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**Crystal Structure  
Communications**

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## **Structure of tetralithium tetrametaphosphate pentahydrate**

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Supplementary Table 1. Analysis of anisotropic temperature factor data  
 - r.m.s. amplitudes (amp) [ $\text{\AA}$ ] and angles [ $^{\circ}$ ] with crystallographic  
 axes (deviations of amp  $\leq 0.003 \text{ \AA}$  deviation of angles  $\leq 0.3^{\circ}$ ).

For symmetrical reasons the thermal vibration ellipsoids around Pb  
 and N are rotation ellipsoids, therefore only the direction of the  
 rotation axis is given.

atom	amp	angle with		
		a	b	c
Pb	0.142			
	0.142			
	0.143	54.7	54.7	54.7
N	0.139			
	0.139			
	0.148		90.0	
O	0.133	110.1	102.2	23.8
	0.164	129.0	39.2	93.3
	0.217	45.8	53.5	66.5

42467

Supplementary Table 2. Structure Factors (observed and calculated), weights, differences ( $F_{\text{obs}} - F_{\text{calc}}$ ), weights, and rejection factor.

h k l

observed

reflection rejected ( $F_{\text{obs}} < F_{\text{calc}}$ ) (weight = 0)

reflection rejected (observed intensity less than  $2\sigma(F)$ )

PB(NO<sub>2</sub>)<sub>2</sub> LEAD NITRATE SACLAY 06/84 w = 0.0103

H	K	L	F(OBS)	F(CALC)	DELTA/SIGMA	EXT. FACTOR
1	1	1	16.375	15.309	2.7638	.9567
0	0	2	24.153	23.896	.8647	.9161
1	0	2	45.772	64.868	1.2776	.5767
1	1	2	48.308	47.219	2.0652	.7582
0	2	2	5.295	3.256	3.3818	.9988 *
1	2	2	16.648	16.977	-1.3094	.9707
2	2	2	92.108	92.385	-.2825	.4939
1	1	2	57.653	57.103	.8753	.7405
2	1	3	4.742	4.756	-.0263	.9981
0	2	2	8.475	5.593	2.0161	.9972
1	2	3	26.843	36.295	1.3509	.8964
2	2	3	12.554	12.025	2.0841	.9891
1	3	3	6.325	6.027	.8406	.9974
2	3	3	29.543	29.225	.9446	.9442
3	3	2	45.986	46.766	-1.5774	.8752
0	0	4	59.700	59.045	1.0103	.7641
1	0	4	38.617	37.622	2.3130	.8983
2	0	4	13.714	13.169	2.2395	.9879
3	0	4	24.903	24.871	.1080	.9616
1	1	4	44.828	44.650	.3566	.8635
2	1	4	18.390	18.998	-.3822	.9755
2	1	4	5.008	3.054	4.2483	.9994 *
0	2	4	27.632	26.973	2.0278	.9502
1	2	4	26.950	26.383	1.7596	.9533
2	2	4	12.008	10.697	5.1026	.9926 *
3	2	4	42.547	42.903	-.1174	.8970
1	3	4	14.396	14.046	1.4492	.9873
2	3	4	21.697	21.764	-.2345	.9724
3	3	4	40.323	29.248	6.8305	.9160
0	4	4	94.155	94.390	-.7259	.6128
1	4	4	13.305	13.691	-1.3400	.9896
2	4	4	2.736 *	.535	1.8620	1.0000 * *
3	4	4	4.910	1.691	3.2374	.9999 *
4	4	4	30.430	21.171	-2.1510	.9550
1	1	5	16.170	16.339	-.6538	.9838
2	1	5	23.148	22.592	2.0640	.9707
3	1	5	45.304	44.726	1.1507	.8972
4	1	5	5.347	4.189	1.5763	.9991
0	2	5	36.843	36.751	.2196	.9233
1	2	5	22.788	22.552	.8257	.9708
2	2	5	4.906	4.745	.2860	.9987
3	2	5	11.462	10.860	1.9438	.9938
4	2	5	51.378	51.725	-.6153	.8782
1	3	5	42.284	42.525	.9571	.9065
2	3	5	50.967	51.461	-.8617	.8708
3	3	5	43.392	43.409	-.0322	.9108
4	2	5	37.321	38.017	-1.6209	.9350
0	4	5	26.809	26.734	-.3781	.9644
1	4	5	14.191	13.869	1.0627	.9904
2	4	5	11.940	11.961	-.0715	.9931
3	4	5	5.536	2.154	3.4895	.9998 *
4	4	5	30.339	31.268	-1.1348	.9578
1	5	5	4.560	2.675	2.6877	.9997

PB(NC3)2 LEAD NITRATE SACLAY 06/84 W = 0.0103

H	K	L	F(OBS)	F(CALC)	DELTA/SIGMA	EXT. FACTOR
2	5	5	10.164	10.184	-.0587	.9953
3	5	5	32.136	31.826	.7963	.9569
4	5	5	12.349	12.132	.5852	.9939
5	5	5	19.309	19.634	-1.1390	.9848
0	0	6	75.051	73.030	2.0030	.7539
1	0	6	29.611	29.738	-.3657	.9542
2	0	6	5.260	3.392	3.2083	.9994
3	0	6	35.615	35.793	-.4335	.9396
4	0	6	5.142	5.773	-.8927	.9985
5	0	6	60.587	60.754	-.2580	.8540
1	1	6	19.177	19.283	-.3978	.9807
2	1	6	40.732	40.680	.1038	.9196
3	1	6	36.093	36.568	-1.1925	.9375
4	1	6	37.662	37.934	-.6292	.9367
5	1	6	34.251	34.229	.0524	.9513
0	2	6	16.511	16.474	.1299	.9862
1	2	6	5.524	5.106	.8970	.9987
2	2	6	59.973	60.551	-.8824	.8359
3	2	6	5.472	5.167	.5050	.9987
4	2	6	18.645	18.849	-.5130	.9843
5	2	6	31.058	22.104	-1.1722	.9578
1	3	6	29.123	29.343	-.5958	.9593
2	3	6	5.161	5.754	.6977	.9984
3	3	6	10.917	10.928	-.0325	.9946
4	3	6	10.760	10.558	.5307	.9952
5	3	6	17.876	18.045	-.5141	.9868
0	4	6	12.527	13.271	-1.3810	.9920
1	4	6	52.399	53.076	-1.1726	.8801
2	4	6	33.295	33.417	-.3067	.9516
3	4	6	10.098	10.646	-1.2399	.9951
4	4	6	44.348	44.921	-1.1312	.9204
5	4	6	5.044	4.532	.2204	.9091
0	5	6	32.900	34.200	-.7168	.9513
1	5	6	42.302	42.378	-.1579	.9276
2	5	6	22.720	22.872	-.4545	.9789
3	5	6	25.244	25.130	.3256	.9755
4	5	6	22.242	22.404	-.4615	.9812
5	5	6	54.651	54.110	.8787	.9890
0	6	6	8.051	8.613	-.9279	.9970
1	6	6	19.104	19.729	-1.7974	.9848
2	6	6	16.579	16.610	-.0818	.9894
3	6	6	5.956	2.703	3.6874	.9997
4	6	6	9.484	9.425	.1266	.9968
5	6	6	43.393	43.015	.7825	.9370
0	6	6	19.240	17.340	-.3682	.9829
1	7	7	10.096	9.557	.7150	.9956
2	7	7	42.233	41.057	.5740	.9263
3	7	7	2.570	4.778	1.1844	.9990
4	7	7	39.322	39.389	-.5824	.9412
5	7	7	7.028	6.314	.9631	.9985
0	7	7	27.564	27.781	-.6277	.9655
1	7	7	38.549	38.568	-.0434	.9352
2	7	7	10.166	9.869	.7033	.9957

PR(N03)2 LEAD NITRATE SACLAY 06/34 W \* 0.0103

H	K	L	F(OBS)	F(CALC)	DELTA/SIGMA	EXT. FACTOR
1	2	7	7.369	7.751	-.6115	.9974
4	2	7	5.513	5.080	.4981	.9989
1	2	7	41.019	41.791	-.3574	.9340
1	2	7	46.508	46.521	.2793	.9103
2	3	7	23.334	23.390	-.1671	.9769
3	3	7	46.668	47.032	-.6691	.9126
4	3	7	21.424	21.426	-.0072	.9819
5	3	7	38.549	39.225	-1.4599	.9429
6	3	7	7.542	7.150	.9745	.9981
0	4	7	39.914	40.295	-.8202	.9343
1	4	7	43.461	43.384	.1556	.9247
2	4	7	22.447	22.687	-.7216	.9792
3	4	7	15.351	15.090	.7320	.9910
4	4	7	13.782	13.261	1.3408	.9932
5	4	7	22.992	23.090	-.3011	.9804
6	4	7	4.339 *	1.996	1.6123	.9999 * **
1	5	7	37.457	37.946	-1.1077	.9445
2	5	7	5.219	6.759	-1.8463	.9982
3	5	7	33.364	33.411	-.1146	.9582
4	5	7	8.324	8.275	.1055	.9975
5	5	7	31.249	32.302	-2.7090	.9630
6	5	7	8.460	7.246	-1.3393	.9970
0	6	7	6.257	6.268	-.0144	.9985
1	6	7	21.014	21.119	-.2910	.9833
3	6	7	11.326	11.334	-.0237	.9953
4	6	7	16.579	16.566	.0403	.9902
5	6	7	11.187	11.141	.1051	.9957
6	6	7	8.801	7.007	2.9557	.9983
1	7	7	9.757	9.682	.1894	.9966
2	7	7	7.776	7.439	.5990	.9980
3	7	7	23.402	23.452	-.1500	.9806
5	7	7	21.626	21.902	-.7321	.9838
6	7	7	15.283	15.198	.1885	.9923
7	7	7	28.393	28.434	-.1322	.9738
0	0	8	43.325	42.942	.7714	.9253
1	0	8	38.958	39.257	-.6638	.9375
2	0	8	3.753 *	2.101	1.3226	.9998 * **
3	0	8	4.940	3.566	1.2727	.9995
4	0	8	15.079	15.166	-.2273	.9911
5	0	8	43.598	43.102	.8116	.9330
6	0	8	16.307	16.089	.6339	.9907
7	0	8	11.121	11.011	.2409	.9958
1	1	8	4.776	4.786	-.0149	.9990
2	1	8	14.501	14.248	.9633	.9917
3	1	8	57.380	57.939	-.8776	.8751
4	1	8	16.548	16.606	.1121	.9894
5	1	8	3.602 *	.594	2.9012	1.0000 * **
6	1	8	4.556	2.444	2.1054	.9998
7	1	8	7.946	7.327	1.0088	.9981
0	2	8	21.083	21.273	-.5621	.9815
1	2	8	49.579	49.406	-1.5086	.9051
2	2	8	35.274	35.370	-.2255	.9509
3	2	8	35.547	36.405	-1.9957	.9493

PE(IN03)2 LEAD NITRATE SACLAY 06/84 W = 0.0103

H	K	L	F(OBS)	F(CALC)	DELTA/SIGMA	EXT. FACTOR
			27.679	30.019	-.0574	.9563
4	2	R	7.028	6.974	.0944	.9982
5	2	R	19.309	19.424	-.3543	.9867
6	2	R	13.168	12.798	.9414	.9944
7	2	R	19.445	19.969	-1.5215	.9842
1	3	R	4.592 *	1.895	2.3111	.9999 * **
2	3	R	14.874	15.386	-1.3052	.9909
3	3	R	5.175	5.143	1.3951	.9990
5	3	R	3.923 *	3.236	.4401	.9996 * **
6	3	R	29.133	28.831	.7882	.9721
7	3	R	14.260	14.103	.3826	.9923
0	4	R	31.999	32.194	-.4785	.9808
1	4	R	16.784	16.284	1.3725	.9899
2	4	R	26.950	26.818	.3755	.9741
4	4	R	23.539	23.854	-.9400	.9800
5	4	R	6.011	6.318	-.3973	.9986
6	4	R	25.927	25.847	.2096	.9778
7	4	R	35.683	35.842	-.3916	.9533
1	5	R	8.254	7.914	.7339	.9977
2	5	R	31.317	31.205	.2922	.9654
3	5	R	17.927	12.679	.3671	.9944
5	5	R	7.232	9.358	-1.4790	.9976
7	5	R	27.223	26.977	.6216	.9751
0	6	R	27.905	28.129	-.6120	.9719
1	6	R	13.441	12.221	3.6890	.9947 *
2	6	R	15.147	15.462	-.8829	.9915
3	6	R	23.266	23.766	-1.4174	.9804
4	6	R	14.123	14.075	.1263	.9932
5	6	R	26.200	26.355	-.4100	.9767
6	6	R	18.490	18.987	-1.1639	.9881
7	6	R	16.443	15.379	2.3344	.9923
1	7	R	11.189	10.432	1.9286	.9962
2	7	R	5.354	5.198	.7858	.9991
3	7	R	4.326 *	.591	1.8990	1.0000 * **
4	7	R	8.529	7.376	1.8346	.9982
5	7	R	6.338	4.686	1.7636	.9993
6	7	R	6.523	4.313	2.2136	.9994
0	8	R	12.213	12.791	-1.2191	.9945
1	8	R	5.274	4.875	.3864	.9992
2	8	R	24.630	24.905	-.6982	.9795
3	8	R	6.700	6.748	-.0529	.9985
4	8	R	10.985	10.503	.8743	.9964
5	8	R	10.917	11.205	-.4393	.9959
6	8	R	23.607	23.848	-.6775	.9785
1	9	R	19.558	19.126	1.1941	.9877
2	9	R	16.511	16.919	-1.2696	.9894
3	9	R	13.792	12.885	2.4710	.9940
4	9	R	4.735 *	2.649	1.3352	.9998 * **
5	9	R	6.727	6.848	-.1511	.9984
6	9	R	38.413	38.327	.1856	.9520
7	9	R	7.096	7.329	-.2452	.9982
8	9	R	37.562	37.772	-.2438	.9473
0	2	O	10.848	11.219	-.7886	.9953
1	2	O				

PR(FC3)2 LEAD NITRATE SACLAY 06/84 W = 0.0103

H	K	L	F(OBS)	F(CALC)	DELTA/SIGMA	EXT. FACTOR
3	2	0	11.667	11.553	.2942	.9951
4	2	0	18.080	18.252	-.5114	.9881
5	2	0	27.490	26.993	1.3568	.9748
6	2	0	11.940	12.114	-.3576	.9950
7	2	0	4.326 *	3.454	.3660	.9996 * **
8	2	0	5.950	4.081	1.0149	.9992
1	3	0	9.484	9.791	-.8055	.9965
2	3	0	32.272	32.689	-1.0787	.9615
3	3	0	51.239	51.486	-.4323	.9089
4	3	0	27.769	28.324	-1.5238	.9720
5	3	0	13.577	13.795	-.5530	.9934
6	3	0	7.437	6.865	.7794	.9984
7	3	0	6.175	5.463	.7434	.9990
8	3	0	9.415	9.430	-.0198	.9971
0	4	0	25.351	24.579	2.3239	.9783
1	4	0	14.737	14.341	1.2207	.9926
2	4	0	25.586	25.860	-.7817	.9763
3	4	0	3.616 *	1.074	1.2338	1.0000 * **
4	4	0	11.253	10.758	1.1228	.9960
5	4	0	15.829	16.176	-.9026	.9911
6	4	0	5.963	2.245	3.2198	.9993 *
1	5	0	7.164	6.783	.7002	.9984
2	5	0	4.747	2.789	1.8648	.9997
3	5	0	21.287	21.660	-1.0495	.9839
4	5	0	10.848	10.168	1.3684	.9965
5	5	0	5.515	5.250	.3257	.9991
6	5	0	22.880	23.639	-.5725	.9820
0	6	0	3.691 *	2.437	.1898	.9996 * **
1	6	0	26.814	26.666	.4234	.9759
2	6	0	21.424	21.488	-.1730	.9844
3	6	0	4.160 *	4.582	-.2897	.9993 * **
4	6	0	10.849	10.196	1.7895	.9890
5	6	0	4.537 *	.947	1.7426	1.0000 * **
6	6	0	23.880	23.667	.4993	.9819
1	7	0	34.251	33.933	.7666	.9621
2	7	0	16.102	16.226	-.2848	.9913
3	7	0	7.232	6.504	.8785	.9986
4	7	0	18.595	18.035	1.4574	.9895
0	8	0	10.784	16.983	-.4483	.9906
1	8	0	7.096	7.424	-.3352	.9982
2	8	0	7.025	8.652	-1.8257	.9976
3	8	0	14.306	14.649	.3168	.9930
0	0	10	10.012	1.640	28.6329	.9999 *
1	0	10	34.660	34.558	.2568	.9581
2	0	10	28.617	38.397	.4919	.9489
3	0	10	23.607	22.185	1.2029	.9813
4	0	10	52.263	51.955	.5243	.9112
5	0	10	26.577	26.145	1.3754	.9771
7	0	10	4.735 *	1.033	1.7065	1.0000 * **
1	1	10	12.690	12.409	.5853	.9944
2	1	10	23.334	23.541	-.6181	.9805
3	1	10	4.326 *	.157	2.4430	1.0000 * **
4	1	10	17.396	17.400	-.0039	.9896



FB(N03)2 LEAD NITRATE SACLAY 06/84 \* = 0.0103

H	K	L	F (OBS)	F (CALC)	DELTA/SIGMA	EXT. FACTOR	
1	1	10	18.831	19.366	1.2209	.9887	
1	1	10	23.266	23.294	-.0722	.9821	
7	1	10	13.032	13.198	-.3222	.9543	
0	2	10	20.673	21.739	-3.2276	.9833	*
1	2	10	6.407	6.259	.2450	.9986	
2	2	10	4.626	3.942	.6340	.9995	
3	2	10	3.616 *	1.107	1.7266	1.0000	* **
4	2	10	3.425 *	.155	1.9171	1.0000	* **
5	2	10	14.942	14.291	1.5325	.9932	
6	2	10	16.170	16.349	-.4098	.9912	
7	2	10	6.257 *	1.050	3.2282	1.0000	* **
1	3	10	10.644	9.968	1.6453	.9965	
2	3	10	13.509	13.319	.4840	.9939	
3	3	10	5.103	3.773	1.2894	.9995	
4	3	10	4.237 *	4.735	-.3491	.9992	* **
5	3	10	9.620	9.126	.7864	.9972	
6	3	10	4.994 *	2.348	1.6938	.9998	* **
0	4	10	52.195	52.367	-.2944	.9099	
1	4	10	24.085	24.455	-1.1052	.9796	
2	4	10	14.191	13.676	1.3225	.9936	
3	4	10	11.372	12.641	-1.6259	.9546	
4	4	10	14.191	13.439	1.7057	.9940	
5	4	10	39.982	39.610	.7515	.9500	
6	4	10	11.258	11.092	.3732	.9953	
7	5	10	31.044	31.001	-.3850	.9478	
1	5	10	16.102	15.934	.6330	.9917	
2	5	10	13.919	13.811	.2074	.9938	
3	5	10	5.922	5.054	.7942	.9992	
4	6	10	5.172	1.369	3.2001	.9999	*
1	6	10	15.351	14.752	1.3648	.9928	
2	6	10	6.492	6.000	.4342	.9988	
3	6	10	33.022	33.256	-.5300	.9645	
4	6	10	8.256	7.961	.3556	.9979	
2	7	10	25.244	25.039	.5975	.9789	
1	1	11	11.735	10.712	2.1644	.9961	
2	1	11	4.837 *	1.974	2.0987	.9999	* **
3	1	11	21.424	21.022	.9741	.9856	
4	1	11	14.464	14.267	.4890	.9931	
0	2	11	15.692	15.218	1.3440	.9922	
1	2	11	5.295	5.142	.1547	.9991	
2	2	11	5.254	3.417	1.5725	.9996	
3	2	11	27.632	27.483	.3783	.9753	
4	2	11	11.735	10.851	1.4921	.9962	
5	2	11	9.006	8.808	.3625	.9974	
1	3	11	21.901	21.957	-.1425	.9840	
2	3	11	20.332	20.622	-.7590	.9860	
3	3	11	13.850	14.493	-1.2719	.9931	
4	3	11	22.780	22.656	.3100	.9834	
5	3	11	4.735 *	4.221	.2367	.9994	* **
0	4	11	4.496 *	.322	2.9276	1.0000	* **
1	4	11	4.574 *	.524	2.2779	1.0000	* **
2	4	11	9.143	8.593	.7609	.9976	
3	4	11	27.564	26.756	1.9102	.9769	

## STRUCTURE FACTORS

PAGE 7

PR(MO?) LEAD NITRATE SACLAY 06/84  $\mu = 0.0103$ 

H	K	L	F(OBS)	F(CALC)	DELTA/SIGMA	EXT. FACTOR
1	5	11	16.352	16.721	.2697	.9909
2	5	11	8.392	7.776	-.8154	.9980
3	5	11	13.441	13.730	-.5200	.9939
0	6	11	32.954	23.344	-.8089	.9645
0	0	12	11.740	10.206	2.1231	.9965
1	0	12	15.078	14.264	2.0697	.9933
2	0	12	7.845	7.420	.5013	.9982
3	0	12	15.829	16.614	-1.6385	.9910
1	1	12	12.590	12.240	1.0037	.9951
2	1	12	7.300	7.420	-.1365	.9982
3	1	12	11.121	11.592	-.7455	.9956
0	2	12	17.398	17.093	.7243	.9905
1	2	12	13.305	12.918	.3694	.9945
2	2	12	24.016	23.809	.5188	.9817
2	2	12	21.014	20.470	1.0497	.9865
1	3	12	6.059	4.569	.9972	.9993