

Molybdenum hcp-A3

$$\text{GHCP}_{\text{Mo}} = G_{\text{Mo}}^{\text{hcp-A3}}(T) - H_{\text{Mo}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 5000.00 : 11550 + \text{GHSER}_{\text{Mo}}$$

Molybdenum liquid

$$\text{GLIQ}_{\text{Mo}} = G_{\text{Mo}}^{\text{liquid}}(T) - H_{\text{Mo}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 2896.00 : 34085.045 + 117.224788 T - 23.56414 T \cdot \ln T$$

$$- 0.003443396 T^2 + 5.66283\text{E-}07 T^3 + 65812 T^{-1}$$

$$- 1.30927\text{E-}10 T^4 + 4.24519\text{E-}22 T^7$$

$$2896.00 < T < 5000.00 : 3538.963 + 271.6697 T - 42.63829 T \cdot \ln T$$

NITROGEN**Nitrogen gas**

$$\text{GHSER}_{\text{N}} = G_{\text{N}}^{\text{gas}}(T) - H_{0.5\text{N}_2}^{\circ}(298.15 \text{ K}) =$$

$$298.15 < T < 950.00 : - 3750.675 - 9.45425 T - 12.7819 T \cdot \ln T$$

$$- 0.00176686 T^2 + 2.681\text{E-}09 T^3 - 32374 T^{-1}$$

$$950.00 < T < 3350.00 : - 7358.85 + 17.2003 T - 16.3699 T \cdot \ln T$$

$$- 6.5107\text{E-}04 T^2$$

$$+ 3.0097\text{E-}08 T^3 + 563070 T^{-1}$$

$$3350.00 < T < 6000.00 : - 16392.8 + 50.26 T - 20.4695 T \cdot \ln T$$

$$+ 2.39754\text{E-}04 T^2 - 8.333\text{E-}09 T^3 + 4596375 T^{-1}$$

Nitrogen liquid

$$\text{GLIQ}_{\text{N}} = G_{\text{N}}^{\text{liquid}}(T) - H_{0.5\text{N}_2}^{\circ}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 29950 + 59.02 T + \text{GHSER}_{\text{N}}$$

NEODYMIUM**Neodymium dhcp**

$$\text{GHSER}_{\text{Nd}} = G_{\text{Nd}}^{\text{dhcp}} - H_{\text{Nd}}^{\circ, \text{dhcp}}(298.15 \text{ K}) =$$

$$298.15 < T < 900.00 : - 8402.93 + 111.10239 T - 27.0858 T \cdot \ln T$$

$$+ 5.56125\text{E-}04 T^2 - 2.6923\text{E-}06 T^3 + 34887 T^{-1}$$

$$900.00 < T < 1128.00 : - 6984.083 + 83.662617 T - 22.7536 T \cdot \ln T$$

$$- 0.00420402 T^2 - 1.802\text{E-}06 T^3$$

$$1128.00 < T < 1799.00 : - 225610.846 + 1673.04075 T - 238.182873 T \cdot \ln T$$

$$+ 0.078615997 T^2 - 6.048207\text{E-}06 T^3 + 38810350 T^{-1}$$

$$1799.00 < T < 2000.00 : - 25742.331 + 276.257088 T - 48.7854 T \cdot \ln T$$

Neodymium bcc-A2

$$\begin{aligned}
 \text{GBCC}_{\text{Nd}} &= G_{\text{Nd}}^{\text{bcc-A2}} - H_{\text{Nd}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\
 298.15 < T < 400.00 &: -6965.635 + 110.556109 T - 27.0858 T \cdot \ln T \\
 &\quad + 5.56125\text{E-}04 T^2 - 2.6923\text{E-}06 T^3 + 34887 T^{-1} \\
 400.00 < T < 1128.00 &: +7312.2 - 153.033976 T + 14.9956777 T \cdot \ln T \\
 &\quad - 0.050479 T^2 + 7.287217\text{E-}06 T^3 - 831810 T^{-1} \\
 1128.00 < T < 1289.00 &: -18030.266 + 239.677322 T - 44.5596 T \cdot \ln T \\
 1289.00 < T < 1800.00 &: +334513.017 - 2363.9199 T + 311.409193 T \cdot \ln T \\
 &\quad - 0.156030778 T^2 + 1.2408421\text{E-}05 T^3 - 64319604 T^{-1}
 \end{aligned}$$

Neodymium liquid

$$\begin{aligned}
 \text{GLIQ}_{\text{Nd}} &= G_{\text{Nd}}^{\text{bcc-A2}} - H_{\text{Nd}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\
 298.15 < T < 300.00 &: -3351.187 + 109.517314 T - 27.0858 T \cdot \ln T \\
 &\quad + 5.56125\text{E-}04 T^2 - 2.6923\text{E-}06 T^3 + 34887 T^{-1} \\
 300.00 < T < 1128.00 &: +5350.01 - 86.593963 T + 5.357301 T \cdot \ln T \\
 &\quad - 0.046955463 T^2 + 6.860782\text{E-}06 T^3 - 374380 T^{-1} \\
 1128.00 < T < 1800.00 &: -16335.232 + 268.625903 T - 48.7854 T \cdot \ln T
 \end{aligned}$$

NICKEL**Nickel fcc-A1(paramagnetic)**

$$\begin{aligned}
 \text{GHSER}_{\text{Ni}} &= G_{\text{Ni}}^{\text{fcc-A1,para}} - H_{\text{Ni}}^{\circ, \text{fcc-A1,para}}(298.15 \text{ K}) = \\
 298.15 < T < 1728.00 &: -5179.159 + 117.854 T - 22.096 T \cdot \ln T \\
 &\quad - 0.0048407 T^2 \\
 1728.00 < T < 3000.00 &: -27840.655 + 279.135 T - 43.1 T \cdot \ln T \\
 &\quad + 1.12754\text{E+}31 T^{-9}
 \end{aligned}$$

Nickel bcc-A2(paramagnetic)

$$\begin{aligned}
 \text{GBCC}_{\text{Ni}} &= G_{\text{Ni}}^{\text{bcc-A2}} - H_{\text{Ni}}^{\circ, \text{fcc-A1,para}}(298.15 \text{ K}) = \\
 298.15 < T < 1300.00 &: +8715.084 - 3.556 T + \text{GHSER}_{\text{Ni}}
 \end{aligned}$$

Nickel hcp-A3(paramagnetic)

$$\begin{aligned}
 \text{GHCP}_{\text{Ni}} &= G_{\text{Ni}}^{\text{hcp-A3}} - H_{\text{Ni}}^{\circ, \text{fcc-A1,para}}(298.15 \text{ K}) = \\
 298.15 < T < 3000.00 &: +1046 + 1.2552 T + \text{GHSER}_{\text{Ni}}
 \end{aligned}$$

Nickel liquid

$$\begin{aligned}
 \text{GLIQ}_{\text{Ni}} &= G_{\text{Ni}}^{\text{liquid}} - H_{\text{Ni}}^{\circ, \text{fcc-A1,para}}(298.15 \text{ K}) = \\
 298.15 < T < 1300.00 &: 16414.686 - 9.397 T - 3.82318\text{E-}21 T^7 \\
 &\quad + \text{GHSER}_{\text{Ni}} \\
 1728.00 < T < 3000.00 &: 18290.88 - 10.537 T - 1.127554+31 T^{-9} \\
 &\quad + \text{GHSER}_{\text{Ni}}
 \end{aligned}$$

NIOBIUM

Niobium bcc-A2

$$\text{GHSER}_{\text{Nb}} = G_{\text{Nb}}^{\text{bcc-A2}}(T) - H_{\text{Nb}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 2750.00 & : -8519.353 + 142.045475 T - 26.4711 T \cdot \ln T \\ & \quad + 2.03475\text{E-}04 T^2 - 3.5012\text{E-}07 T^3 + 93399 T^{-1} \\ 2750.00 < T < 1000.00 & : -37669.3 + 271.720843 T - 41.77 T \cdot \ln T \\ & \quad + 1.528238\text{E+}32 T^{-9} \end{aligned}$$

Niobium fcc-A1

$$\text{GFCC}_{\text{Nb}} = G_{\text{Nb}}^{\text{fcc-A1}}(T) - H_{\text{Nb}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 13500 + 1.7 T + \text{GHSER}_{\text{Nb}}$$

Niobium hcp-A3

$$\text{GHCP}_{\text{Nb}} = G_{\text{Nb}}^{\text{hcp-A3}}(T) - H_{\text{Nb}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 5000.00 : 10000 + 2.4 T + \text{GHSER}_{\text{Nb}}$$

Niobium liquid

$$\text{GLIQ}_{\text{Nb}} = G_{\text{Nb}}^{\text{liquid}}(T) - H_{\text{Nb}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 2750.00 : 29781.555 - 10.816417 T \\ - 3.06098\text{E-}23 T^7$$

$$+ \text{GHSER}_{\text{Nb}}$$

$$298.15 < T < 2750.00 : 30169.9 - 10.9647 T - 1.52824\text{E+}32 T^{-9} \\ + \text{GHSER}_{\text{Nb}}$$

SILICON

Silicon diamond

$$\text{GHSER}_{\text{Si}} = G_{\text{Si}}^{\text{diamond}}(T) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 1687.00 & : -8162.609 + 137.236859 T - 22.8317533 T \cdot \ln T \\ & \quad - 1.912904\text{E-}3 T^2 - 0.003552\text{E-}6 T^3 + 176667 T^{-1} \\ 1687.00 < T < 3600.00 & : -9457.642 + 167.281367 T - 27.196 T \cdot \ln T \\ & \quad - 420.369\text{E}28 T^{-9} \end{aligned}$$

Silicon bcc-A2

$$\text{GBCC}_{\text{Si}} = G_{\text{Si}}^{\text{bcc-A2}}(T) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 1687.00 : 47000.0 - 22.5 T + \text{GHSER}_{\text{Si}}$$

Silicon cbcc-A12

$$G_{\text{Si}}^{\text{bcc-A12}}(T) - H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 50208.0 - 20.377 T + \text{GHSE}_{\text{Si}}$$

Silicon cub-A13

$$G_{\text{Si}}^{\text{cub-A13}}(T) - H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 47279.0 - 20.377 T + \text{GHSE}_{\text{Si}}$$

Silicon fcc-A1

$$G_{\text{Si}}^{\text{fcc-A1}}(T) - H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 51000.00 - 21.8 T + \text{GHSE}_{\text{Si}}$$

Silicon hcp-A3

$$G_{\text{Si}}^{\text{hcp-A3}}(T) - H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 49200 - 20.8 T + \text{GHSE}_{\text{Si}}$$

Silicon liquid

$$G_{\text{Si}}^{\text{liquid}}(T) - H_{\text{Si}}^{\text{o,diamond}}(298.15 \text{ K}) =$$

$$298.15 < T < 1687.00 : 50696.4 - 30.0994 T + 2.09307\text{E-}21 T^7$$

$$+ \text{GHSE}_{\text{Si}}$$

$$1687.00 < T < 6000.00 : 49828.2 - 29.5591 T + 4.20369\text{E+}30 T^{-9}$$

$$+ \text{GHSE}_{\text{Si}}$$

TANTALUM**Tantalum bcc-A2**

$$\text{GHSE}_{\text{Ta}} = G_{\text{Ta}}^{\text{bcc-A2}}(T) - H_{\text{Ta}}^{\text{o,bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 1300.00 : -7285.889 + 119.139858 T - 23.7592624 T \cdot \ln T$$

$$- 0.002623033 T^2 + 1.70109\text{E-}07 T^3 - 3293 T^{-1}$$

$$1300.00 < T < 2500.00 : -22389.955 + 243.88676 T - 41.137088 T \cdot \ln T$$

$$+ 0.006167572 T^2 - 6.55136\text{E-}07 T^3 + 2429586 T^{-1}$$

$$2500.00 < T < 3258.00 : +229382.886 - 722.59722 T + 78.5244752 T \cdot \ln T$$

$$- 0.017983376 T^2 + 1.95033\text{E-}07 T^3 - 93813648 T^{-1}$$

$$3258.00 < T < 6000.00 : -963392.734 + 2773.7774 T - 337.227976 T \cdot \ln T$$

$$+ 0.039791303 T^2 - 9.74251\text{E-}07 T^3$$

$$+ 5.09949511\text{E+}08 T^{-1}$$

Tantalum fcc-A1

$$\text{GFCC}_{\text{Ta}} = G_{\text{Ta}}^{\text{fcc-A1}}(T) - H_{\text{Ta}}^{\text{o,bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 16000 + 1.7 T + \text{GHSE}_{\text{Ta}}$$

Tantalum hcp-A3

$$\text{GHCP}_{\text{Ta}} = G_{\text{Ta}}^{\text{hcp-A3}}(T) - H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 12000 + 2.4 T + \text{GHSER}_{\text{Ta}}$$

Tantalum liquid

$$\text{GLIQ}_{\text{Ta}} = G_{\text{Ta}}^{\text{liquid}}(T) - H_{\text{Ta}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : 29160.975 - 7.578729 T + \text{GHSER}_{\text{Ta}}$$

$$1000.00 < T < 1300.00 : 51170.228 - 181.121652 T + 23.7872147 T \cdot \ln T - 0.009707033 T^2 + 4.4449\text{E-}07 T^3 - 3520045 T^{-1} + \text{GHSER}_{\text{Ta}}$$

$$1300.00 < T < 2500.00 : 66274.294 - 305.868555 T + 41.1650403 T \cdot \ln T - 0.018497638 T^2 + 1.269735\text{E-}06 T^3 - 5952924 T^{-1} + \text{GHSER}_{\text{Ta}}$$

$$2500.00 < T < 3290.00 : -185498.547 + 660.615425 T - 78.4965229 T \cdot \ln T + 0.00565331 T^2 + 4.19566\text{E-}07 T^3 + 90290310 T^{-1} + \text{GHSER}_{\text{Ta}}$$

$$3290.00 < T < 6000.00 : 1036069.47 - 2727.38037 T + 320.319132 T \cdot \ln T - 0.043117795 T^2 + 1.055148\text{E-}06 T^3 - 5.54714342\text{E+}08 T^{-1} + \text{GHSER}_{\text{Ta}}$$

TIN**Tin bct-A5**

$$\text{GHSER}_{\text{Sn}} = G_{\text{Sn}}^{\text{bct-A5}}(T) - H_{\text{Sn}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) =$$

$$100.00 < T < 250.00 : -7958.517 + 122.765451 T - 25.858 T \cdot \ln T + 0.51185\text{E-}3 T^2 - 3.192767\text{E-}6 T^3 + 18440 T^{-1}$$

$$250.00 < T < 505.078 : -5855.135 + 65.443315 T - 15.961 T \cdot \ln T - 18.8702\text{E-}3 T^2 + 3.121167\text{E-}6 T^3 - 61960 T^{-1}$$

$$505.078 < T < 800.00 : 2524.724 + 4.005269 T - 8.2590486 T \cdot \ln T - 16.814429\text{E-}3 T^2 + 2.623131\text{E-}6 T^3 - 1081244 T^{-1} - 123.07\text{E}23 T^{-9}$$

$$800.00 < T < 3000.00 : -8256.959 + 138.99688 T - 28.4512 T \cdot \ln T - 123.07\text{E}23 T^{-9}$$

Tin bcc-A2

$$\text{GBCC}_{\text{Sn}} = G_{\text{Sn}}^{\text{bcc-A2}}(T) - H_{\text{Sn}}^{\circ, \text{bct-A5}}(298.15 \text{ K}) =$$

$$100.00 < T < 3000.00 : 4400.00 - 6.0 T + \text{GHSER}_{\text{Sn}}$$

Tin fcc-A1

$$\text{GFCC}_{\text{Sn}} = G_{\text{Sn}}^{\text{fcc-A1}}(T) - H_{\text{Sn}}^{\circ, \text{bcc-A5}}(298.15 \text{ K}) =$$

$$100.00 < T < 3000.00 : 5510.0 - 8.46 T + \text{GHSE}_{\text{Sn}}$$

Tin hcp-A3

$$\text{GHCP}_{\text{Sn}} = G_{\text{Sn}}^{\text{bcc-A2}}(T) - H_{\text{Sn}}^{\circ, \text{bcc-A5}}(298.15 \text{ K}) =$$

$$100.00 T < 3000.00 : 3900.00 - 4.4 T + \text{GHSE}_{\text{Sn}}$$

Tin liquid

$$\text{GLIQ}_{\text{Sn}} = G_{\text{Sn}}^{\text{liquid}}(T) - H_{\text{Sn}}^{\circ, \text{bcc-A5}}(298.15 \text{ K}) =$$

$$100.00 < T < 505.078 : 7103.092 - 14.087767 T + 1.47031\text{E-}18T^7$$

$$+ \text{GHSE}_{\text{Sn}}$$

$$505.078 < T < 3000.00 : 6971.587 - 13.814382 T + 1.2307\text{E+}25 T^{-9}$$

$$+ \text{GHSE}_{\text{Sn}}$$

TITANIUM**Titanium hcp-A3**

$$\text{GHSE}_{\text{Ti}} = G_{\text{Ti}}^{\text{hcp-A3}}(T) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 900.00 : -8059.921 + 133.615208 T - 23.9933 T \cdot \ln T$$

$$- 4.777975\text{E-}3 T^2 + 0.106716\text{E-}6 T^3 + 72636 T^{-1}$$

$$900.00 < T < 1155.00 : -7811.815 + 132.988068 T - 23.9887 T \cdot \ln T$$

$$- 4.2033\text{E-}3 T^2 - 0.090876\text{E-}6 T^3 + 42680 T^{-1}$$

$$1155.00 < T < 1941.00 : 908.837 + 66.976538 T - 14.9466 T \cdot \ln T$$

$$- 8.1465\text{E-}3 T^2 + 0.202715\text{E-}6 T^3 - 1477660 T^{-1}$$

$$1941.00 < T < 4000.00 : -124526.786 + 638.806871 T - 87.2182461 T \cdot \ln T$$

$$+ 8.204849\text{E-}3 T^2 - 0.304747\text{E-}6 T^3$$

$$+ 36699805 T^{-1}$$

Titanium bcc-A2

$$\text{GBCC}_{\text{Ti}} = G_{\text{Ti}}^{\text{bcc-A2}}(T) - H_{\text{Ti}}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 1155.00 : -1272.064 + 134.71418 T - 25.5768 T \cdot \ln T$$

$$- 0.663845\text{E-}3 T^2 - 0.278803\text{E-}6 T^3 + 7208 T^{-1}$$

$$1155.00 < T < 1941.00 : 6667.385 + 105.366379 T - 22.3771 T \cdot \ln T$$

$$+ 1.21707\text{E-}3 T^2 - 0.84534\text{E-}6 T^3 - 2002750 T^{-1}$$

$$1941.00 < T < 4000.00 : 26483.26 - 182.426471 T + 19.0900905 T \cdot \ln T$$

$$- 22.00832\text{E-}3 T^2 + 1.228863\text{E-}6 T^3 + 1400501 T^{-1}$$

Titanium cbcc-A12

$$G_{\text{Ti}}^{\text{cbcc-A12}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 4602.2 + \text{GHSER}_{\text{Ti}}$$

Titanium bct-A5

$$G_{\text{Ti}}^{\text{bct-A5}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 4602.2 + \text{GHSER}_{\text{Ti}}$$

Titanium cub-A13

$$G_{\text{Ti}}^{\text{cub-A13}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 7531.2 + \text{GHSER}_{\text{Ti}}$$

Titanium diamond

$$G_{\text{Ti}}^{\text{diamond}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 25000.00 + \text{GHSER}_{\text{Ti}}$$

Titanium fcc-A1

$$G_{\text{Ti}}^{\text{fcc-A1}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 6000.0 - 0.1 T + \text{GHSER}_{\text{Ti}}$$

Titanium Laves-C14

$$G_{\text{Ti:Ti}}^{\text{Laves-C14}}(T) - 3.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 15000.0 + 3.0 \text{ GHSER}_{\text{Ti}}$$

Titanium Laves-C15

$$G_{\text{Ti:Ti}}^{\text{Laves-C14}}(T) - 3.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 15000.0 + 3.0 \text{ GHSER}_{\text{Ti}}$$

Titanium liquid

$$G_{\text{Ti}}^{\text{liquid}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 1300.00 : + 12194.415 - 6.980938 T + \text{GHSER}_{\text{Ti}}$$

$$1300.00 < T < 1941.00 : + 368610.36 - 2620.999038 T + 357.005867 T \cdot \ln T$$

$$- 155.262855\text{E-}03 T^2 + 12.254402\text{E-}06 T^3$$

$$- 65556856 T^{-1} + \text{GHSER}_{\text{Ti}}$$

$$1941.00 < T < 6000.00 : + 104639.72 - 340.070171 T + 40.9282461 T \cdot \ln T$$

$$- 8.204849\text{E-}03 T^2 + 0.304747\text{E-}06 T^3$$

$$- 36699805 T^{-1} + \text{GHSER}_{\text{Ti}}$$

TUNGSTEN

Tungsten bcc-A2

$$\begin{aligned} \text{GHSE}_{\text{W}} &= G_{\text{W}}^{\text{bcc-A2}}(T) - H_{\text{W}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ 298.15 < T < 3695.00 &: -7646.311 + 130.4 T - 24.1 T \cdot \ln T \\ &\quad - 0.001936 T^2 + 2.07\text{E-}07 T^3 + 44500 T^{-1} \\ &\quad - 5.33\text{E-}11 T^4 \\ 3695.00 < T < 6000.00 &: -82868.801 + 389.362335 T - 54 T \cdot \ln T \\ &\quad + 1.528621\text{E+}33 T^{-9} \end{aligned}$$

Tungsten fcc-A1

$$\begin{aligned} \text{GFCC}_{\text{W}} &= G_{\text{W}}^{\text{fcc-A1}}(T) - H_{\text{W}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ 298.15 < T < 3695.00 &: 11653.689 + 131.03 T - 24.1 T \cdot \ln T \\ &\quad - 0.001936 T^2 + 2.07\text{E-}07 T^3 + 44500 T^{-1} \\ &\quad - 5.33\text{E-}11 T^4 \\ 3695.00 < T < 6000.00 &: -63568.801 + 389.992335 T - 54 T \cdot \ln T \\ &\quad + 1.528621\text{E+}33 T^{-9} \end{aligned}$$

Tungsten hcp-A3

$$\begin{aligned} \text{GHCP}_{\text{W}} &= G_{\text{W}}^{\text{hcp-A3}}(T) - H_{\text{W}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ 298.15 < T < 3695.00 &: 7103.689 + 130.4 T - 24.1 T \cdot \ln T \\ &\quad - 0.001936 T^2 + 2.07\text{E-}07 T^3 + 44500 T^{-1} \\ &\quad - 5.33\text{E-}11 T^4 \\ 3695.00 < T < 6000.00 &: -68118.801 + 389.362335 T - 54 T \cdot \ln T \\ &\quad + 1.528621\text{E+}33 T^{-9} \end{aligned}$$

Tungsten liquid

$$\begin{aligned} \text{GLIQ}_{\text{W}} &= G_{\text{W}}^{\text{liquid}}(T) - H_{\text{W}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ 298.15 < T < 3695.00 &: 44514.273 + 116.29001 T - 24.1 T \cdot \ln T \\ &\quad - 0.001936 T^2 + 2.07\text{E-}07 T^3 + 44500 T^{-1} \\ &\quad - 5.33\text{E-}11 T^4 - 2.713468\text{E-}24 T^7 \\ 3695.00 < T < 6000.00 &: -30436.051 + 375.175 T - 54 T \cdot \ln T \end{aligned}$$

VANADIUM

Vanadium bcc-A2

$$\begin{aligned} \text{GHSE}_{\text{V}} &= G_{\text{V}}^{\text{bcc-A2}}(T) - H_{\text{V}}^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\ 298.15 < T < 790.00 &: -7930.43 + 133.346053 T - 24.134 T \cdot \ln T \\ &\quad - 3.098\text{E-}3 T^2 + 0.12175\text{E-}6 T^3 + 69460 T^{-1} \end{aligned}$$

$$\begin{aligned}
 790.00 < T < 2183.00 & : -7967.842 + 143.291093 T - 25.9 T \cdot \ln T \\
 & \quad + 0.0625E-3 T^2 - 0.68E-6 T^3 \\
 2183.00 < T < 4000.00 & : -41689.864 + 321.140783 T - 47.43 T \cdot \ln T \\
 & \quad + 644.389E29 T^{-9}
 \end{aligned}$$

Vanadium fcc-A1

$$\begin{aligned}
 \text{GFCC}_V &= G_V^{\text{fcc-A1}}(T) - H_V^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\
 298.15 < T < 4000.00 & : 7500.0 + 1.7 T + \text{GHSER}_V
 \end{aligned}$$

Vanadium hcp-A3

$$\begin{aligned}
 \text{GHCP}_V &= G_V^{\text{hcp-A3}}(T) - H_V^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\
 298.15 < T < 4000.00 & : 4000.0 + 2.4 T + \text{GHSER}_V
 \end{aligned}$$

Vanadium liquid

$$\begin{aligned}
 \text{GLIQ}_V &= G_V^{\text{liquid}}(T) - H_V^{\circ, \text{bcc-A2}}(298.15 \text{ K}) = \\
 298.15 < T < 2183.00 & : 20764.117 - 9.455552 T - 5.19136E-22 T^7 \\
 & \quad + \text{GHSER}_V \\
 2183.00 < T < 6000.00 & : 22072.353 - 10.0848 T - 6.44389E+31 T^{-9} \\
 & \quad + \text{GHSER}_V
 \end{aligned}$$

YTTRIUM**Yttrium hcp-A3**

$$\begin{aligned}
 \text{GHSER}_Y &= G_Y^{\text{hcp-A3}}(T) - H_Y^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\
 298.15 < T < 1500.00 & : -7347.055 + 117.532124 T - 23.8685 T \cdot \ln T \\
 & \quad - 0.003845475 T^2 + 1.1125E-08 T^3 - 16486 T^{-1} \\
 1500.00 < T < 1799.00 & : -15802.62 + 229.831717 T - 40.2851 T \cdot \ln T \\
 & \quad + 0.0068095 T^2 - 1.14182E-06 T^3 \\
 1799.00 < T < 3700.00 & : -72946.216 + 393.885821 T - 58.2078433 T \cdot \ln T \\
 & \quad + 0.002436461 T^2 - 7.2627E-08 T^3 + 20866567 T^{-1}
 \end{aligned}$$

Yttrium bcc-A2

$$\begin{aligned}
 \text{GBCC}_Y &= G_Y^{\text{bcc-A2}}(T) - H_Y^{\circ, \text{hcp-A3}}(298.15 \text{ K}) = \\
 298.15 < T < 1752.00 & : -1861.198 + 97.522398 T - 20.940576 T \cdot \ln T \\
 & \quad - 0.007995833 T^2 + 7.58716E-07 T^3 - 54349 T^{-1} \\
 1752.00 < T < 1799.00 & : -10207.724 + 195.741984 T - 35.0201 T \cdot \ln T \\
 1799.00 < T < 3700.00 & : +104813.954 - 386.167564 T + 39.8075986 T \cdot \ln T
 \end{aligned}$$

Yttrium liquid

$$\text{GLIQ}_Y = G_Y^{\text{liquid}}(T) - H_Y^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 1799.00 : 3934.121 + 59.921688 T - 14.8146562 T \cdot \ln T \\ - 0.015623487 T^2 + 1.442946E-06 T^3 \\ - 140695 T^{-1}$$

$$1799.00 < T < 3700.00 : -13337.609 + 258.004539 T - 43.0952 T \cdot \ln T \\ - 0.019918739 T^2 + 8.41308E-07 T^3 \\ - 31549963 T^{-1}$$

ZINC**Zinc hcp-Zn**

$$\text{GHSER}_{\text{Zn}} = G_{\text{Zn}}^{\text{hcp-Zn}}(T) - H_{\text{Zn}}^{\circ, \text{hcp-Zn}}(298.15 \text{ K}) =$$

$$298.15 < T < 692.68 : -7285.787 + 118.470069 T - 23.701314 T \cdot \ln T \\ - 1.712034E-3 T^2 - 1.264963E-6 T^3$$

$$692.68 < T < 1700.00 : -11070.559 + 172.34566 T - 31.38 T \cdot \ln T \\ + 470.514E24 T^{-9}$$

Zinc hcp-A3

$$G_{\text{Zn}}^{\text{hcp-A3}}(T) - H_{\text{Zn}}^{\circ, \text{hcp-Zn}}(298.15 \text{ K}) =$$

$$298.15 < T < 1700 : 2970 - 1.57 T + \text{GHSER}_{\text{Zn}}$$

Zinc bcc-A2

$$\text{GBCC}_{\text{Zn}} = G_{\text{Zn}}^{\text{bcc-A2}}(T) - H_{\text{Zn}}^{\circ, \text{hcp-Zn}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 2886.96 - 2.5104 T + \text{GHSER}_{\text{Zn}}$$

Zinc bct-A5

$$G_{\text{Zn}}^{\text{bct-A5}}(T) - H_{\text{Zn}}^{\circ, \text{hcp-Zn}} =$$

$$298.15 < T < 6000.00 : 2886.96 - 2.5104 T + \text{GHSER}_{\text{Zn}}$$

Zinc fcc-A1

$$G_{\text{Zn}}^{\text{fcc-A1}}(T) - H_{\text{Zn}}^{\circ, \text{hcp-Zn}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 2969.82 - 1.56968 T + \text{GHSER}_{\text{Zn}}$$

Zinc liquid

$$G_{Zn}^{\text{liquid}}(T) - H_{Zn}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 692.68 : 7157.213 - 10.29299 T - 3.5896E-19 T^7 \\ + \text{GHSER}_{Zn}$$

$$692.68 < T < 1700.00 : 7450.168 - 10.737066 T - 4.7051E+26 T^{-9} \\ + \text{GHSER}_{Zn}$$

ZIRCONIUM**Zirconium hcp-A3**

$$\text{GHSE}_{Zr} = G_{Zr}^{\text{T, hcp-A3}}(T) - H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 2128.00 : -7827.595 + 125.64905 T - 24.1618 T \cdot \ln T \\ - 4.37791E-3 T^2 + 34971 T^{-1}$$

$$2128.00 < T < 4000.00 : -26085.921 + 262.724183 T - 42.144 T \cdot \ln T \\ - 1342.895E28 T^{-9}$$

Zirconium bcc-A2

$$\text{GBCC}_{Zr} = G_{Zr}^{\text{T, bcc-A2}}(T) - H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 2128.00 : 7302.056 - 0.70335 T - 1.445606 T \cdot \ln T \\ + 4.037826E-3 T^2 - 9.7289735E-9 T^3 \\ - 7.6142894E-11 T^4 - 9737.0 T^{-1} + \text{GHSE}_{Zr}$$

$$2128.00 < T < 4000.00 : -4620.034 + 1.55998 T + 1.41035E+32 T^{-9}$$

Zirconium fcc-A1

$$\text{GFCC}_{Zr} = G_{Zr}^{\text{fcc-A1}}(T) - H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$130.00 < T < 4000.00 : 7600.00 - 0.9 T + \text{GHSE}_{Zr}$$

Zirconium liquid

$$\text{GLIQ}_{Zr} = G_{Zr}^{\text{liquid}}(T) - H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$130.00 < T < 2128.00 : +18147.703 - 9.080762 T + 1.6275E-22 T^7 \\ + \text{GHSE}_{Zr}$$

$$2128.00 < T < 4000.00 : +17804.649 - 8.91153 T + 1.343E+31 T^{-9} \\ + \text{GHSE}_{Zr}$$

Zirconium Laves-C14

$$G_{Zr:Zr}^{\text{Zr, Laves-C14}} - 3.0 H_{Zr}^{\circ, \text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 15000.0 + 3.0 \text{GHSE}_{Zr}$$

Zirconium Laves-C15

$$G_{\text{Zr:Zr}}^{\text{Zr,Laves-C15}} - 3.0 H_{\text{Zr}}^{\text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 15000.0 + 3.0 \text{ GHSEr}_{\text{Zr}}$$

Zirconium Laves-C36

$$G_{\text{Zr:Zr}}^{\text{Zr,Laves-C36}} - 3.0 H_{\text{Zr}}^{\text{hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 15000.0 + 3.0 \text{ GHSEr}_{\text{Zr}}$$

APPENDIX II: MAGNETIC CONTRIBUTION TO THE GIBBS ENERGIES OF THE PURE ELEMENTS (S.I. units) ¹

$$G^{\text{mag}} = R T \ln (\beta^{\text{mag}} + 1)g(\tau)$$

Chromium

Chromium bcc-A2

$$T_{\text{N}}(\text{bcc-A2,Cr}) = 311.5 \quad \beta^{\text{mag}}(\text{bcc-A2,Cr}) = 0.008$$

Chromium fcc-A1

$$T_{\text{N}}(\text{fcc-A1,Cr}) = 369.667 \quad \beta^{\text{mag}}(\text{fcc-A1,Cr}) = 0.82$$

Chromium hcp-A3

$$T_{\text{N}}(\text{hcp-A3,Cr}) = 369.667 \quad \beta^{\text{mag}}(\text{hcp-A3,Cr}) = 0.82$$

Iron

Iron bcc-A2

$$T_{\text{c}}(\text{bcc-A2,Fe}) = 1043.0 \quad \beta^{\text{mag}}(\text{bcc-A2,Fe}) = 2.22$$

Iron fcc-A1

$$T_{\text{c}}(\text{fcc-A1,Fe}) = 1043.0 \quad \beta^{\text{mag}}(\text{fcc-A1,Fe}) = 2.22$$

Manganese

Manganese cbcc-A12

$$T_{\text{N}}(\text{cbcc-A12,Mn}) = 95.0 \quad \beta^{\text{mag}}(\text{cbcc-A12,Mn}) = 0.22$$

Manganese bcc-A2

$$T_{\text{N}}(\text{bcc-A2,Mn}) = 580.0 \quad \beta^{\text{mag}}(\text{bcc-A2,Mn}) = 0.27$$

Manganese fcc-A1

$$T_{\text{N}}(\text{fcc-A1,Fe}) = 540.0 \quad \beta^{\text{mag}}(\text{fcc-A1,Mn}) = 0.62$$

Manganese hcp-A3

$$T_{\text{N}}(\text{hcp-A3,Fe}) = 540.0 \quad \beta^{\text{mag}}(\text{hcp-A3,Mn}) = 0.62$$

¹Scientific Group Thermodata Europe (S.G.T.E.) Data for Pure Elements, A.T. Dinsdale, Calphad, 15, 4, 317 - 425 (1991).

Nickel

Nickel bcc-A2

$$T_c(\text{bcc-A2,Ni}) = 575.0 \quad \beta^{mag}(\text{bcc-A2,Ni}) = 0.85$$

Nickel fcc-A1

$$T_c(\text{fcc-A1,Ni}) = 633.0 \quad \beta^{mag}(\text{fcc-A1,Ni}) = 0.52$$

Nickel hcp-A3

$$T_c(\text{hcp-A3,Ni}) = 633.0 \quad \beta^{mag}(\text{hcp-A3,Ni}) = 0.52$$

bcc-A2

$$\begin{aligned} \text{for } \tau = T < T_c \quad g(\tau) &= 1 - 0.905299383 \tau^{-1} - 0.153008346 \tau^3 \\ &\quad - 0.00680037095 \tau^9 - 0.00153008346 \tau^{15} \\ \text{for } \tau = T_c < T \quad g(\tau) &= -0.0641731208 \tau^{-5} - 0.00203724193 \tau^{-15} \\ &\quad - 4.27820805\text{E-}04 \tau^{-25} \end{aligned}$$

cbcc-A12

$$\begin{aligned} \text{for } \tau = T < T_c \quad g(\tau) &= 1 - 0.860338755\tau^{-1} - 0.17449124\tau^3 \\ &\quad - 0.00775516624 \tau^9 - 0.0017449124 \tau^{15} \\ \text{for } \tau = T_c < T \quad g(\tau) &= -0.0426902268\tau^{-5} - 0.0013552453\tau^{-15} \\ &\quad - 2.84601512\text{E-}04\tau^{-25} \end{aligned}$$

fcc-A1

$$\begin{aligned} \text{for } \tau = T < T_c \quad g(\tau) &= 1 - 0.860338755\tau^{-1} - 0.17449124\tau^3 \\ &\quad - 0.00775516624 \tau^9 - 0.0017449124 \tau^{15} \\ \text{for } \tau = T_c < T \quad g(\tau) &= -0.0426902268\tau^{-5} - 0.0013552453\tau^{-15} \\ &\quad - 2.84601512\text{E-}04\tau^{-25} \end{aligned}$$

hcp-A3

$$\begin{aligned} \text{for } \tau = T < T_c \quad g(\tau) &= 1 - 0.860338755\tau^{-1} - 0.17449124\tau^3 \\ &\quad - 0.00775516624 \tau^9 - 0.0017449124 \tau^{15} \\ \text{for } \tau = T_c < T \quad g(\tau) &= -0.0426902268\tau^{-5} - 0.0013552453\tau^{-15} \\ &\quad - 2.84601512\text{E-}04\tau^{-25} \end{aligned}$$

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